DENSIFICATION OF GEODETIC CONTROL NETWORKS UNDER REPRODUCING PARAMETRIC AND STOCHASTIC FIDUCIAL CONSTRAINTS

BY

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A thesis submitted in partial fulfilment for the degree

(monordal)

of

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DECLARATIONS

This thesis is my original work and has not been presented for a degree in any other university.

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15.10.2001

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This thesis has been submitted for examination with our approval as university supervisors

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ABSTRACT

A principal consideration in densification of geodetic systems has been the need to incorporate the stochasticity of the datum parameters in the densification process. The special question however is *how to incorporate the stochasticity of the datum parameters in the estimation of the new parameters while reproducing the datum parameters together with their stochasticity (respectively reproducing parametric and stochastic fiducial constraints)*. A number of approaches addressing the above question have been proposed. These include: static-dynamic, pseudo-dynamic and sub-optimal network fusion approaches. Of these, pseudo-dynamic, staticdynamic and sub-optimal network fusion approaches reproduce the datum parameters and their stochasticity while static and dynamic approaches do not possess the reproducing quality.

The aim in this study was to evaluate the practical applicability, and to establish the suitability, of two densification approaches with the reproducing quality. The static-dynamic and suboptimal fusion approaches are considered, with a view to identifying their strength and weaknesses as approaches to densification of geodetic systems. The results are compared to establish which of the approaches is best suited for recommendation to be adopted for geodetic densification and under what circumstances. For a general perspective, the non-reproducing techniques namely; static and dynamic approaches are also discussed, evaluated and compared to the two approaches. Although the pseudo-dynamic approach has the reproducing capability, it is not considered since the approach has the drawback in that. on one hand datum parameters are treated as non-stochastic entities, thus fixed, while on the other hand, they are treated as stochastic, resulting in an inconsistent estimation model.

To evaluate these approaches, each of the techniques is used to adjust simulated and real test geodetic networks at two levels of densification. The simulated geodetic network consists of three first order, three second order and nine third order points while the real geodetic network points were extracted from the national geodetic network of Kenya consisting of eleven first order, fifteen second order and ten third order points. For each approach, and at every level of densification on the two networks, the parameters, the standard errors and their corresponding error ellipses were compared against each other.

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The results indicate that the datum parameters in the static-dynamic and the sub-optimal fusion approaches are reproduced together with their stochasticity, that is, maintained definitive. Although the datum parameters are reproduced together with their stochasticity, the new point parameters obtained using sub-optimal fusion approach are similar to the parameters obtained using the dynamic approach. That is, it compares to adjusting the network using the dynamic approach and applying a corrective term on the datum parameters to keep them unchanged. The covariance matrices obtained through the two approaches are closer to each other as demonstrated by the confidence error ellipses. The results generally demonstrate that both the static-dynamic and sub-optimal fusion approaches give more realistic estimates of the parameters than the static and dynamic approaches.

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DEDICATION

To my father Narkiso Ogonda Ong'wen To my mother Mary Ochung' Ogonda And to my wife Carren Adhiambo You have given me so much. This is dedicated to you.

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NOTATION

Listed below are the notations used in the text. The page in which the notation first appears is given in parenthesis.

y is the $u \times 1$ vector of observation increments (14)

x is the $m \times 1$ vector of unknown parameters (14)

 x_1 is the $c \times 1$ vector of parameters with prior information (15)

 x_2 is the $(m-c) \times 1$ vector of parameters without prior information (15)

 \hat{x}_{1} as defined in the text (15)

 \hat{x} , as defined in the text (15)

A is the $n \times m$ coefficient matrix (14)

 $[A_1 A_2]$ as defined in the text (15)

W is the $n \times n$ positive definite weight matrix (14)

e is the $n \times 1$ vector of random observation errors (14)

 e_0 is the $c \times 1$ vector of restriction errors (17)

D(y) is the dispersion of y (14)

 Σ is the dispersion matrix (14)

 $\Sigma_{\rm w}$ is the dispersion matrix of the observations (18)

 Σ_{-} is the dispersion matrix of the restrictions (18)

 Σ_{ac} as defined in the text (25)

 σ_0^2 is the a-priori variance of unit weight (14)

 σ_0^2 is the a-posteriori variance of unit weight (15)

D(e) dispersion of e (14)

K is the $c \times 1$ restriction design matrix (17)

 Z_0 is the $c \times 1$ vector of restriction parameters (17)

C denotes the covariance (17)

 $W_{\rm r}$ is the weight of the restrictions (17)

W, is the weight of the observations (17)

n is the number of observations (18)

c is the number of the restrictions (18)

m is the number of unknown parameters (18)

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- D(x) dispersion of x (21)
- $D(\hat{x}_{1})$ is the dispersion of \hat{x}_{1} (15)
- $E(\hat{x})$ is the expectation of \hat{x} (15)
- $E(x_2)$ is the expectation of x_2 (15)
- N is the normal equation matrix (15)
- G is the orthogonal matrix made up of eigenvectors (19)
- Q_{xx} is the cofactor matrix of the unknown parameters (19)
- $tr(Q_{xx})$ is the trace of Q_{xx} (19)
- Δx_i is the approximate value of the x_i coordinates (20)
- Δy_i is the approximate value of the y_i coordinates (20)
- L is the Lagrange function (17)
- N_r as defined in the text (22)
- λ vector of Lagrange multipliers (17)
- $\overline{\sigma}_c$ is the circular probable error (52)
- σ_E, σ_N is the standard error in E and N respectively (52)
- E, N are the easting and northing co-ordinates respectively (33)
- $\sigma_{\rm v}^2$ is the variance of the N (55)
- σ_{E}^{2} is the variance of the E (55)
- σ_{EV} is the covariance between E and N (55)
- ψ is the bearing of a (55)
- H_o is the null hypothesis (118)
- $H_{\rm a}$ is the alternative hypothesis (118)
- χ_m^2 is the Chi-square test at *m* degrees of freedom (118)
- $F_{m_1,m_2} = \frac{\sigma_1}{\overline{\sigma}_2}$ is the F-test statistic at m_1, m_2 degrees of freedom for independent samples 1 and 2 (123)

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- ϕ is the target function (29)
- ζ as defined in the text (25)
- y_{\pm} as defined in the text (25)
- $A_{\rm c}$ as defined in the text (25)
- W_{c} as defined in the text (25)

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INTRODUCTION

1.1 The Geodetic Densification Problem

The introduction of new points into an already existing geodetic system of control points is termed densification. The densification process, that is, the measurement of geometrical relations of certain new points to a number of previously estimated control points is a problem commonly encountered by geodesists in their work. The basic guiding principle in geodesy, "from the whole to the part", is as valid today as it was hundreds of years ago. Progress in technology, though, has had an important effect in the amount of data that can be collected and analyzed in geodetic systems. In this context, emphasis has been put in the study of efficient and accurate densification approaches.

The basic problem of geodetic densification is two-fold; firstly the problem of optimal design of a geodetic system and secondly the problem of establishing the most suitable technique for processing and for post analysis of the system. Having achieved the optimal design of a geodetic system in its fundamental configuration, then as a rule, the densification problem arises in that with additional observations, certain new points have to be intercalated into the fundamental network. This generally involves interpolation, or to a lesser extent, extrapolation about the datum (fiducial) points. Densification, as addressed in this report, begins by a given field of datum points at which certain prior information is known, which then is followed by the interpolation of the information at points other than the datum (fiducial) points. The question is then that of how to handle the position values of the already fixed stations.

The densification problem has existed for many years and has been considerably applied to problems in geodesy, hydrography, cadastral surveying, engineering surveying, photogrammetry and recently also in the Global Positioning System (GPS). In Kenya for example, several first order, second order, and third order frameworks of survey stations have been established and

permanently marked on the ground via the process of densification using triangulation, traversing and Doppler satellite positioning techniques on the Arc Datum 1960 based on Clarke's 1880 ellipsoid. Research into suitable densification approaches thus becomes clearly relevant to the needs of the geodetic community as also evidenced by the number of studies on the subject by several researchers.

The central concern in both the design and processing of geodetic systems is the formulation of functional relations between unknown parameters and the observables. The unknown parameters are then estimated through an estimator that only succeeds in optimal statistics characteristics if it is unbiased, of minimum variance (best) and invariant from any other geodetic estimation results calculated in the same model. In geodetic practice, in one form, the functional models are linear and several such estimates which satisfy few of the optimal statistics characteristics have been proposed and include for example Best Linear Estimate (BLE), Best Linear Unbiased Estimate (BLUE), Best Linear Minimum Biased Estimate (BLMBE).

In free network adjustment of geodetic systems, the "datum" is normally defined over a number of network points in "free mode". and this results in the problem that neither the dispersion matrix nor the configuration matrix of the system are of full rank. The results therefore are biased estimates where the bias could be a minimum and the unknowns are estimated with minimum variance. This, as noted by *Grafarend [1976]*, is highly preferred in the adjustment of first order and underdetermined geodetic systems where no prior information is available.

In second and higher order densification of geodetic systems. incorporation of prior information in the densification process results in two data sets that need to be fused. Depending on the manner in which the reference data (prior information) is handled in the process, we have the following four possible cases:

- Holding existing prior information as fixed and errorless.
- Treating existing prior information as fixed and errorless but propagating their covariance information.
- Perform weighted parameter adjustment with the existing prior information weighted by their predetermined covariance matrix.

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• Holding existing information as fixed stochastic entities.

The conventional approach to densification was performed by over-constraining the geodetic system, in which case, the control point parameters are considered as fixed, non-stochastic, entities in the form of exact restrictions (respectively exact prior information). However the control points should be considered stochastic having been obtained from previous adjustment. Classically, one performs a number of observations on a framework of control parameters and new parameters and then deduces, from the observations, the new parameters on the assumption that the control parameters are known exactly. The approach whereby the control point parameters are considered as errorless has been termed as *hierarchical densification* by *Pelzer [1980]*, as *static densification* by *Cooper [1987]* and *Aduol [1993]* while *Vanicek and Lugoe [1986]* refer to it *as over-constrained adjustment of densification*. The approach, although reproducing the results from the previous adjustment exactly, gives too optimistic results as a consequence of neglecting the variance-covariance matrix of the datum points and is therefore considered rarely optimal among all possible reproducing techniques. The approach is also non-rigorous in the statistical sense.

The proposal to consider the control point parameters as stochastic was already made by the beginning of the twentieth century as noted by *Wolf [1983]*. The new points were estimated on the basis of the static mode, while the stochasticity of the estimated points were computed through error propagation incorporating the stochasticity of the control point parameters *[Aduol 1993]*. Works by *Van Mierlo [1984]*, *Nickerson et al. [1986]* and *Wolf [1984]* refer to this approach as *quasi-hierarchic or pseudo-dynamic*. The quasi-hierarchic (respectively pseudo-dynamic) approach has the disadvantage that the model for parameter estimation and that for stochastic on one hand and on the other treats them as non-stochastic *[Aduol, 1993]*. The end result is that the covariance matrix of the new points is updated by a corrective term.

In another approach, the densification is done by considering control point parameters as stochastic and then proceed to estimate all the new points including the control points by combining them in the model the parametric and stochastic constraints. *Vanicek and Lugoe* [1986] noted that, a statistically rigorous way to densification of geodetic systems is to simultaneously adjust both the prior information of the control points and the introduced framework of new points through the imposition of properly weighted constraints on existing control point parameters. This is only achieved through rigorous propagation of the covariance matrix of the fiducial constraints. This approach has been referred to by, among others. *Pelzer*

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[1980], El-Hakim [1982] and Grafarend and Schaffrin [1988] as dynamic model. The result of the rigorous densification of the geodetic systems is that the existing control framework changes position due to the effect of new observations propagated into the existing system. This is thought, as indicated by Vanicek and Lugoe [1986], "to be rather unfortunate from the practical point of view". One is left wondering whether to replace the datum points with the new results or not. This may be justified if it is established that the newly densified framework is more accurate than the existing reference framework as would be the case in observations derived from Very Long Baseline Interferometry (VLBI) for instance, or if blunders or systematic errors are detected in the existing control framework. Although stochastically rigorous, powerful and efficient, the dynamic approach has the drawback that the control point parameters change to new values with every new single point added to the geodetic system. Therefore, if control point parameters are not properly updated, accumulation of inconsistencies may destroy the quality of the geodetic system. This is the problem experienced by the dynamic approach to densification, whose practical applicability however is still an open question.

It is evident that there exist considerable differences in quality between the datum points and new points in densification of networks. *Schaffrin* [1985] suggested that it was not appropriate to deal with both the new and datum points in the same manner by simply adding the previous coordinates as "pseudo observations", e.g. as used in the static and dynamic approaches, instead he constructed a more robust method "the best homogeneously linear (weakly) unbiased predictor" (homBLUP). This method proved to be robust enough against eventual errors in the prior information without destroying the "homogeneity of the neighbourhoog".

Hierarchical models for densification are considered the most appropriate approaches to densification since they keep the parameters of higher order points unchanged. The problem encountered in hierarchical densification however is that of how to incorporate the datum point covariances in the estimation of the new point parameters in the most rigorous and proper way. This is a fact that was already fully recognized by *W. Baarda* in writing specifications for the activities of the Dutch cadastre [Baarda, et al. 1956].

To address the geodetic densification problem, *Aduol [1993]* proposed an approach to densification referred to as the *static-dynamic model*. In this approach, the control points are treated as stochastic restrictions (respectively stochastic prior information) while the control point parameters are reproduced with their covariance matrix as definitive with the concept of a

consistent mathematical formulation and thus combines the properties of both *static* and *dynamic* approaches. This approach is referred to as, *estimation with incomplete prior information* by *Theil* [1963,1971] and as *stepwise regression* by *Toutenburg* [1975], *Bibby and Toutenburg* [1977] and *Toutenburg* [1977].

In order to overcome the same geodetic densification problem, *Schaffrin [1998]* has proposed the *sub-optimal fusion* approach. In the *sub-optimal fusion* approach the best linear uniformly unbiased estimate (BLUUE) is determined. Like the *static-dynamic* approach, *sub-optimal fusion* approach has the property that the datum parameters are exactly reproduced and their stochasticity incorporated in the rigorous estimation of the new point parameters together with their dispersion matrix. In this study, the performance of the sub-optimal fusion approach as regards the rationale of overcoming the geodetic densification problem of exactly reproducing the datum point parameters together with their stochasticity in the densification process has been investigated.

1.2 Statement of the Problem

In the conventional approach to the densification of the geodetic systems, termed *static* by *Aduol* [1993], the control points are considered as non-stochastic fixed entities. The consideration of parametric and stochastic fiducial constraints as exact resulted in the estimated new points having less dispersion than they really have, thus giving falsified estimates [Aduol, 1999].

The need to incorporate the stochasticity of the control point parameters in the estimation of the new point parameters led to the development of the dynamic approach in which the control point parameters obtain corrections for their values hence new values are obtained after the adjustment. As a result, the control point parameters change their values dynamically in principle with every single measurement added to the system, that is, the control points move during adjustment. If the control points are not properly updated, accumulation of inconsistencies may destroy the quality of the geodetic system [Schaffrin, 1998].

The principal problem in geodetic densification therefore is, how to incorporate stochasticity of the control points in the estimation of the new points while reproducing the control point parameters together with their dispersion matrix (respectively reproducing parametric and stochastic fiducial constraints). To address this problem some authors have proposed the

adoption of the dynamic approach, but to ignore changes to the control point parameters unless they are "significantly" large. In this case, where the changes to the control point parameters are neglected on the basis of whether they are "large" or not, the final parameters adopted cannot be consistent with the mathematical model used for the estimation of the new point parameters.

In the static-dynamic approach proposed by *Aduol [1993]*, the properties of the static and dynamic models are combined, thus the control point parameters are taken as stochastic while at the same time retain their definitiveness. Addressing the same problem, *Schaffrin [1998]* has proposed a densification approach with similar properties as the static-dynamic approach. The approach reproduces control point parameters together with their dispersion matrix while incorporating their stochasticity in the estimation of the new points. *Schaffrin [1998]* has referred to the approach as the *sub-optimal network fusion*, which gives reproducing best linear uniformly unbiased estimates (repro *BLUUE*).

Densification of geodetic systems calls for use of proper estimation techniques that also give the reliability of the estimated parameters. Studies by *Miima [1997]* indicated that the models that incorporate the *static-dynamic* concept. that is, reproducing the control point parameters while incorporating their stochasticity in the estimation of new point parameters, produce best statistically agreeable results. There is need therefore to study the *sub-optimal network fusion* approach against the *static-dynamic* approach with a view to evaluating its practical applicability in a densification exercise and overall suitability in densification work in general.

In this study, the approaches with reproducing property (i.e. *static-dynamic and sub-optimal network fusion*) are considered. The approaches are compared with each other in view of determining their relative effectiveness to densification of geodetic systems.

The *static* and *dynamic* approaches discussed above have been used to compute the parameters and the results compared to those obtained by the static-dynamic and sub-optimal fusion approaches. It is however noted that the static approach does not possess the reproducing property, that is, it reproduces the control parameters while the variance-covariance matrix vanishes. Similarly the *dynamic* approach does not have the reproducing property in that both the control point parameters and their stochasticity are updated through the densification process.

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1.3 Objectives of the Study

The main objective of this study is to demonstrate practical applicability, and to evaluate the suitability, of the *sub-optimal network fusion* approach to densification as proposed by *Schaffrin* [1998], in relation to the *static-dynamic* densification approach as proposed by *Aduol* [1993]. Through this, it is hoped to gain an insight into the relative effectiveness of these two approaches to densification, i.e. how to incorporate the stochasticity of the control points in the estimation of the new points while reproducing the parametric and stochastic fiducial constraints, and also to establish which of the approaches is best suited for recommendation to be adopted for densification and under what circumstances.

The specific objectives of the study are:

- To obtain densification results of the real and the simulated geodetic systems through the *Static-Dynamic* approach and the *Sub-Optimal network fusion* approach.
- Analyze and compare the accuracy, efficiency and consistency between the prior information and the densification results obtained by the two approaches.
- To determine the reliability and suitability of the two approaches relative to each other.

1.4 Literature Review

With the improvements on positioning technology, several studies have been carried out on densification to provide for more precise and refined control points. The densification concepts though remain unchanged, as stated in [Aduol 1993] "In the densification of networks we normally have two groups of points to be handled in the parameter estimation. These are the already existing points over which the network datum is defined, and then there are the densification points to be newly coordinated".

In densification of geodetic systems, the manner in which the prior information is handled classifies the various densification approaches as either *reproducing or non-reproducing* densification techniques. In the conventional approach referred to as *static* approach by among others *Cooper* [198⁻] and *Aduol* [1993], and the *hierarchical* 'approach by. among others, *Pelzer* [1980], the prior information about the control points are treated as exact non-stochastic entities. The *static* approach has the problem in that, it does not reproduce the stochastic fiducial constraints but rather reproduces the parametric fiducial constraints as exact non-stochastic

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entities. This approach thus reproduces the control point parameters at the expense of neglecting their corresponding variance-covariance matrices.

The need to consider control point information as stochastic was already recognized as early as 1882 when *W. Jordan* advocated that the control points in the densification of geodetic systems be treated as "correlated observation" *[Wolf 1983]*. The early researchers estimated the new points on the basis of *static* approach, while the stochasticity on the estimated new points were computed through "error propagation" incorporating the errors on the control points *[Aduol 1993]*. Recent works on this approach have termed it as *quasi-hierarchic* or *pseudo-dynamic [Van Mierlo 1984, Nickerson et al. 1986]*.

Theil and Goldberger [1961] highlighted the uncertainties that arise when, during statistical estimation of economic relations, a hypothesis is formulated, and appropriate computation to provide desirable estimates of parameters of the linear relation carried out, only to find out that the estimated income elasticity of some commodity was negative. In their search for a statistical estimator, *Theil and Goldberger [1961]* are quoted as saying "The difficulty seems to be that the investigator has a prior knowledge which he can not conveniently incorporate in the hypothesis and which he therefore omits. This kind of a prior knowledge, however, is precisely the major source of rejections in hypothesis. It seems clear that it is logically more consistent to incorporate such knowledge in the hypothesis right at the beginning than exclude it from the hypothesis and reject it afterwards when the results contradict the omitted knowledge".

Theil and Goldberger [1961] then proposed a model of "mixed" estimation that was an effort to incorporate prior knowledge of coefficients in regression analysis and other linear statistical models. The prior knowledge was formulated in terms of prior estimates of parameters, which were assumed to be biased and to have a moment matrix [Miima 1997]. This can be considered as part of the fundamental mathematical formulation of the dynamic model.

Theil [1963] analyzed the use of incomplete prior information in regression analysis by considering the combination of prior and sample information with the fact that both are stochastic but independent of each other. He tested the compatibility of the two and proposed a measure for the relative contribution of sample and prior information to the results of estimation.

Toutenburg [1974] developed an approach for combining stochastic prior information in a vector of regression coefficients with incomplete prior information on the variances of the disturbance terms. This enlarged the general linear regression model to yield a restricted regression model. This work was actually the basis for the *static-dynamic* approach.

Blaha [1974] studied densification networks when fixed parameters were neglected in the variance-covariance propagation with the aim to correct the variance-covariance matrices for the contribution of such uncertainties. This was to be done through considering the general least-squares solution with weighted unknown or some weighted and some unknown parameters, hence providing a more general approach to *hierarchical* densification. His work was an expansion on the work of *Papo [1973]*, who had he proposed a method by which, without altering the values of the adjusted parameters their a-posteriori covariance matrix could be improved by inclusion of the effect of uncertainties in the constants of the adjustment process. The algorithm outlined in *Blaha [1974]*, is a method that permits the propagation of random errors from a previously determined network into the accuracy estimates and solution vector.

Cooper and Leahy [1978] undertook densification of a geodetic system under two approaches, one, by considering the control points to be fixed absolutely and in the other by regarding the control points as correlated, and hence not fixed. The result of their study indicated that the approach where the control points are treated as correlated observations yielded better results. It has to be noted that this approach has a weakness as pointed out in [Aduol 1993] through the statement "Taken to its ultimate, one has for instance with this that where only a single point is being coordinated by "intersection" with the datum points forming a part of a national geodetic reference system, the single new point would (theoretically) cause all points in the national network to acquire new coordinate values and new stochastic parameters. With this we note that the concept of a national geodetic reference system is effectively lost."

In [Koch. 1983a]. densification of geodetic systems by considering the fixed control points as random variables is discussed. He also addressed a special case of transformation of covariance matrix for the parameters of the control points if the system of the control points was changed during the densification process.

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In trying to answer the question of whether to consider the control points as stochastic or as fixed non-stochastic entities, *Van Mierlo [1984]* suggested the adoption of a "compromise solution". He proposed the consideration of fundamental geodetic systems as stochastic so that their covariances are fully taken into account while at the same time they are considered as non-stochastic, in which case they are not corrected by the resulting residuals and the discrepancies are arbitrarily put to zero [*Miima 1997*]. *Wolf [1983]* demonstrated that this approach led to a bias in the residual of the geodetic system, thus giving falsified angles and distances to the given points.

Schaffrin [1984] proposed the adoption of the *dynamic* approach to densification but to ignore the changes to the control point parameters and their stochasticity unless they are "significantly large". In this case *Aduol* [1993] states however, that as long as the changes are merely neglected on the basis of whether they are large or not, the final parameters adopted can not be consistent with the mathematical model adopted for the estimation of the new parameters.

Schaffrin [1985] suggested that it was not appropriate to deal with both the new and old measurements in the same manner by simply adding the previous parameters as "pseudo observations" as in the case of *static* and *dynamic* approaches. Instead he constructed a more robust method called " *the best homogeneously linear (weakly) unbiased predictor*". This proved to be robust enough against eventual errors in the prior information without destroying the "homogeneity of the neighbourhood".

Nickerson et al [1986] performed densification of a second order geodetic control network by static. dynamic and semi-dynamic approaches. The results indicated, that the dynamic approach provided realistic error ellipses for geodetic system densification but resulted in the change of control point parameters. They recommended that "one simply records and not apply the corrections to the control point parameters and use the covariance information provided by the dynamic approach". It can be noted that this assumption leads to the distortion in geodetic systems which is not reflected in the confidence ellipses.

Vanicek and Lugoe [1986] suggested that a statistically rigorous densification of geodetic systems must consist of a simultaneous adjustment of both the reference control point framework and the new point framework. Vanicek and Lugoe [1986] state that: "The statistically rigorous way of adjusting the new points, i.e. the densification network, into the

existing network is to adjust both networks together, using both the 'old' and 'new' observations. Alternatively, the new densification network, including the junction points, can be rigorously adjusted in a phase adjustment mode, where the information from the existing network is propagated into the new phase of the adjustment by (1) using the existing positions of the junction points for initial estimates; and (2) using the inverse of the covariance matrix of these existing positions (as obtained from the previous adjustment) for a prior weight matrix of the junction points". They noted that, unfortunately, as a result of the rigorous adjustment, the positions of the junction points as well as the old points do change. This however should have been expected as the proposed approach was simply the dynamic densification approach.

Cooper [1987] indicated the necessity to consider the control points as stochastic rather than non-stochastic fixed entities. In his work, the result of *dynamic* approach is that the control point parameters change as a result of the estimation of new points in the geodetic system. This introduces the anomaly of having two sets of parameters for the national control point and so *Cooper [1987]* recommended a re-estimation of parameters and stochasticity of all points in the geodetic system, not just of the new points.

Illner [1988] considered the hierarchical densification of geodetic systems and proposed models for *dynamic*, *static* and *hybrid* approaches to densification

In his study, *Lugoe [1990]* discussed approaches to densification of geometrically strong and geometrically weak geodetic systems and also considered the simultaneous densification and integration. He observed this as being a statistically viable approach as pertaining to densification and integration together.

Aduol [1993] suggested the *static-dynamic* approach to densification, which he then compared to the *static* and *dynamic* approaches to densification of geodetic systems. From the analysis of the respective variance-covariance matrices, strong theoretical and practical qualities of the *static-dynamic* approach against the fully *static* and *dynamic* approaches to densification are demonstrated. The results are based on a simulated network adjustment and he recommended a similar study on a real network to ascertain the results.

Furthering the study carried out by Aduol [1993], Miima [1997] states: "There are basically four densification approaches which have been proposed. The main distinction in the models is

dependent on how the coordinates of the higher control stations are treated during densification". Miima [1997] considered densification under static, dynamic and static-dynamic approaches of a real two-dimensional geodetic system comprising 15 secondary and 22 tertiary points built on a control system defined by 8 primary points. The resulting parameters, standard errors and standard error ellipses were compared. Analysis of the results indicated that the static-dynamic approache gives more realistic estimates than the static and dynamic approaches. which was in agreement with the results of the study carried out by Aduol [1993].

Schaffrin [1997] noted that the static approach in which the control point parameters are considered fixed, non-stochastic, constraints will rarely be optimal among all possible hierarchical data fusion methods that ought to keep the so called "reference information unchanged". He derived the "optimal reproducing estimator" in the context of geodetic network densification by employing non-Bayesian techniques. Hierarchical estimators have, in contrast, been proposed by Berliner [1996] for time series and by Wilke et al. [1998] for time-space models [Schaffrin and Cothren, 1999].

Schaffrin and Cothren, [1999] noted the need for stability of the reference data that are meant to provide information of such high quality. To avoid their change during the densification process, they outlined a strictly *hierarchical* method in which the estimation procedure is designed to reproduce everything that belongs to a "higher category" and perform an adjustment in the least-squares sense on everything else in the geodetic system. The technique is then compared to the traditional approach based on Helmert's transformation and the non-hierarchical approach through the integration of photogrammetric geodetic systems of substantially different scales. The result of their study indicated that the traditional approach based on Helmert's transformation and the non-hierarchical approach through the integration of photogrammetric geodetic systems of substantially different scales. The result of their study indicated that the traditional approach based on Helmert's transformation approach based on Helmert's transformation is non-optimal (in the sense of minimum mean-square error). They also realized that in the *hierarchical* approach, the reference points involved remain unchanged and that the *optimal* method provides the same result for the new points as the *non-hierarchical* approach except for slightly enlarged variance component estimates.

In comparing the free net adjustment, followed by *Helmert transformation* to the *sub-optimal fusion* approach. *Schaffrin [2000]* realized that the latter approach is superior over the former in terms of the Mean-Squared-Error (MSE) risk.

1.5 Organization of the Report

The report is organized into eight chapters. In Chapter Two, linear estimation methods relevant to the study are discussed. In Chapter Three, the densification techniques, both reproducing and non-reproducing, are presented. The general experimental design and the geodetic test networks on which the densification techniques are applied are presented in Chapter Four. Chapter Five outlines the test results of the computations obtained from the four experiments carried out in the study. Analysis of the results is contained in Chapter Six. Discussions are contained in Chapter Eight.

ESTIMATION METHODS

The data collected from experiments and surveys are normally analyzed and then used to estimate essential parameters using relevant estimation techniques. Though estimation techniques are used so extensively in the theory and application of geodetic densification approaches, it is impossible in this report to discuss all the techniques. This section therefore, is primarily concerned with the *Gauss-Markov model with stochastic restriction* and *free network adjustment* techniques. The techniques are briefly discussed since they are relevant to the estimation of parameters in the present study.

2.1 The Gauss-Markov Model

The simple Gauss-Markov model is the basis for the least-squares estimation technique which minimizes the sum of the squares of the residuals. The model is given as

 $E(y) = Ax, \qquad D(y) = \sigma_0^2 W^{-1}$ (2.1.1) where y is a n× vector of observational increments A is the n× coefficient matrix x is the m×1 vector of unknown parameters σ_0^2 is the (typically unknown) variance component or variance of unit weight W is the n×n positive definite weight matrix

Since y is stochastic then (2.1.1) takes the form

y = Ax + e, $e \sim (0, \sum = \sigma_0^2 W^{-1})$, \sum is positive definite

where e is a $n \times$ vector of random observation errors

 $\Sigma = D(e)$ is the corresponding $n \times n$ dispersion matrix

With the assumption that the prior information is given in the form of estimated parameters which, in turn, appear in the linearized observation equations for the estimation of the new points, we obtain the extended Gauss-Markov model as

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(2.1.2)

$$y = A_1 x_1 + A_2 x_2 + e$$

where $A := \begin{bmatrix} A_1 & A_2 \end{bmatrix}$ is the $n \times$ coefficient matrix

 x_1 is a $c \times 1$ vector of parameters with prior information

 x_{2} is a $(m-c) \times 1$ vector of parameters without prior information

With the least squares requirement that the sum of weighted squared residuals be minimum, and taking into consideration the weights of the observations, and provided the coefficient matrix A has full column rank, then the estimate of the unknown parameter x is given by

$$\bar{x} = (A'WA)^{-1}A'Wy$$
 (2.1.4)

with

$$D(x_2) = \sigma_0^2 (A'WA)^{-1}$$
(2.1.5)

and

$$\hat{\sigma}_0^2 = \frac{e \, W e}{v_0} \, , \quad \hat{e} = y - A \hat{x} \, (2.1.6)$$

Further

$$E(\hat{x}) = x \tag{2.1.7}$$

indicating that x is an unbiased estimate of x.

Estimation under the Gauss-Markov model is the only possible where the geodetic system has been freed of any datum defects since the model assumes that the resultant normal equation matrix has full rank. Therefore, any datum defects in the system must be overcome before hand.

2.2 Gauss-Markov Model with Restrictions

In the event that the coefficient matrix A is not of full column rank, we would have the case of a Gauss-Markov model with rank defect. In such case $(A'WA)^{-1}$ in (2.1.4) and (2.1.5) above would not exist. This situation arises when for instance the datum for the parameters being adjusted is incompletely defined by observations and restrictions, i.e. the observations do not cater for all the degrees of freedom in the network. *Koch [1987, p212]* states that, when observations are formed, it is necessary to add a set of restrictions, which in effect complete the definition of the datum.

A coordinate system in three-dimensional space necessitates the definition of seven degrees of freedom. If it is defined in shape, this includes one scale, three translation elements and three orientation elements. For a two-dimensional space, four elements, namely, one scale, one orientation and two translations are to be defined. The necessary and sufficient number and type of datum elements can be defined by appropriate combination of measurements. *Cooper* [1987] outlines the number and type of Cartesian coordinate datum elements for two- and three-dimensional spaces which are defined by inclusion of certain measurements in a network. Datum defects due to fewer degrees of freedom than necessary may be overcome through the incorporation of appropriate restrictions. This section discusses the variants of the Gauss-Markov model under different forms of restriction.

2.2.1 Exact Restrictions

Exact restrictions may be incorporated in the geodetic system for two main reasons; firstly, to overcome datum defects and secondly, to fulfill certain physical and geometrical conditions in the model. In general, the Gauss-Markov model with exact restrictions is set up in the form

$$y = Ax + e \tag{2.2.1}$$

(2.2.2)

and $z_0 = Kx$

with (2.2.2) as the exact restriction, in which

 z_0 is a $c \times 1$ vector of restriction parameters (non-random)

and K is a $c \times m$ restriction design matrix, rk = c

(2.2.2) may also be referred to as exact prior information [Durbin, 1953] and [Aduol, 1993].

To determine the estimate of x under the least-squares condition and further fulfilling (2.2.2), the Lagrange function L is used, along with the $c \times 1$ vector λ of Lagrange multipliers $L = e'We + 2(Kx - z_0)'\lambda$ (2.2.3)

with which, under least-squares condition the resulting normal equations take the form

$$\begin{bmatrix} A'WA & K'\\ K & 0 \end{bmatrix} \begin{bmatrix} \hat{x}\\ \hat{\lambda} \end{bmatrix} = \begin{bmatrix} A'Wy\\ z_0 \end{bmatrix}$$
(2.2.4)

Provided the model (2.2.1) and (2.2.2) is of full rank, the estimates of x and λ may be obtained as

$$\begin{bmatrix} \hat{x} \\ \hat{\lambda} \end{bmatrix} = \begin{bmatrix} A'WA & K' \\ K & 0 \end{bmatrix}^{-1} \begin{bmatrix} A'Wy \\ z_0 \end{bmatrix}$$
(2.2.5)
The inversion of the normal equations matrix may be performed through block matrix techniques, see Aduol [1999] and Schaffrin [1984].

2.2.2 Stochastic Restrictions

In this case, the rank defect in the coefficient matrix A is overcome by introducing restrictions together with their stochasticity. The stochastic restrictions are set on in the form

$$= K_x + e_0 , \quad z_0 \sim (0, \sum_z = \sigma_0^2 W_z^{-1}) , \quad C(e, e_0) = 0$$
(2.2.6)

where z_0 is a $c \times 1$ vector of restriction parameters (random),

K is a $c \times l$ restriction design matrix

 e_0 is a $c \times m$ error vector of z_0 , rk K = c,

 \sum_{z} is a $c \times c$ covariance matrix of z_0

C denote "covariance"

Taking (2.2.6) together with (2.1.3), Gauss-Markov with stochastic restrictions is expressed as

$$\begin{bmatrix} y \\ z_0 \end{bmatrix} = \begin{bmatrix} A_1 & A_2 \\ K_1 & K_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} e \\ e_0 \end{bmatrix}$$
(2.2.7)

which on taking

$$\overline{y} = \begin{bmatrix} y \\ z_0 \end{bmatrix}, \quad \overline{A} = \begin{bmatrix} A_1 & A_2 \\ K_1 & K_2 \end{bmatrix}, \quad x := \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \text{ and } \overline{e} = \begin{bmatrix} e \\ e_0 \end{bmatrix}$$
(2.2.8)

Then (2.2.7) may be written as

$$\overline{y} := \overline{A}x + \overline{e} \text{ with } \overline{e} \sim (0, \sum_{\overline{y}})$$
(2.2.9)

for
$$D(\bar{e}) = \sum_{\bar{y}} = \begin{bmatrix} \sum_{y} & 0 \\ 0 & \sum_{z} \end{bmatrix}$$
 (2.2.10)

on the assumption that y and z are independent.

From (2.2.10) the combined weight matrix \overline{W} is defined in the form

$$\overline{W} = \Sigma_{y}^{-1} = \begin{bmatrix} \Sigma_{y}^{-1} & 0\\ 0 & \Sigma_{z}^{-1} \end{bmatrix}$$
(2.2.11)

provided the inverse exists.

Under the least-squares condition we have that

$$\bar{x} = (\bar{A}'\bar{W}\bar{A})^{-1}\bar{A}\bar{W}\bar{y}$$
(2.2.12)

with
$$\hat{D}(\hat{x}) = \hat{\Sigma} = \hat{\sigma}_0^2 (\overline{A}' \overline{W} \overline{A})^{-1}$$
 (2.2.13)

where $\hat{\sigma}_0^2$ is the variance of unit weight given in the form

$$\frac{\vec{e}\cdot\vec{We}}{n+c-m} , \quad \vec{e} = \vec{y} - A\hat{x}$$
(2.2.14)

for n being the number of observations, c the number of restrictions and m the number of unknowns.

We have

$$E(\hat{x}) = (\overline{A}' \overline{W} \overline{A})^{-1} (\overline{A}' \overline{W} \overline{A}) x = x$$
(2.2.15)

thus demonstrating that \hat{x} is an unbiased estimate of x.

Densification of a geodetic system may be performed under stochastic restrictions where some of the unknown parameters in the system are known a priori with their stochasticity. In such a case, the unknowns may be incorporated into the estimation model as stochastic prior information through the *Gauss-Markov model with stochastic restrictions*.

In the case where restrictions are introduced only to overcome datum defects and define the reference system, we have a minimally constrained model [Mikhail, 1976]. [Koch, 1987]. Where restrictions are more than, but involve, those needed to overcome datum defects, we have an over-constrained model [Aduol, 1999]. Under the over-constrained models, it may happen that the simple Gauss-Markov model has full rank, in such a case it is called over-constrained with full rank. However, if the simple Gauss-Markov model has a rank defect, such that among the restrictions, some go towards overcoming the rank defects, it is referred to as over-constrained with rank defect.

2.3 The Free Network Adjustment Technique

Free network adjustment is the technique in which the geodetic system is defined over exact restrictions without however considering any particular parameter (unknown or observable) as fixed. Such a geodetic system is considered free, in that, its geometrical size and shape is determined while remaining essentially independent of the control points.

In free network adjustment, the restriction design matrix in (2.2.2) must be chosen in such a way that the restrictions overcome the rank defect. Such a matrix K will be one whose columns are made up of the normalized eigenvectors of those eigenvalues in the normal equation matrix N = A'WA (2.3.1)

which have values equal to zero, due to the rank defect in N. If we denote the special form of K as G', then due to its special form

$$NG = 0 \tag{2.3.2}$$

and
$$G'G = D$$
, D diagonal (2.3.3)

since the columns of G are eigenvectors orthogonal to each other.

Specifically in the free network adjustment, the geodetic system datum is defined over all the approximate values computed to an arbitrary datum. This concept is referred to as "inner solution" and gives unique results. The "inner solution" is the minimum norm in least-squares condition of the singular equations:

$$e'We \Rightarrow \min$$
 (2.3.4a)
 $r'r \Rightarrow \min$ (2.3.4b)

yielding
$$tr(O_{rr}) \Rightarrow \min$$
 (2.3.4c)

These are the generalized inner constraints with (2.3.4a) as the basic least-squares condition, (2.3.4b) as the scale control that minimizes deviation of the final geodetic values from the approximate values and (2.3.4c) as the inner accuracy that ensures that the accuracy of the estimated values is the best possible [Schmitt, 1982].

For a two-dimensional geodetic system in which only angles have been observed, the corresponding restriction design matrix for n points is given in the form

| | 1 | 0 | 1 | 0 | • | 1 | 0] |
|------|-------|-----------------|-------|----------|---|-----------------|-----------------------|
| G' = | 0 | 1 | 0 | 1 | | 0 | 1 |
| | y_1 | $-x_1$ | y_2 | $-x_{2}$ | | \mathcal{Y}_n | $-x_n$ |
| | _x, | \mathcal{Y}_1 | x_2 | y_2 | • | x_n | <i>y</i> _n |

For conditions (2.3.4) to be fulfilled, it turns out that the restriction equation (2.2.2) with G as already specified above, in fact becomes

If we take approximate values of x_i and y_i as x'_i and y'_i such that

$$x_{i} = x'_{i} + \Delta x_{i}, \quad y_{i} = y'_{i} + \Delta y$$
 (2.3.7)

then we note from (2.3.5) and (2.3.6) that, the rows in G' respectively establish the condition that

(i)
$$\sum_{i=1}^{n} \Delta x_i = 0$$
 (2.3.8a)

(ii)
$$\sum_{i=1}^{n} \Delta y_i = 0$$
 (2.3.8b)

(iii)
$$\sum_{i=1}^{n} (x_i \Delta y_i - y_i \Delta x_i) = 0$$
 (2.3.8c)

(iv)
$$\sum_{i=1}^{n} (x_i \Delta x_i + y_i \Delta y_i) = 0$$
 (2.3.8d)

Conditions (i) and (ii) go towards overcoming translation defects by ensuring that the centre of mass of the geodetic system is maintained at that defined by the approximate values. Condition (iii) is to overcome the rotation defect, by ensuring that the directions in the geodetic system are each changed by as minimum a value as possible, while condition (iv) overcome the scale defect by changing the scale as defined by the approximate values as little as possible.

The restriction design matrix is applied to the normal equations in the form

 $\overline{N} = A'W, A + GG' \tag{2.3.9}$

from which obtain

$$F_{11} = \overline{N}^{-1} - \overline{N}^{-1} G G' \overline{N}^{-1}$$

$$F_{12} = \overline{N}^{-1} G$$

$$F_{21} = G' \overline{N}^{-1}$$

$$F_{22} = 0$$

$$(2.3.10a)$$

$$(2.3.10b)$$

$$(2.3.10c)$$

$$(2.3.10d)$$

which gives the estimates of the unknowns as

$$\begin{aligned} x &= F_{11}A'W_{y}y + F_{12}Z_{0} \\ &= F_{11}A'W_{y}y \quad for \quad Z_{0} = 0 \quad , \end{aligned}$$
 (2.3.11)

and

$$\bar{D}(\bar{x}) = \hat{\sigma}_0^2 \bar{N}^{-1} A' W_{\gamma} A \bar{N}^{-1} = \hat{\sigma}_0^2 F_{11}$$
(2.3.12)

The result of such a free network adjustment is the consistency and thus the internal precision of the geodetic system that may be checked free of external influences associated with attaching a geodetic system to an absolute control system. This makes the free network adjustment best suited for adjustment of control geodetic systems, as it results in fairly representative estimates of the systems parameters with uniformly distributed accuracies.

Various forms of the restriction matrix, depending on different observation combinations, are listed by *Illner [1985]*. Since the normal equation in (2.3.1) is singular, the free network problem can be viewed as principally overcoming this rank defect. Several approaches to the solution of N are considered in detail by, among others, *Mittermayer [19^{-2]}*, *Pope [1973]*, *Grafarend and Schaffrin [1974]*, *Brunner [1979]*, and Meissl [1982].

GEODETIC DENSIFICATION TECHNIQUES

3.1 Introduction

From the statistical point of view, the classical least-squares adjustment is a procedure to estimate free unknowns and residuals. It is also possible, and usual, to estimate additional parameters, for example the variance of unit weight of the observations to obtain a statement of its accuracy. The problem arises where heterogeneous geodetic observations are to be used together in an adjustment model, for example, in densification, where there are distances and directions observed. Additional problem to this is, to estimate the weight relation between those various observations so as to obtain the accuracy of the various groups of observations in their relation or even correlation. The attempt to solve this task led to the proposal of several densification approaches.

In this chapter, the various approaches to densification are discussed. They are grouped into either reproducing or non-reproducing depending on whether the datum points are affected or not, when the heterogeneous data sets are fused.

3.2 Non-Reproducing Densification Techniques

Densification approaches that do not preserve the control point parameters together with their variance-covariance matrices (respectively do not reproduce every "reference information" that belongs to a "higher category" together with their stochasticity) are termed non-reproducing densification techniques. The two most commonly used approaches in this category, namely the *Static* and the *Dynamic* approaches, are presented in this section based on the works of *Aduol* [1993,1999].

3.2.1 The Static Densification Approach

The basic concept of this approach to densification is based on the Gauss-Markov model. The Gauss-Markov model with stochastic restrictions is given in (2.1.3) and (2.2.6) as

$$y = A_1 x_1 + A_2 x_2 + e ag{3.2.1a}$$

$$z_0 = Kx + e_0$$
 (3.2.1b)

In the static densification approach, the datum parameters contained in x_1 are treated as exact prior information thus the representation in (3.2.1b) then becomes

$$z_0 = Kx \quad e_0 = 0, \quad e_0 \sim (0,0) \tag{3.2.2}$$

The full parameter estimation model then becomes

$$y = A_1 x_1 + A_2 x_2 + e \quad e \sim (0, \sigma_{0y}^{2} W_y^{-1}) = (0, \Sigma_{yy})$$
(3.2.3a)

$$z_0 = K_1 x_1 - K_2 x_2 \tag{3.2.3b}$$

Under the least-squares condition, the normal equations for the set up take the form

$$\begin{bmatrix} A_1'W_y A_1 & A_1'W_y A_2 & K_1' \\ A_2'W_y A_1 & A_2'W_y A_2 & K_2' \\ K_1 & K_2 & 0 \end{bmatrix} \begin{bmatrix} \hat{x}_1 \\ \hat{x}_2 \\ \hat{\lambda} \end{bmatrix} = \begin{bmatrix} A_1'W_y y \\ A_2'W_y y \\ Z_0 \end{bmatrix}$$
(3.2.4)

where λ is the vector of Lagrange multipliers. From this we obtain the estimate x of x is as

$$\bar{x} = (N_r^{-1} - N_r^{-1} K' R_r^{-1} K N_r^{-1}) A' W + N_r^{-1} K' R_r^{-1} z_0$$
(3.2.5a)

for
$$N_r := A' W_r A + K' K$$
 and $R_r := K N_r^{-1} K'$ (3.2.5b)

with
$$A:= \begin{bmatrix} A_1 & A_2 \end{bmatrix}$$
 and $K:= \begin{bmatrix} K_1 & K_2 \end{bmatrix}$ (3.2.5c)

Also the estimate dispersion matrix $D(\hat{x})$ is given as

$$D(\hat{x}) = \hat{\Sigma} = \hat{\sigma}_0^2 (N_r^{-1} - N_r^{-1} K' R_r^{-1} K N_r^{-1}) N(N_r^{-1} - N_r^{-1} K' R_r^{-1} K N_r^{-1})$$
(3.2.6a)

$$= \hat{\sigma}_{0}^{2} (N_{r}^{-1} - N_{r}^{-1} K' R_{r}^{-1} K N_{r}^{-1})$$
(3.2.6b)

with
$$\hat{\sigma}_{0}^{2} = \frac{\hat{e}' W_{y} \hat{e}}{n+c-m}$$
, $\hat{e} = y - A\hat{x}$ (3.2.7)

In the special case that K_1 is non-singular and $K_2 = 0$, we should have from (3.2.3b) that

$$x_1 = K_1^{-1} z_0 \tag{3.2.8}$$

and with (3.2.3a) we obtain that

$$y - A_1 K_1^{-1} z_0 = A_2 x_2 + e \tag{3.2.9}$$

If in this we set $\zeta = y - A_1 K_1^{-1} z_0 \qquad (3.2.10)$

then (3.2.9) becomes a simple Gauss-Markov model in the form

$$\zeta = A_2 x_2 + e \quad e \sim (0, \sigma_0^2 W_y^{-1}) = (0, \Sigma_{yy}) = (0, \Sigma_{\zeta\zeta})$$
(3.2.11)

In which we now have only the unknown sub-vector x_2 appearing and $\Sigma_{\zeta\zeta} = D(\zeta)$.

In practice we normally have the exact prior information of (3.2.3b) comprising only the control point parameters so that the vector x_1 contains only the control point parameters. If we let the exact prior information values of x_1 be ζ_1 , then (3.2.3b) becomes simply

$$\zeta_1 = x_1$$
 (3.2.12)

being equivalent to taking $z_0 = \zeta_1$ and $K = I_1$; where I_1 is the $c \times c$ identity matrix. With this we now have that

$$\zeta = y - A_1 \zeta_1 \tag{3.2.13}$$

From (3.2.11) the estimate x_2 of x_2 is obtained in the form

$$\hat{x}_{2} = (A_{2}^{\prime}W_{\nu}A_{2})^{-1}A_{2}^{\prime}W_{\nu}\zeta$$
(3.2.14a)

with
$$\hat{D}(x) = \hat{\sigma}_0^2 (A_2^{\prime} W_x A_2)^{-1}$$
 (3.2.14b)

for
$$\hat{\sigma}_0^2 = \frac{\hat{e}' W_1 \hat{e}}{n - m_2}$$
, $m_2 = m - c$ (3.2.14c)

It is usual in geodetic computations to start off a parameter estimation process from approximate values of the parameters, normally for linearization purposes. Moreover even in linear models, approximate values are still normally adopted for ease of numerical reasons for example as in levelling. In such cases we could have that

$$x_1 = x_{01} + \Delta x_1$$
 and $x_2 = x_{02} + \Delta x_2$ (3.2.15)

In which x_{01} and x_{02} are the approximate values to x_1 and x_2 respectively. In such situation (3.2.1) takes the form

$$\overline{y} = y - A_1 x_{01} - A_2 x_{02} = A_1 \Delta x_1 + A_2 \Delta x_2 + e \quad e \sim (0, \sigma_0^2 W_v^{-1})$$
(3.2.16a)

and
$$z_0 = K \Delta x + e_0 = Z_0 - K_1 x_{01} - K_2 x_{02}$$
, $e_0 \sim (0, \Sigma_{ZZ})$ (3.2.16b)

Since the unknown parameters to be estimated are now Δx_1 and Δx_2 from which the estimates of x_1 and x_2 may then be obtained through (3.2.15); and correspondingly (3.2.3b) and (3.2.8) would become

$$\vec{z}_{0} = K_{1}\Delta x_{1} + K_{2}\Delta x_{2} \quad and \quad \Delta x_{1} = K_{1}^{-1}\vec{z}_{0}$$
(3.2.17)
If in (3.2.15) we take $x_{1} = x_{01}$, then in (3.2.17) we have that
 $\Delta x_{1} = K_{1}^{-1}\hat{z}_{0} = 0$
(3.2.18)
And following into this we have that (3.2.16) becomes
 $\vec{y} = A_{2}\Delta x_{2} + e_{2} e^{-(0,\sigma_{0y}^{2}W_{y}^{-1})}$ (3.2.19)
which is similar to (3.2.11).
From this we obtain the usual estimates
 $\Delta \bar{x}_{2} = (A_{2}^{*}W_{y}A_{2})^{-1}A_{2}^{*}W_{y}\bar{y}$ (3.2.20a)
 $\hat{D}(\Delta x_{2}) = \hat{\sigma}_{0}^{2}(A_{2}^{*}W_{y}A_{2})^{-1}$ (3.2.20b)
and $\hat{\sigma}_{0}^{2} = \frac{\hat{e}^{*}W_{y}\hat{e}}{n-m_{2}}$, $\hat{e} = \hat{y} - A_{2}\Delta \hat{x}_{2}$, $m_{2} = m - c$ (3.2.20c)

This is the form of parameter estimation often adopted in the static densification of geodetic systems.

Even though this approach reproduces the control point parameters exactly, in the context of this study, it is termed a non-reproducing technique since the approach ignores the stochasticity of the parameters and thus does not reproduce the prior information variance-covariance matrix. This implicit omission is not justified as the control point parameters themselves could probably have been obtained earlier through an adjustment process and have a variance-covariance matrix associated with them. The effect of neglecting the variance-covariance matrix is considered in depth by *Wolf [1983]*.

3.2.2 The Dynamic Densification Approach

The dynamic densification approach is based on the use of stochastic restrictions within the framework of the model suggested by *J. Durbin* [1953] as represented in (2.2.7). that is

$$y = A_1 x_1 + A_2 x_2 + e, \quad e \sim (0, \sigma_{ov}^2 W_y^{-1}) = (0, \Sigma_{vv})$$
(3.2.21a)

$$z_0 = K_1 x_1 + K_2 x_2 + e_0, \qquad e_0 \sim (0, \sigma_{\omega Z}^2 W_Z^{-1}) = (0, \Sigma_{ZZ}) \quad , \quad c(e_1 \, e_2) = 0$$
(3.2.21b)

from which it may be written as

$$\begin{bmatrix} y \\ z_0 \end{bmatrix} = \begin{bmatrix} A_1 & A_2 \\ K_1 & K_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} e \\ e_0 \end{bmatrix}$$
(3.2.22)

$$y_{\varsigma} = \begin{bmatrix} y \\ z_0 \end{bmatrix}; \quad A_{\varsigma} = \begin{bmatrix} A_1 & A_2 \\ K_1 & 0 \end{bmatrix}; \quad x_{\varsigma} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}; \quad e_{\varsigma} = \begin{bmatrix} e \\ e_0 \end{bmatrix}$$
(3.2.23)

We have that

$$y_{\varsigma} = A_{\varsigma} x_{\varsigma} + e_{\varsigma} \quad e_{\varsigma} \sim (0, \sigma_{oy}^{2} W_{y}^{-1})$$
(3.2.24)

In which, on the assumption that y and Z_0 are independent, we shall now be having

$$E(e_{\varphi}) = 0, \quad D(e_{\varphi}) = \begin{bmatrix} \sigma_{oy}^{2} W_{y}^{-1} & 0\\ 0 & \sigma_{oz}^{2} W_{z}^{-1} \end{bmatrix} = \Sigma_{\varphi\varphi}$$
(3.2.25)

The corresponding weight matrix W_{μ} is given as

$$W_{\varsigma} = \begin{bmatrix} \sigma_{a\rho}^2 W_{\nu} & 0\\ 0 & \sigma_{az}^2 W_z \end{bmatrix} = \Sigma_{\varsigma\varsigma}^{-1}$$
(3.2.26)

This is the mixed estimation of *Theil and Goldberger [1961]*. From this with the definition $A = \begin{bmatrix} A_1 & A_2 \end{bmatrix}$, $K = \begin{bmatrix} K_1 & 0 \end{bmatrix}$, we have that

$$x = (A'_{*}W_{*}A_{*})^{-1}A'_{*}W_{*}v$$
(3.2.27a)

$$= (A' \Sigma_{yy}^{-1} A + K' \Sigma_{zz}^{-1} K)^{-1} (A' \Sigma_{yy}^{-1} y + K' \Sigma_{zz}^{-1} z_{0})$$
(3.2.27b)

with

$$D(\bar{x}) = (A' \Sigma_{yy}^{-1} A + K' \Sigma_{zz}^{-1} K)^{-1} = \Sigma_{\bar{x}\bar{x}}$$
(3.2.28)

and

$$\hat{\sigma}_{0y}^{2} = \frac{\hat{e}' W_{y} \hat{e}}{trace(W_{y} Q_{e} Q_{e})}$$
(3.2.29a)

$$\hat{\sigma}_{0z}^{2} = \frac{\hat{e}_{0}'W_{z}\hat{e}_{0}}{trace(W_{z}Q_{e_{0}}Q_{e_{0}})}$$
(3.2.29b)

In which

$$Q_{e_0}Q_{e_0} = Q_{zz} - KQ_{zz} - KQ_{zz} - K(A'W_{zz} - M_z)^{-1} - K(A'W_{zz} - K)^{-1} K' = \sigma_{0z}^{-2}D(\hat{e}_0) = \sigma_{0z}^{-2}(\sum_{zz} - K\sum_{xx} K')$$
(3.2.30a)

$$Q_e Q_e = Q_{yy} - A Q_{xx} A' - W_y^{-1} - A (A' W_{yy}^{-1} A' = \sigma_{0y}^{-2} D(\hat{e}) = \sigma_{0y}^{-2} (\sum_{xx} - A \sum_{xx} A')$$
(3.2.30b)

$$e = Q_{c}Q_{e}W_{y}y$$
 [cf. Mikhail 1976] (3.2.31a)

$$e_0 = Q_{e_0} Q_{e_1} W_Z z_0$$
 (3.2.31b)

Researchers have proved that the dynamic approach to densification is statistically a better approach as compared to the static approach since the stochasticity of the control point parameters are considered in the densification of the geodetic systems thus providing a more realistic estimation. However, this approach results in change of the control point parameters "dynamically" in principle with every single measurement added to the geodetic system. As a result the concept of a national reference system loses meaning.

3.3 Reproducing Densification Techniques

Contrary to non-reproducing densification techniques, densification approaches that preserve the control point parameters together with their variance covariance matrices (respectively reproduce the parametric and stochastic fiducial constraints) are termed reproducing densification techniques. In this section, two such approaches are discussed namely; *Static-Dynamic* and *Sub-Optimal fusion*.

3.3.1 Static-Dynamic Approach

From (2.2.6) we have the parametric and stochastic fiducial constraints given as

$$z_0 = K x_1 + e_0 - e_0 \sim (0, \sigma_{0z}^2 W_z^{-1}) \cdot C(e, e_0) = 0$$
(3.3.1)

From equation (3.3.1) we have that if K such that K^{-1} exist then:

$$x_1 = K^{-1}(z_0 - e_0) \tag{3.3.2}$$

replacing (3.3.2) into 3.3.1) we obtain that

$$y = A_1 K^{-1} (z_0 - e_0) + A_2 x_2 + e \quad e \sim (0, \sigma_{0y}^2 W_3^{-1})$$
(3.3.3)

which we may rewrite as

$$y - A_1 K^{-1} z_0 = A_2 x_2 + e - A_1 K^{-1} e_0$$
(3.3.4)

On taking

$$\bar{y} = y - A_1 K^{-1} z_0$$
 and $\bar{e} = e - A_1 K^{-1} e_0$ (3.3.5)

(3.3.4) then becomes

$$\overline{y} = A_2 x_2 + \overline{e} \cdot \overline{e} \sim (0, \sigma_0^2 \Sigma_{\overline{yy}})$$
(3.3.6)

and

$$D(\overline{e}) = \sigma_{0y}^2 W_y^{-1} + A_1 K^{-1} \Sigma_{zz} (A_1 K^{-1})' = \Sigma_{\overline{yy}}$$
(3.3.7)

On using least-squares condition we obtain x_2 estimate of x_2 as

1

$$\hat{x}_{2} = (A_{2}^{\prime} \Sigma_{\overline{y}\overline{y}} A_{2})^{-1} A_{2} \Sigma_{\overline{y}\overline{y}}^{-1} \overline{y}$$
(3.3.8)

and

$$D(x_2) = (A_2 \Sigma_{yy} A_2)^{-1}$$
(3.3.9)

$$D(\hat{x}_2) = (A'_2 \Sigma_{\overline{y}} A_2)^{-1}$$
(3.3.9)

Now, in densification where only the coordinates of the datum points have been collected in x_1 , we notice that we shall have $K_1 = I$, i.e an identity matrix of the same dimension as K_1 .

Then, from (3.3.8) and (3.3.9) we would now have that

$$\hat{x}_{2} = \left[A_{2}'(\sigma_{0y}^{2}W_{y}^{-1} + A_{1}\Sigma_{ZZ}A_{1}')^{-1}A_{2}\right]^{-1}A_{2}'(\sigma_{0y}^{2}W_{y}^{-1} + A_{1}\Sigma_{ZZ}A_{1}')^{-1}(y - A_{1}z_{0})$$
(3.3.10)

$$D(\hat{x}_2) = \left[A_2'(\sigma_{0y}^2 W_y^{-1} + A_1 \Sigma_{ZZ} A_1')^{-1} A_2\right]^{-1}$$
(3.3.11)

We note that with this model, we are able to estimate densification parameters x_2 by incorporating control point parameters x_1 as stochastic prior information while at the same time keeping x_1 numerically unchanged. This combines the properties of both the static and dynamic models. *Theil* [1963,1971] refers to this model as *estimation with incomplete prior information while Toutenburg* [1975], Bibby and Toutenburg [1977] and Toutenburg [1977] refer to it as stepwise regression.

3.3.2 Sub-Optimal Fusion Approach

Another approach to densification is the *sub-optimal network fusion model* discussed by *Schaffrin [1998]* in which the best linear uniformly unbiased estimate \bar{x} with the reproducing property is determined. We set the restriction

$$K\bar{x} = z_0 \qquad D(K\bar{x}) = \sigma_{0Z}^2 W_Z^{-1}$$
 (3.3.12)

This estimator has the linear property that

$$\bar{x} = L_1 y + L_2 z_0 \tag{3.3.13}$$

With L_1 and L_2 as the unknowns to be determined. The estimator is also uniformly unbiased in that

$$x = E(\overline{x}) = L_1 A x + L_2 K x \quad \text{for all } x \in \Re^m$$
(3.3.14a)

which implies

$$L_1 A + L_2 K - I_m = 0 ag{3.3.14b}$$

The model also has the reproducing property in that

$$0 = K\bar{x} - z_0 = (KL_1) \cdot y + (KL_2 - I_1) \cdot z_0 \text{ for arbitrary } y \in \Re^n, z_0 \in \Re^l$$
(3.3.15)

$$K L_{1} = 0$$
 L_{1} and thus with (3.3.14b) $A'L'_{1}K' = 0$ (3.3.16)

The estimate \bar{x} has the best or minimum variance (Mean Square Error) given by

$$D(\bar{x}) = \sigma_{0_y}^2 (L_1 W_y^{-1} L_1') + \sigma_{0_z}^2 (L_2 W_z^{-1} L_2')$$

= $\sigma_{0_y}^2 l_1' (I_m \otimes W_y^{-1}) l_1 + \sigma_{0_z}^2 l_2' (I_m \otimes W_z^{-1}) l_2$ (3.3.17)
for $l_1 = vec L_1', \quad l_2 := vec L_2', \otimes$ denotes the Kronecker-Zehfuss Product

for $I_1 = \text{vec}(L_1)$, $I_2 = \text{vec}(L_2)$, O denotes the function

To obtain the unknowns L_1 and L_2 in the case $\sigma_{0_v}^2 = \sigma_{0_z}^2$ we set the Lagrange target functions in the form:

$$\phi[l_{1} = \operatorname{vec} L_{1}', l_{2} = \operatorname{vec} L_{2}', \lambda_{1}, \lambda_{2}] := l_{1}'(I_{m} \otimes W_{y}^{-1})l_{1} + l_{2}'(I_{m} \otimes W_{2}^{-1})l_{2} + 2\lambda_{1}'(K \otimes A')l_{1} + 2\lambda_{2}'[(I_{m} \otimes A')l_{1} + (I_{m} \otimes K')l_{2} - \operatorname{vec} I_{m}] = \operatorname{stationary} l_{1}, l_{2}, \lambda_{1}, \lambda_{2}$$

$$(3.3.18)$$

The Euler-Lagrange necessary conditions then become

$$1 = (I_m \otimes W_v^{-1}) l_1 + (K' \otimes A) \hat{\lambda}_1 + (I_m \otimes A) \hat{\lambda}_2 = 0$$
(3.3.19a)

$$\frac{1}{2} \frac{\partial \phi}{\partial t} = (I_m \otimes W_z^{-1})I_2 + (I_m \otimes K)\hat{\lambda}_2 = 0$$
(3.3.19b)

$$\frac{1}{2} \cdot \frac{\partial \phi}{\partial x} = (K \otimes A') l_1 = 0$$
(3.3.19c)

$$\frac{1}{2} \cdot \frac{\partial \theta}{\partial \lambda_2} = (I_m \otimes A') l_1 + (I_m \otimes K') l_2 - Vec \ I_m = 0$$
(3.3.19d)

Sufficient condition for the solution of the Lagrange target functions is.

$$\frac{1}{2} \cdot \frac{\partial^2 \partial}{\partial \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}} = \begin{bmatrix} I_m \otimes W_v^{-1} & 0 \\ 0 & I_m \otimes W_z^{-1} \end{bmatrix} \text{ is positive definite}$$

Using the Euler-Lagrange necessary conditions, from equation (3.3, 19a) we have that

$$I_1 = -(K' \otimes W_y A)\hat{\lambda}_1 - (I_m \otimes W_y A)\hat{\lambda}_2$$
(3.3.20)

Substituting (3.3.20) into (3.3.19c) we have that

$$0 = (K \otimes A')l_1 = -(KK' \otimes N)\hat{\lambda}_1 - (K \otimes N)\hat{\lambda}_2$$

$$(3.3.21)$$

From (3.3.19d) we obtain

$$\operatorname{vec} I_{m} = (I_{m} \otimes K')I_{2} - (K' \otimes N)\hat{\lambda}_{1} - (I_{m} \otimes N)\hat{\lambda}_{2}$$

$$(3.3.22)$$

which implies

$$-\lambda_{1} = \operatorname{vec} N^{-1} - (I_{m} \otimes N^{-1}K')I_{2} + (K' \otimes I_{m})\hat{\lambda}_{1}$$
(3.3.23)

Substituting (3.3.19c) into (3.3.19d) we obtain

| $(K \otimes K')l_2 = vec K'$ | (3.3.24) |
|---|-----------|
| From $(3.3.20)$ and $(3.3.23)$ we also have that | |
| $I_{1} = vec (W_{y}AN^{-1}) - [I_{m} \otimes (W_{y}AN^{-1}K')]I_{2}$ | (3.3.25) |
| From (3.3.19b) and (3.3.23) we obtain that | |
| $I_2 = -(I_m \otimes W_2 K) \hat{\lambda}_2$ | (3.3.26a) |
| $= \operatorname{vec}(W_{Z}KN^{-1}) - [I_{m} \otimes (W_{Z}KN^{-1}K')]I_{2} + (K' \otimes W_{Z}K)\hat{\lambda}_{1}$ | (3.3.26b) |
| which implies that | |
| $[I_m \otimes W_Z(W_Z^{-1} + KN^{-1}K')]l_2 = \operatorname{vec}(W_ZKN^{-1}) + (K' \otimes W_ZK)\hat{\lambda}_1$ | (3.3.26c) |
| which further reduces to | |
| $l_{z} = vec[(W_{z}^{-1} - KN^{-1}K')^{-1}KN^{-1}] + [K' \otimes (W_{z}^{-1} + KN^{-1}K')^{-1}K]\hat{\lambda}_{1}$ | (3.3.27) |
| Substituting (3.3.24) into (3.3.27) we obtain that | |
| $vec K' - vec[K'(W_{Z}^{-1} + KN^{-1}K')^{-1}KN^{-1}K'] = vec[K'(W_{Z}^{-1} + KN^{-1}K')^{-1}W_{Z}^{-1}]$ | (3.3.28a) |
| $= [KK' \otimes K'(W_{Z}^{-1} + KN^{-1}K')^{-1}K]\hat{\lambda}_{1}$ | (3.3.28b) |
| which implies | |
| $[I_1 \otimes KK'(W_2^{-1} + KN^{-1}K')^{-1}] \cdot [vec(KK'W_2)^{-1} - (I_1 \otimes K)\hat{\lambda}_1]$ | (3.3.28c) |
| and further reduces to | |
| $(I_1 \otimes K)\hat{\lambda}_1 = vec (KK'W_Z)^{-1} = vec [KK'(KK')^{-1}W_Z^{-1}(KK')^{-1}]$ | |
| $= (I_1 \otimes K) \cdot vec [K'(KK'W_ZKK')^{-1}]$ | (3.3.29) |
| substituting (3 3.29) into (3 3.27) we obtain | |
| $l_2 = vec [(W^{-1} + KN^{-1}K')^{-1}KN^{-1}] + [K' \otimes (W_Z^{-1} + KN^{-1}K')^{-1}] \cdot vec (KK'W_Z)^{-1}$ | |
| $= vec \left[(W_{Z}^{-1} - KN^{-1}K')^{-1} (KN^{-1} + W_{Z}^{-1} (KK')^{-1}K) \right] = vec L'_{2}$ | (3.3.30) |
| which implies | |
| $L_{2} = [N^{-1}K' - K'(KK')^{-1}W_{Z}^{-1}](W_{Z}^{-1} + KN^{-1}K')^{-1}$ | |
| $= [N^{-1}K'W_{Z} - K'(KK')^{-1}](I_{I} + KN^{-1}K'W_{Z})^{-1}K'(KK')^{-1}$ | |
| $= [I_m + N^{-1}KW_2K - I_m + K'(KK')^{-1}K](I_m + N^{-1}KW_2K)^{-1}K'(KK')^{-1} = \dots =$ | |
| $= K'(KK')^{-1} - [I_m - K'(KK')^{-1}K](N + K'W_ZK)^{-1}K'W_Z$ | (3.3.31) |
| Similarly substituting (3.3.30) into (3.3.25) we obtain | - |
| $l_{1} = vec (W_{y}AN^{-1}) - [I_{m} \otimes (W_{y}AN^{-1}K')] \cdot l_{2}$ | |

$$= vec (W_y AN^{-1}) - vec \{W_y AN^{-1}K'(I_1 + W_z KN^{-1}K')^{-1}[W_z KN^{-1} + (KK')^{-1}K]\}$$

$$= \operatorname{vec} \{W_{v}A(N + K'W_{z}K)^{-1}[I_{m} - K'(KK')^{-1}K]\} = \operatorname{vec} L'_{1}$$
(3.3.32)

which implies that

$$I_{1} = [I_{m} - L_{2}K)N^{-1}A'W_{y} = [I_{m} - K'(KK')^{-1}K](N + K'W_{z}K)^{-1}A'W_{y}$$

= $[I_{m} - K'(KK')^{-1}K][N^{-1} - N^{-1}K'(W_{z}^{-1} + KN^{-1}K')^{-1}KN^{-1}]A'W_{y}$ (3.3.33)

Substituting (3.3.31) and (3.3.33) into (3.3.13) we obtain the results as

$$\bar{x} = L_{1}y + L_{2}z_{0} = N^{-1}A'W_{y}y + L_{2}(z_{0} - KN^{-1}A'W_{y}y)$$

$$= \bar{x}_{u} + [N^{-1}K' + K'(KK')^{-1}W_{z}^{-1}](W_{z}^{-1} + KN^{-1}K')^{-1}(z_{0} - K\bar{x}_{u}) = \dots =$$

$$= \bar{x} + K'(KK')^{-1}(I_{1} + KN^{-1}K'W_{z})^{-1}\bar{e}_{0} = \bar{x} + K'(KK)^{-1}(z_{0} - K\bar{x}) \qquad (3.3.34)$$

and

$$D(\bar{x}) = \sigma_0^{-2} (L_1 W_1^{-1} L_1') + \sigma_0^{-2} (L_2 W_z^{-1} L_2')$$

$$= \sigma_0^{-2} (N^{-1} - L_2 K N^{-1} - N^{-1} K' L_2' + L_2 (K N^{-1} K' + W_z^{-1}) L_2'] = \dots =$$

$$= \sigma_0^{-2} [N^{-1} - N^{-1} K' (W_z^{-1} + K N^{-1} K')^{-1} K N^{-1} + K' (K K')^{-1} W_z^{-1} (W_z^{-1} + K N^{-1} K')^{-1} W_z^{-1} (K K')^{-1} K]$$

$$= D\{x\} + D\{K' (K K')^{-1} (z_0 - K x)\}$$

$$(3.3.35)$$

Further

$$E(\bar{x}) = x, \qquad z_0 - K\bar{x} = \bar{e}_0 = 0, \qquad D(K\bar{x}) = D(z_0) = \sigma_0^2 W_Z^{-1}$$
 (3.3.36)

With this approach, we note that control points keep their values while for the new points, the optimal estimates will be obtained. This generalizes (and improves) Helmert's approach.

EXPERIMENTAL DESIGN

4.1 General Experimental Design

Experimental design refers to the framework or structure of an experiment. Fisher [1960] enumerated three principles that should be followed in experimental designs; the principle of replication which requires that the experiment should be repeated more than once. the principle of randomization which requires protection against extraneous factors and the principle of local control in which the range of the variable is made as wide as possible but the causes of the variability should be measured and eliminated from the experimental errors.

There are four types of formal experimental designs; *Completely Randomized* design, *Randomized Block* design, *Latin Square* design and *Factorial* design [Kothari, 1990]. Of these, Completely Randomized design (C. R. Design) is the simplest possible design and its procedure of analysis is also easier, e.g. by analysis of variance. The essential characteristic of this design is that subjects are randomly assigned to experimental treatments (or vice versa). The design involves only two principles; viz., the principle of replication and the principle of randomization. *Kothari* [1990] described a simple randomized design using a flow chart given below:



Figure 4.1: Two group Simple Randomized design (After C. Kothari)

In this report, the real network was randomly selected from the geodetic network of Kenya while the simulated network was randomly designed so as to obtain a symmetric triangle. The experimental design can be said to be of the simple randomized experimental design

4.2 The Test Networks

To test and evaluate the densification approaches discussed in chapter three, two types of geodetic networks were adopted. For the real network, data were obtained from Survey of Kenya records consisting of initial observations for the first, second and third orders. The real first order network consisted of eleven points (as shown in Fig. 4.5). The first order network was then densified to fifteen second order points (as shown in Fig. 4.6) and the second order network was further densified to another fifteen third order points (as shown in Fig. 4.6). The data consisted of original field note observations for distances and angles and the adjusted coordinates of the network based on U.T.M projection referred to Clarke's 1880 ellipsoid on the African Arc Datum 1960. The adjusted coordinates were adopted as approximate coordinates in the present study.

A simulated two-dimensional network comprising of 15 points was also adopted for the study. The simulated first order network consisted of three points (as shown in Fig. 4.2.). The first order network was then densified to three second order points (as shown in Fig. 4.3.) and the second order network was further densified to fifteen third order points (as shown in Fig. 4.4.). The observables were horizontal directions and distances. Actual observations were simulated and coordinates of the computed points obtained in order to demonstrate as well as analyze the different densification approaches. For the fundamental network and the first level densification, the horizontal directions were assigned a standard error of ± 0.5 " while for the second and third order densification levels, the standard errors were taken to be ± 1 ". Distances were assigned a uniform standard error of ± 0.03 metres throughout.

4.2.1 The Simulated Network

4.2.1.1 First Order Network

The simulated first order network consisted of three stations as shown in Fig. (4.2) with corresponding approximate coordinates and observation data sets given in Tables (4.1) and Table (4.2) respectively. This was considered as the fundamental simulated network upon which

the first level and second level simulated network densifications were performed. The fundamental network was defined by adjusting the first order network within the framework of a free network model. The standard error of the network was taken to be ± 0.5 " based on the report by *Aduol [1981, 1993]*.

| POINT | COORDINATES | | | | |
|-------|-------------|---------|--|--|--|
| | N (m) | E (m) | | | |
| 1 | 100.000 | 100.000 | | | |
| 2 | 446.410 | 300.000 | | | |
| 3 | 100.000 | 500.000 | | | |

Table 4.1: Approximate coordinates for the simulated first order network

| I LILITO TIMI O COVET MELVINE WALKE CALD AVE MENDAW SECOND ALMAN AND AVE TO A | Table 4.2: | Observational | data sets | for the | simulated | first or | der network |
|---|------------|---------------|-----------|---------|-----------|----------|-------------|
|---|------------|---------------|-----------|---------|-----------|----------|-------------|

| Observation | | Line | | Bear | ing | Distance |
|-------------|---|------|-----|------|-------|----------|
| Number | | | 0 | 1 | AX | (m) |
| 1 | 1 | 2 | 30 | 0 | 0.00 | 400.006 |
| 2 | 1 | 3 | 90 | 0 | 10.61 | 399.991 |
| 3 | 2 | 3 | 150 | 0 | 0.00 | 399.993 |
| 4 | 2 | 1 | 209 | 59 | 53.01 | _ |
| 5 | 3 | 1 | 270 | 0 | 0.00 | _ |
| 6 | 3 | 2 | 329 | 59 | 54.99 | - |

4.2.1.2 Second Order Network

The simulated second order network consisted of three stations connected onto the simulated first order network described in section 4.2.1.1 (cf. Fig. 4.3). The corresponding observational data sets are as given in Table 4.4 while the approximate coordinates are listed in Table (4.3). In Table (4.3), the first three approximate coordinates were determined through free network adjustment of the simulated first order network. The standard error of the observations was taken to be ± 1 ".

| Table 4.3: Approximate coordinates for the simulated second order networ | Table | e 4.3 | 3: Ap | proximate | coordinates | for | the | simulated | l second | order | networ | k |
|--|-------|-------|-------|-----------|-------------|-----|-----|-----------|----------|-------|--------|---|
|--|-------|-------|-------|-----------|-------------|-----|-----|-----------|----------|-------|--------|---|

| POINT | COORDINATES | | | | | |
|-------|-------------|----------|--|--|--|--|
| | N (m) | E (m)" | | | | |
| 1 | 99.9956 | 99.9971 | | | | |
| 2 | 446.4037 | 300.0064 | | | | |
| 3 | 100.0057 | 499.9965 | | | | |
| 4 | 273.0500 | 200.0700 | | | | |
| 5 | 273.0500 | 400.0900 | | | | |
| 6 | 100.0600 | 300.0500 | | | | |



Figure 4.2: The simulated first order network

| Observation | | Line | | Bea | ring | Distance |
|-------------|---|------|-----|-----|-------|----------|
| Number | | | 0 | • | ** | (m) |
| 1 | 1 | 4 | 30 | 0 | 0.00 | 200.060 |
| 2 | 1 | 6 | 90 | 0 | 10.61 | 200.040 |
| 3 | 2 | 4 | 209 | 59 | 53.01 | 200.080 |
| 4 | 2 | 5 | 150 | 0 | 4.99 | 199.980 |
| 5 | 3 | 5 | 329 | 59 | 54.99 | 200.030 |
| 6 | 3 | 6 | 270 | 0 | 3.01 | 199.930 |
| 7 | 4 | 1 | 210 | 0 | 0.00 | - |
| 8 | 4 | 2 | 30 | 0 | 7.00 | - |
| 9 | 4 | 5 | 89 | 59 | 52.62 | 200.020 |
| 10 | 4 | 6 | 150 | 0 | 5.42 | 200.090 |
| 11 | 5 | 2 | 329 | 59 | 50.99 | - |
| 12 | 5 | 4 | 270 | 0 | 4.37 | - |
| 13 | 5 | 6 | 209 | 59 | 58.02 | 199.920 |
| 14 | 5 | 3 | 150 | 0 | 13.96 | - |
| 15 | 6 | 1 | 270 | 0 | 0.00 | - |
| 16 | 6 | 4 | 329 | 59 | 57.71 | - |
| 17 | 6 | 5 | 30 | 0 | 6.43 | - |
| 18 | 6 | 3 | 89 | 59 | 54.98 | - |

Table 4.4: Observational data sets for the simulated second order network

4.2.1.3 Third Order Network

The simulated third order network consisted of nine stations connected onto the simulated second order network described in section 4.2.1.2 (cf. Fig. 4.4). The corresponding observational data sets are as given in Table (4.6) while the approximate coordinates are given in Table (4.5a), (4.5b), (4.5c) and (4.5b). In Table (4.5a), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Static-Dynamic approach while in Table (4.5b), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Sub-Optimal Fusion approach. In Table (4.5c), all the approximate coordinates were determined through first level densification of the simulated second order network using the Dynamic approach while in Table (4.5d), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Dynamic approach while in Table (4.5d), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Dynamic approach while in Table (4.5d), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Dynamic approach while in Table (4.5d), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Dynamic approach while in Table (4.5d), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Dynamic approach while in Table (4.5d), the first six approximate coordinates were determined through first level densification of the simulated second order network using the Static approach.



Figure 4.3: The simulated second order network

| POINT | (| COORDINATES |
|-------|----------|-------------|
| | N (m) | E (m) |
| 1 | 99.9956 | 99.9971 |
| 2 | 446.4087 | 300.0064 |
| 3 | 100.0057 | 499.9965 |
| 4 | 272.8963 | 200.1378 |
| 5 | 272.8948 | 400.1745 |
| 6 | 100.1226 | 300.0987 |
| 7 | 100.0000 | 200.0000 |
| 8 | 186.6000 | 150.0000 |
| 9 | 186.6020 | 250.0000 |
| 10 | 359.8080 | 250.0000 |
| 11 | 359.8080 | 350.0000 |
| 12 | 273.2050 | 300.0000 |
| 13 | 186.6020 | 450.0000 |
| 14 | 100.0000 | 400.0000 |
| 15 | 186.6020 | 350.0000 |

Table 4.5.1: Approximate coordinates for the simulated third order network used in the Static-Dynamic densification approach

 Table 4.5.2: Approximate coordinates of the simulated third order network used in the Sub-Optimal Fusion densification approach

| uu-Opiinai i usi | on densitication approa | ion - | |
|------------------|-------------------------|----------|----|
| POINT | COORDI | NATES | |
| | 11 (m) | E (m) | |
| 1 | 99.9956 | 99.9971 | |
| 2 | 446.4087 | 300.0064 | |
| 3 | 100.0057 | 499.9965 | |
| 4 | 272.8809 | 200.1552 | |
| 5 | 272.8795 | 400.1517 | |
| 6 | 100.1419 | 300.0960 | |
| 7 | 100.0000 | 200.0000 | 11 |
| 8 | 186.6000 | 150.0000 | 6 |
| 9 | 186.6020 | 250.0000 | |
| 10 | 359.8080 | 250.0000 | |
| 11 | 359.8080 | 350.0000 | |
| 12 | 273.2050 | 300.0000 | |
| 13 | 186.6020 | 450.0000 | |
| 14 | 100.0000 | 400.0000 | |
| 15 | 186.6020 | 350.0000 | |
| | | | |

.....

| POINT | COORDINATES | | | | | | |
|-------|-------------|----------|-----|--|--|--|--|
| | N (m) | E | (m) | | | | |
| 1 | 100.0051 | 100.0179 | | | | | |
| 2 | 446.3823 | 300.0025 | | | | | |
| 3 | 100.0116 | 499.9775 | | | | | |
| 4 | 272.8809 | 200.1552 | | | | | |
| 5 | 272.8795 | 400.1517 | | | | | |
| 6 | 100.1419 | 300.0960 | | | | | |
| 7 | 100.0000 | 200.0000 | | | | | |
| 8 | 186.6000 | 150.0000 | | | | | |
| 9 | 186.6020 | 250.0000 | | | | | |
| 10 | 359.8080 | 250.0000 | | | | | |
| 11 | 359.8080 | 350.0000 | | | | | |
| 12 | 273.2050 | 300.0000 | | | | | |
| 13 | 186.6020 | 450.0000 | | | | | |
| 14 | 100.0000 | 400.0000 | | | | | |
| 15 | 186.6020 | 350.0000 | | | | | |

Table 4.5.3: Approximate coordinates of the simulated third order network used in the Dynamic densification approach

 Table 4.5.4: Approximate coordinates for the simulated third order network used in the Static densification approach

| POINT | CC | ORDINATES |
|-------|----------|-----------|
| | N m) | E (m) |
| 1 | 99.9956 | 99.9971 |
| 2 | 446.4087 | 300.0064 |
| 3 | 100.0057 | 499.9965 |
| 4 | 272.9269 | 200.1238 |
| 5 | 272.9257 | 400.1571 |
| б | 100.1099 | 300.0885 |
| 7 | 100.0000 | 200.0000 |
| 8 | 186.6000 | 150.0000 |
| 9 | 186.6020 | 250.0000 |
| 10 | 359.8080 | 250.0000 |
| 11 | 359.8080 | 350.0000 |
| 12 | 273.2050 | 300.0000 |
| 13 | 186.6020 | 450.0000 |
| 14 | 100.0000 | 400.0000 |
| 15 | 186.6020 | 350.0000 |

Table 4.6: Observational data sets for the simulated third order network

| Observation | | Line | | Beari | ng | Distance |
|-------------|---|------|-----|-------|-------|----------|
| Number | | | 0 | ` | 11 | (m) |
| 1 | 1 | 8 | 29 | 59 | 54.90 | 100.060 |
| 2 | 1 | 7 | 89 | 59 | 53.00 | 100.040 |
| 3 | 2 | 10 | 209 | 59 | 57.01 | 100.080 |
| 4 | 2 | 11 | 149 | 59 | 58.00 | 99.980 |
| 5 | 3 | 13 | 330 | 0 | 0.00 | 100.030 |
| 6 | 3 | 14 | 269 | 59 | 52.01 | 99.930 |
| 7 | 4 | 8 | 209 | 59 | 53.00 | 100.020 |



Figure 4.4: The simulated third order network

Table 4.6: Continued

| Number (m) | |
|---|-----|
| · · · · · · · · · · · · · · · · · · · | |
| | |
| | |
| <u>4</u> <u>12</u> <u>90</u> <u>0</u> <u>2.62</u> <u>99.970</u> | |
| 10 4 10 30 0 8.42 100.030 | |
| 11 5 11 330 0 2.90 99.890 | |
| 12 5 12 269 59 54.37 100.080 | |
| 13 5 15 210 0 5.02 99.940 | |
| 14 5 13 150 0 3.96 99.990 | |
| 15 6 7 270 0 9.00 99.980 | |
| 16 9 329 59 54.71 99.930 | |
| 17 6 15 30 0 6.43 100.020 | |
| 18 6 14 90 0 1.98 100.030 | |
| 19 7 1 270 0 0.00 - | |
| 20 7 8 330 0 10.00 - | |
| 21 7 9 29 59 51.00 99.970 | |
| 22 7 6 89 59 57.00 - | |
| 23 8 1 210 0 0.00 - | |
| 24 8 7 150 0 0.10 100.000 | |
| 25 8 9 90 0 0.10 100.060 | |
| 26 8 4 29 59 57.90 - | |
| 27 9 4 330 0 0.00 - | |
| 28 9 12 29 59 53.00 100.040 | |
| 29 9 15 89 59 55.00 100.010 | |
| 30 9 6 150 0 10.90 - | |
| 31 9 7 209 59 59.00 - | |
| 32 9 8 270 0 5.00 - | |
| 33 10 2 29 59 55.00 - | |
| 34 10 4 209 59 57.00 - | |
| 35 10 12 149 59 50.00 - | |
| 36 10 11 90 0 5.00 100.000 | |
| 37 11 2 330 0 1.00 - | |
| 38 11 10 269 59 54.00 - | |
| 39 11 12 209 59 54.00 - | |
| 40 11 5 150 0 1.00 - | |
| 41 12 9 210 0 0.00 - | 6.0 |
| 42 12 4 269 59 52.00 - | X |
| 43 12 10 330 0 0.00 100.060 | 100 |
| 44 12 11 30 0 0.00 99.980 | |
| | |
| 46 12 15 149 59 55.00 99.970 | |
| 47 13 5 330 0 7.00 - | |
| 48 13 15 269 59 58.00 - | |
| 49 13 14 209 59 58.00 99.960 | |
| 50 13 3 149 59 53 00 - | |
| | |
| | |
| 53 14 15 329 59 59 00 - | |
| 54 14 13 29 59 50.00 | |
| 55 15 5 20 50 50 00 - | |
| 56 15 12 220 0 2.00 | |
| 57 15 9 269 59 55 90 - | |
| 58 15 6 210 0 2.00 | |
| 59 15 14 150 0 4.00 100.050 | |
| 60 15 13 89 59 50 10 100.030 | |

4.2.2 The Real Network

4.2.2.1 First Order Network

The real first order network consisted of eleven stations as shown in Fig. (4.5) with corresponding approximate coo2dinates and observation data sets given in Tables (4.7) and Table (4.8) respectively. This was considered the fundamental real network upon which the real first level and real second level network densifications were performed. The fundamental network was defined by adjusting the real first order network within the framework of free network model. In the study, all the eleven points were considered approximate and the adjustment done assuming that the measurements were of first order precision with the standard error of the directions taken as ± 0.5 ". This was based on a variety of experiences from various studies and field surveys e.g. *Miima* [1997], *Musyoka* [1993] and Aduol [1981].

| Point | S.K | S.K | Coordi | nates |
|-------|------|-------------|-------------|---------------------|
| | Code | Name | N (m) | E (m) |
| 1 | Sk56 | TARU | 9583105.104 | 513215.911 |
| 2 | SK60 | JIBANA | 9576179.214 | 574648.574 |
| 3 | SK61 | KABANINI | 9600981.179 | 569580.645 |
| 4 | SK62 | KILIFI | 9599052.465 | 594885.489 |
| 5 | SK63 | SOKOKE | 9611665.689 | 589503.327 |
| 6 | SK64 | KILIMANJARO | 9624778.596 | 606329.877 |
| 7 | SK65 | MANGEA | 9640229.659 | 580182.061 |
| 8 | SK66 | KIKUYUNI | 9644287.319 | 609203.330 |
| 9 | SK67 | KOYENI | 9661267.194 | 585576.660 |
| 10 | SK68 | BORE | 9660984.693 | 598816.071 |
| 11 | SK69 | MAGARINI | 9661696.939 | \$2 8181.173 |

Table 4.7: Approximate coordinates for the real first order network

Table 4.8: Observational data sets for the real first order network

| Observation | Li | ne | | Beari | ng | Distance |
|-------------|----|----|-----|-------|------|-----------|
| Number | | | 0 | ١ | 11 | (m) |
| 1 | 1 | 2 | 96 | 25 | 56.3 | 61821.778 |
| 2 | 1 | 3 | 72 | 24 | 12.7 | 59131.496 |
| 3 | 1 | 7 | 49 | 32 | 4.6 | 88020944 |
| 4 | 2 | 1 | 276 | 25 | 56.5 | - |
| 5 | 2 | 3 | 348 | 27 | 5.0 | 25314.493 |
| 6 | 2 | 5 | 22 | 42 | 51.5 | 38470.110 |
| 7 | 2 | 4 | 41 | 30 | 1.9 | 30540.413 |
| 8 | 3 | 1 | 252 | 24 | 12.9 | - |
| 9 | 3 | 7 | 15 | 06 | 55.6 | 40655.120 |
| 10 | 3 | 5 | 61 | 47 | 43.3 | 22606.877 |
| 11 | 3 | 4 | 94 | 21 | 30.9 | 25378.281 |
| 12 | 3 | 2 | 168 | 27 | 5.0 | - |
| 13 | 4 | 2 | 221 | 30 | 1.8 | - |



| Observation | Li | ne | | Beari | ng | Distance |
|-------------|----|----|-----|-------|------|-----------|
| Number | | | 0 | 1 | | (m) |
| | | | | | | |
| 14 | 4 | 3 | 274 | 21 | 31.0 | - |
| 15 | 4 | 5 | 336 | 53 | 30.0 | 13713.543 |
| 16 | 4 | 6 | 23 | 58 | 55.4 | 28156.771 |
| 17 | 5 | 4 | 156 | 53 | 30.1 | - |
| 18 | 5 | 2 | 202 | 42 | 51.7 | - |
| 19 | 5 | 3 | 241 | 47 | 43.4 | - |
| 20 | 5 | 7 | 341 | 55 | 37.0 | 30046.422 |
| 21 | 5 | 8 | 31 | 7 | 39.1 | 38108.480 |
| 22 | 5 | 6 | 52 | 4 | 14.6 | 21332.688 |
| 23 | 6 | 4 | 203 | 58 | 55.6 | - |
| 24 | 6. | 5 | 232 | 4 | 14.7 | - |
| 25 | 6 | 7 | 300 | 34 | 45.6 | 30371.764 |
| 26 | 6 | 8 | 08 | 2 | 4.0 | 19719.190 |
| 27 | 7 | 1 | 229 | 32 | 4.6 | - |
| 28 | 7 | 3 | 195 | - 6 | 55.7 | - |
| 29 | 7 | 5 | 161 | 5 | 37.0 | _ |
| 30 | 7 | 6 | 120 | 34 | 45.7 | - |
| 31 | 7 | 8 | 82 | 2 | 26.4 | 29303.530 |
| 32 | 7 | 11 | 60 | 32 | 9.8 | 43643.720 |
| 33 | 7 | 10 | 41 | 55 | 3.7 | 27892.630 |
| 34 | 7 | 9 | 14 | 22 | 56.2 | 21718.190 |
| 35 | 8 | 6 | 188 | 22 | 44.0 | |
| 36 | 8 | 5 | 211 | 7 | 39.0 | _ |
| 37 | 8 | 7 | 262 | 2 | 26.4 | - |
| 38 | 8 | 9 | 305 | 42 | 13.7 | 29095.230 |
| 39 | 8 | 10 | 328 | 6 | 52.8 | 19664.661 |
| 40 | 8 | 11 | 27 | 16 | 45.7 | 19588.160 |
| 41 | 9 | 7 | 194 | 22 | 56.4 | - |
| 42 | 9 | 8 | 125 | 42 | 13.7 | - |
| 43 | 9 | 10 | 91 | 13 | 20.4 | 13242.450 |
| 44 | 9 | 11 | 89 | 14 | 41.4 | 32607.292 |
| 45 | 10 | 9 | 271 | 13 | 20.5 | - |
| 46 | 10 | 7 | 221 | 55 | 3.8 | - |
| 47 | 10 | 8 | 148 | 6 | 52.9 | - |
| 48 | 10 | 11 | 87 | 53 | 37.1 | 19378.227 |
| 49 | 11 | 9 | 269 | 14 | 41.5 | - 7 |
| 50 | 11 | 10 | 267 | 53 | 37.0 | |
| 51 | 11 | 7 | 240 | 32 | 9.9 | _ |
| 52 | 11 | 8 | 207 | 16 | 45.8 | - |

Table 4.8: Continued

4.2.2.2 Second Order Network

The real second order network consisted of fifteen stations connected onto the real first order network described in section (4.2.2.1) above. (cf. Fig. 4.6). The corresponding observational data sets are as listed in Table (4.10) while the approximate coordinates are given in Table (4.9). In Table (4.9), the first eleven approximate coordinates were determined through free network

adjustment of the real first order network while the rest are obtained from Survey of Kenya. The angular error of the observations was taken to be ± 1 .

| Point | S.K | Coordinates | | |
|-------|----------|-------------|------------|--|
| | Code | N (m) | E (m) | |
| 1 | SKP56 | 9583104.004 | 513215.950 | |
| 2 | SKP60 | 9576179.235 | 574648.607 | |
| 3 | SKP61 | 9600981.218 | 569580.575 | |
| 4 | SKP62 | 9599052.507 | 594885.488 | |
| 5 | SKP63 | 9611665.696 | 589503.231 | |
| 6 | SKP64 | 9624778.565 | 606329.885 | |
| 7 | SKP65 | 9640229.703 | 580182.077 | |
| 8 | SKP66 | 9644287.286 | 609203.286 | |
| 9 | SKP67 | 9661267.225 | 585576.691 | |
| 10 | SKP68 | 9660984.753 | 598816.111 | |
| 11 | SKP69 | 9661696.859 | 618181.218 | |
| 12 | 192.S.4 | 9651426.870 | 578082.210 | |
| 13 | 192.S.8 | 9649302.660 | 592482.850 | |
| 14 | 193.S.2 | 9640093.640 | 625611.430 | |
| 15 | 198.S.12 | 9614609.390 | 603055.440 | |
| 16 | 192.5.2 | 9626055.670 | 593121.870 | |
| 17 | 192.S.1 | 9623694.380 | 582449.870 | |
| 18 | 192.S.3 | 9625643.250 | 561292.670 | |
| 19 | 197.S.4 | 9607749.860 | 545064.590 | |
| 20 | 198.S.8 | 9610759.110 | 559563.590 | |
| 21 | 198.S.9 | 9609410.820 | 563591.710 | |
| 22 | 198.S.7 | 9592183.630 | 576550.570 | |
| 23 | 198.S.3 | 9584543.130 | 589735.740 | |
| 24 | 198.S.5 | 9585354.590 | 561756.300 | |
| 25 | 197.S.1 | 9580752.500 | 538526.380 | |
| 26 | 197.S.2 | 9589557.530 | 528224.190 | |

Table 4.9: Approximate coordinates for the real second order network

Table 4.10: Observational data sets for the real second order network

| Observation | L | ine | | Bearin | ng | Distance |
|-------------|----|-----|-----|--------|------|------------|
| Number | | | 0 | | ** | (m) |
| 1 | 12 | 7 | 169 | 22 | 42.3 | 11392.335 |
| 2 | 12 | 9 | 37 | 17 | 34.9 | 12369.293 |
| 3 | 13 | • 7 | 233 | 35 | 15.5 | - |
| 4 | 13 | 8 | 106 | 41 | 48.0 | - |
| 5 | 13 | 9 | 330 | 0 | 19.6 | 13814.687 |
| 6 | 14 | 6 | 231 | 32 | 25.3 | 24623.681 |
| 7 | 14 | 8 | 284 | 20 | 13.6 | 16935.563 |
| 8 | 14 | 11 | 341 | 1 | 11.6 | - |
| 9 | 15 | 4 | 207 | 42 | 24.5 | · • • = |
| 10 | 15 | 5 | 257 | 44 | 41.4 | - |
| 11 | 15 | 6 | 17 | 50 | 53.6 | 10683.383 |
| 12 | 16 | - 5 | 194 | 6 | 54.6 | 14837.980 |
| 13 | 16 | 6 | 95 | 31 | 21.6 | 113269.516 |
| 14 | 16 | 8 | 41 | 24 | 51.2 | 24310.634 |
| 15 | 16 | 7 | 317 | 36 | 22.6 | - |
| 16 | 17 | 5 | 149 | 36 | 47.3 | - |
| 17 | 17 | 3 | 193 | 54 | 57.5 | - |



Figure 4.6: The real second order network

| Observation | Li | ne | | Bearir | ıg | Distance |
|-------------|----|----|-----|--------|------|-----------|
| Number | | | 0 | , | " | (m) |
| 18 | 17 | 18 | 275 | 15 | 46.6 | - |
| 19 | 17 | 7 | 352 | 11 | 25.9 | 16690.070 |
| 20 | 18 | 20 | 186 | 37 | 34.5 | 14984.326 |
| 21 | 18 | 7 | 52 | 19 | 28.9 | 23865.886 |
| 22 | 18 | 17 | 95 | 15 | 46.0 | - |
| 23 | 18 | 5 | 116 | 21 | 25.0 | 31483.464 |
| 24 | 19 | 6 | 222 | 47 | 24.0 | 24790.315 |
| 25 | 19 | 4 | 143 | 18 | 7.5 | - |
| 26 | 19 | 3 | 105 | 26 | 4.2 | - |
| 27 | 19 | 20 | 78 | 16 | 29.4 | 14808.001 |
| 28 | 20 | 21 | 108 | 30 | 23.4 | 4247.690 |
| 29 | 20 | 18 | 06 | 37 | 34.9 | - |
| 30 | 20 | 19 | 258 | 16 | 29.6 | - |
| 31 | 21 | 3 | 144 | 36 | 27.9 | 10340.648 |
| 32 | 21 | 20 | 288 | 30 | 23.4 | _ |
| 33 | 21 | 7 | 28 | 17 | 39.9 | 35000.587 |
| 34 | 22 | 2 | 270 | 0 | 9.3 | 17894.890 |
| 35 | 22 | 3 | 120 | 5 | 28.5 | 15238.942 |
| 36 | 22 | 5 | 33 | 37 | 5.1 | 23394.975 |
| 37 | 22 | 3 | 321 | 36 | 42.0 | |
| 38 | 23 | 2 | 240 | 59 | 50.2 | - |
| 39 | 23 | 4 | 19 | 32 | 28.1 | 15396.022 |
| 40 | 23 | 22 | 300 | 5 | 28.4 | _ |
| 41 | 24 | 2 | 125 | 26 | 21.1 | 15823.986 |
| 42 | 24 | 3 | 26 | 35 | 50.9 | -99 |
| 43 | 24 | 19 | 323 | 18 | 7.5 | - |
| 44 | 24 | 6 | 277 | 8 | 39.0 | 33794.283 |
| 45 | 24 | 5 | 258 | -7 | 39.4 | 23681.294 |
| 46 | 25 | 1 | 275 | 18 | 31.7 | 25419.370 |
| 47 | 25 | 6 | 310 | 31 | 10.6 | 13552.337 |
| 48 | 25 | 4 | 78 | 47 | 38.4 | - |
| 49 | 26 | 1 | 246 | 44 | 0.1 | 16336.566 |
| 50 | 26 | 25 | 130 | 31 | 11.1 | _ |
| 51 | 26 | 24 | 97 | 8 | 39.5 | - |
| 52 | 26 | 19 | 42 | 47 | 24.4 | - |

Table 4.10: Continued

4.2.2.3 Third Order Network

The real third order network consisted of fifteen stations connected onto the real second order network described in section 4.2.2.2 (cf. Fig. 4.7). The corresponding observational data sets are as listed in Table (4.12) while the approximate coordinates are given in Table (4.11a). (4.11b), (4.11c) and (4.11d). In Table (4.11a), the first twenty six approximate coordinates were determined through densification process using the Static-Dynamic approach while in Table (4.11b) the first twenty six approximate coordinates were determined through first level densification process using the Sub-Optimal Fusion approach of the real second order network. In Table (4.11c) all the approximates were determined through first level densification process

using the dynamic approach while in Table (4.11d), the first twenty six coordinates were determined through densification process using the static approach. The rest are as obtained from Survey of Kenya.

| Point | S.K | Coordinates | |
|-------|----------|-------------|------------|
| | Code | N (m) | E (m) |
| 1 | SKP56 | 9583104.004 | 513215.950 |
| 2 | SKP60 | 9576179.235 | 574648.607 |
| 3 | SKP61 | 9600981.218 | 569580.575 |
| 4 | SKP62 | 9599052.507 | 594885.488 |
| 5 | SKP63 | 9611665.696 | 589503.231 |
| 6 | SKP64 | 9624778.565 | 606329.885 |
| 7 | SKP65 | 9640229.703 | 580182.077 |
| 8 | SKP66 | 9644287.286 | 609203.286 |
| 9 | SKP67 | 9661267.225 | 585576.691 |
| 10 | SKP68 | 9660984.753 | 598816.111 |
| 11 | SKP69 | 9661696.859 | 618181.218 |
| 12 | 192.S.4 | 9651426.855 | 578082.243 |
| 13 | 192.S.8 | 9649302.681 | 592482.865 |
| 14 | 193.S.2 | 9640093.572 | 625611.395 |
| 15 | 198.S.12 | 9614609.371 | 603055.410 |
| 16 | 192.S.2 | 9626055.619 | 593121.942 |
| 17 | 192.S.1 | 9623694.425 | 582449.886 |
| 18 | 192.S.3 | 9625643.288 | 561292.564 |
| 19 | 197.S.4 | 9607749.690 | 545064.420 |
| 20 | 193.S.8 | 9610759.097 | 559563.423 |
| 21 | 198.S.9 | 9609410.878 | 563591.472 |
| 22 | 193.S.7 | 9592183.544 | 576550.590 |
| 23 | 198.S.3 | 9584543.218 | 589735.830 |
| 24 | 198.S.5 | 9585354.356 | 561756.098 |
| 25 | 197.S.1 | 9580752.250 | 538526.297 |
| 26 | 197.S.2 | 9589557.286 | 528224.012 |
| 27 | 197.T.1 | 9598477.45 | 540001.04 |
| 28 | 197.T.4 | 9590143.01 | 544871.93 |
| 29 | 193.T.2 | 9592184.55 | 558655.59 |
| 30 | 198.T.9 | 9586646.84 | 596567.51 |
| 31 | 193.T.5 | 9593341.46 | 585647.23 |
| 32 | 193.T.13 | 9610982.26 | 577814.01 |
| 33 | 193.T.14 | 9608655.32 | 595394.33 |
| 34 | 193.T.20 | 9619838.45 | 564763.86 |
| 35 | 192.T.3 | 9620013.73 | 589321.42 |
| 36 | 192.T.7 | 9635147.76 | 567613.38 |
| 37 | 192.T.18 | 9630041.92 | 586400.12 |
| 38 | 192.T.26 | 9639112.32 | 594892.10 |
| 39 | 192.T.21 | 9635021.72 | 609221.86 |
| 40 | 192.T.30 | 9649311.34 | 618081.16 |
| 41 | 192.T.35 | 9656888.74 | 608069.420 |

Table 4.11.1: Approximate coordinates for the real third order network used in the Static-Dynamic densification approach

| CodeN (m)E (m)1SKP569583104.004513215.9502SKP609576179.235574648.6073SKP61960981.218569580.5754SKP629599052.507594885.4885SKP639611665.696589503.2316SKP649624778.565606329.8857SKP659640229.703580182.0778SKP669644287.286609203.2869SKP679661267.225585576.69110SKP689660984.753590816.11111SKP699661696.859618181.21812192.S.4951426.813578082.22613192.S.89649302.665592482.85914193.S.29640093.569625611.42415198.S.12961609.393603055.42516192.S.29626055.643593121.94817192.S.19623694.391582449.93618192.S.3962643.222561292.59619197.S.4960749.665545064.45220198.S.99609410.818563591.51122198.S.9950957.318528223.99627197.S.1958254.357551756.08125197.S.1958957.318528223.99627197.S.19592184.55558655.5930198.T.9958646.84596567.5131198.T.13961098.26577814.0132198.T.139620013.73589321.423 | Point | S.K | Coord | Coordinates | | | |
|--|-------|----------|-------------|-------------|--|--|--|
| 1SKP56 9583104.004 513215.950 2SKP60 9576179.235 574648.607 3SKP61 9600981.218 569580.575 4SKP62 959052.507 594885.488 5SKP63 9611665.696 589503.231 6SKP64 9624778.565 606329.885 7SKP65 9640229.703 580182.077 8SKP66 9644287.286 609203.286 9SKP67 9661267.225 58576.691 10SKP68 9660984.753 598816.111 11SKP69 9661696.859 618181.218 12 $192.S.4$ 9651426.813 578082.226 13 $192.S.8$ 9649302.665 592482.859 14 $193.S.2$ 9640093.569 625611.424 15 $198.S.12$ 9614609.393 603055.425 16 $192.S.2$ $9622695.643.222$ 561292.596 19 $197.S.4$ 9607749.665 545064.452 20 $198.S.8$ 9610759.036 559563.462 21 $198.S.9$ 969410.818 563591.511 22 $198.S.3$ 958957.318 528223.996 23 $198.S.3$ 958957.318 528223.996 24 $198.S.5$ 958957.318 528223.996 25 $197.S.1$ 9592184.55 558655.59 30 $198.T.2$ 9593341.46 585647.23 32 $198.T.3$ 9620013.73 589321.42 33 $198.T.14$ 9608655.32 595394.33 </td <td></td> <td>Code</td> <td>N (m)</td> <td colspan="3">E (m)</td> | | Code | N (m) | E (m) | | | |
| 2 SKP60 9576179.235 574648.607 3 SKP61 9600981.218 569580.575 4 SKP62 9599052.507 594885.488 5 SKP63 9611665.696 589503.231 6 SKP64 9624778.565 606329.885 7 SKP65 9640229.703 580182.077 8 SKP66 9644287.286 609203.286 9 SKP66 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.2 9640093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.9 9609410.818 563591.511 | 1 | SKP56 | 9583104.004 | 513215.950 | | | |
| 3 SKP61 9600981.218 S69580.575 4 SKP62 9599052.507 594885.488 5 SKP63 9611665.696 589503.231 6 SKP64 9624778.565 606329.885 7 SKP65 9640229.703 580182.077 8 SKP66 9644287.286 609203.286 9 SKP66 9660984.753 599816.111 10 SKP68 9660984.753 599816.111 11 SKP69 9661966.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.2 962093.665 592482.859 14 193.S.2 9640093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.1 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 | 2 | SKP60 | 9576179.235 | 574648.607 | | | |
| 4 SKP62 9599052.507 594885.488 5 SKP63 9611665.696 589503.231 6 SKP64 9624778.565 606329.885 7 SKP65 9640229.703 580182.077 8 SKP66 9644287.286 609203.286 9 SKP67 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.5.4 9651426.813 578082.226 13 192.5.8 9649302.665 592482.859 14 193.5.2 9624093.569 625611.424 15 198.5.12 9614609.393 603055.425 16 192.5.2 9626643.222 561292.596 19 197.5.4 9607749.665 545064.452 20 198.5.8 9610759.036 559563.462 21 198.5.9 9580752.276 538526.270 23 198.5.5 9585354.357 561756.081 | 3 | SKP61 | 9600981.218 | 569580.575 | | | |
| 5 SKP63 9611665.696 589503.231 6 SKP64 9624778.565 606329.885 7 SKP65 9640229.703 580182.077 8 SKP66 9644287.286 609203.286 9 SKP67 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.s.4 951426.813 578082.226 13 192.s.8 964093.569 625611.424 15 198.5.12 9640093.569 625611.424 15 198.5.12 9626055.643 593121.948 17 192.s.1 9625643.222 561292.596 18 192.s.3 9625643.222 561292.596 19 197.s.4 9607749.665 545064.452 20 198.s.8 9610759.036 559563.462 21 198.s.9 9502183.530 576550.637 23 198.5.5 9585354.357 561756.081 <t< td=""><td>4</td><td>SKP62</td><td>9599052.507</td><td>594885.488</td></t<> | 4 | SKP62 | 9599052.507 | 594885.488 | | | |
| 6 SKP64 9624778.565 606329.885 7 SKP65 9640229.703 580182.077 8 SKP66 9644287.286 609203.286 9 SKP67 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.8 9649302.665 592482.859 14 193.S.2 9626055.643 593121.948 17 192.S.1 9623694.391 582449.936 18 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.7 9592183.530 576550.637 23 198.S.7 9592183.530 576550.637 24 198.S.5 9585354.357 561756.081 25 197.S.1 9589477.45 540001.04 28 197.T.1 9598447.145 58655.59 <tr< td=""><td>5</td><td>SKP63</td><td>9611665.696</td><td>589503.231</td></tr<> | 5 | SKP63 | 9611665.696 | 589503.231 | | | |
| 7 SKP65 9640229.703 580182.077 8 SKP66 9644287.286 609203.286 9 SKP67 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.5.4 9651426.813 578082.226 13 192.5.8 9649302.665 592482.859 14 193.5.2 9640093.569 625611.424 15 198.5.12 9614609.393 603055.425 16 192.5.3 9625643.222 561292.596 18 192.5.3 9625643.222 561292.596 19 197.5.4 9607749.665 545064.452 20 198.5.8 9610759.036 559563.462 21 198.5.9 9609410.818 563591.511 22 198.5.7 958354.357 561756.0637 23 198.5.3 958354.357 561756.0637 24 198.5.5 9586354.357 561756.0637 <td>6</td> <td>SKP64</td> <td>9624778.565</td> <td>606329.885</td> | 6 | SKP64 | 9624778.565 | 606329.885 | | | |
| 8 SKP66 9644287.286 609203.286 9 SKP67 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.8 9649302.665 592482.859 14 193.S.2 9640093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.7 9592183.530 576550.637 23 198.S.3 9584543.174 589735.857 24 198.S.5 9580557.318 528223.996 27 197.T.1 9598477.45 540001.04 28 197.T.1 9598457.318 528223.996 <td>7</td> <td>SKP65</td> <td>9640229.703</td> <td>580182.077</td> | 7 | SKP65 | 9640229.703 | 580182.077 | | | |
| 9 SKP67 9661267.225 585576.691 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.8 9649302.665 592482.859 14 193.S.2 9640093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.1 9623694.391 582449.936 18 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.9 9609410.818 563591.511 22 198.S.3 9584543.174 589735.857 24 198.S.5 9585354.357 561756.081 25 197.S.1 9592184.55 58655.59 30 198.T.2 9592184.55 58655.59 30 198.T.2 9592184.55 586656.59 | 8 | SKP66 | 9644287.286 | 609203.286 | | | |
| 10 SKP68 9660984.753 598816.111 11 SKP69 9661696.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.8 9649302.665 592482.859 14 193.S.2 9610093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.1 9623694.391 582449.936 18 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.7 9592183.530 576550.637 23 198.S.3 9584543.174 589735.857 24 198.S.5 9585354.357 561756.081 25 197.S.1 9580752.276 538526.270 26 197.S.2 9589557.318 528223.996 27 197.T.1 95992184.55 558655.59 | 9 | SKP67 | 9661267.225 | 585576.691 | | | |
| 11 SKP69 9661696.859 618181.218 12 192.S.4 9651426.813 578082.226 13 192.S.8 9649302.665 592482.859 14 193.S.2 9640093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.1 9623694.391 582449.936 18 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.9 9609410.818 563591.511 22 198.S.7 9592183.530 576550.637 23 198.S.3 9584543.174 589735.857 24 198.S.5 958354.357 561756.081 25 197.S.1 9580752.276 538526.270 26 197.S.2 9592184.55 558655.59 30 198.T.2 9592184.55 558655.59 | 10 | SKP68 | 9660984.753 | 598816.111 | | | |
| 12 192.s.4 9651426.813 578082.226 13 192.s.8 9649302.665 592482.859 14 193.s.2 9640093.569 625611.424 15 198.s.12 9614609.393 60305s.425 16 192.s.2 9626055.643 593121.948 17 192.s.1 9623694.391 582449.936 18 192.s.3 9625643.222 561292.596 19 197.s.4 9607749.665 545064.452 20 198.s.8 9610759.036 559563.462 21 198.s.9 9609410.818 563591.511 22 198.s.7 9592183.530 576550.637 23 198.s.3 9584543.174 589735.857 24 198.s.5 958354.357 561756.081 25 197.s.1 9580752.276 538526.270 26 197.s.2 9592184.55 558655.59 30 198.T.2 9592184.55 558655.59 30 198.T.2 9593341.46 585647.23 | 11 | SKP69 | 9661696.859 | 618181.218 | | | |
| 13 192.S.8 9649302.665 592482.859 14 193.S.2 9640093.569 625611.424 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.1 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.9 9609410.818 563591.511 22 198.S.3 9584543.174 589755.637 23 198.S.3 9584543.174 589735.857 24 198.S.5 9585354.357 561756.081 25 197.S.1 9580752.276 538526.270 26 197.S.2 958957.318 528223.996 27 197.T.1 9598477.45 540001.04 28 197.T.4 9590143.01 544871.93 29 198.T.2 9593341.46 585647.23 31 198.T.3 9610982.26 577814.01 < | 12 | 192.S.4 | 9651426.813 | 578082.226 | | | |
| 14193.S.29640093.569625611.42415198.S.129614609.393603055.42516192.S.29626055.643593121.94817192.S.19623694.391582449.93618192.S.39625643.222561292.59619197.S.49607749.665545064.45220198.S.89610759.036559563.46221198.S.99609410.818563591.51122198.S.79592183.530576550.63723198.S.39584543.174589735.85724198.S.59585354.357561756.08125197.S.19598477.45540001.0428197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29593341.46585647.2331198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334192.T.39620013.73589321.4236192.T.79635147.76567613.8637192.T.18963041.92586400.1238192.T.219635021.72609221.8640192.T.219656888.74608069.420 | 13 | 192.S.8 | 9649302.665 | 592482.859 | | | |
| 15 198.S.12 9614609.393 603055.425 16 192.S.2 9626055.643 593121.948 17 192.S.1 9623694.391 582449.936 18 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.9 9609410.818 563591.511 22 198.S.7 9592183.530 576550.637 23 198.S.5 9585354.357 561756.081 25 197.S.1 9580752.276 538526.270 26 197.S.2 9589557.318 528223.996 27 197.T.1 9598477.45 540001.04 28 197.T.4 9590143.01 544871.93 29 198.T.2 9592184.55 558655.59 30 198.T.3 9610982.26 577814.01 33 198.T.14 9608655.32 595394.33 34 198.T.20 961988.45 564763.86 <td>14</td> <td>193.S.2</td> <td>9640093.569</td> <td>625611.424</td> | 14 | 193.S.2 | 9640093.569 | 625611.424 | | | |
| 16192.S.29626055.643593121.94817192.S.19623694.391582449.93618192.S.39625643.222561292.59619197.S.49607749.665545064.45220198.S.89610759.036559563.46221198.S.99609410.818563591.51122198.S.79592183.530576550.63723198.S.39584543.174589735.85724198.S.59585354.357561756.08125197.S.19580752.276538526.27026197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 15 | 198.S.12 | 9614609.393 | 603055.425 | | | |
| 17192.S.19623694.391582449.93618192.S.39625643.222561292.59619197.S.49607749.665545064.45220198.S.89610759.036559563.46221198.S.99609410.818563591.51122198.S.79592183.530576550.63723198.S.39584543.174589735.85724198.S.59585354.357561756.08125197.S.19580752.276538526.27026197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.139610982.26577814.0133198.T.149608655.32595394.3334192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 16 | 192.S.2 | 9626055.643 | 593121.948 | | | |
| 18 192.S.3 9625643.222 561292.596 19 197.S.4 9607749.665 545064.452 20 198.S.8 9610759.036 559563.462 21 198.S.9 9609410.818 563591.511 22 198.S.7 9592183.530 576550.637 23 198.S.3 9584543.174 589735.857 24 198.S.5 9585354.357 561756.081 25 197.S.1 9580752.276 538526.270 26 197.S.2 958957.318 528223.996 27 197.T.1 9598477.45 540001.04 28 197.T.4 9590143.01 544871.93 29 198.T.2 9592184.55 558655.59 30 198.T.9 9586646.84 596567.51 31 198.T.13 9610982.26 577814.01 33 198.T.14 9608655.32 595394.33 34 192.T.3 9620013.73 589321.42 36 192.T.7 9635147.76 567613.38 37 192.T.18 9630041.92 586400.12 < | 17 | 192.S.1 | 9623694.391 | 582449.936 | | | |
| 19197.s.49607749.665545064.45220198.s.89610759.036559563.46221198.s.99609410.818563591.51122198.s.79592183.530576550.63723198.s.39584543.174589735.85724198.s.59585354.357561756.08125197.s.19580752.276538526.27026197.s.29589557.318528223.99627197.T.19590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.139610982.26577814.0133198.T.149608655.32595394.3334192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.219635021.72609221.8640192.T.359656888.74608069.420 | 18 | 192.5.3 | 9625643.222 | 561292.596 | | | |
| 20198.s.89610759.036559563.46221198.s.99609410.818563591.51122198.s.79592183.530576550.63723198.s.39584543.174589735.85724198.s.59585354.357561756.08125197.s.19580752.276538526.27026197.s.29589557.318528223.99627197.r.19598477.45540001.0428197.r.49590143.01544871.9329198.r.29592184.55558655.5930198.r.99586646.84596567.5131198.r.139610982.26577814.0133198.r.149608655.32595394.3334198.r.209619838.45564763.8635192.r.39620013.73589321.4236192.r.79635147.76567613.3837192.r.189630041.92586400.1238192.r.219635021.72609221.8640192.r.359656888.74608069.420 | 19 | 197.S.4 | 9607749.665 | 545064.452 | | | |
| 21198.S.99609410.818563591.51122198.S.79592183.530576550.63723198.S.39584543.174589735.85724198.S.59585354.357561756.08125197.S.19580752.276538526.27026197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 20 | 198.S.8 | 9610759.036 | 559563.462 | | | |
| 22198.s.79592183.530576550.63723198.s.39584543.174589735.85724198.s.59585354.357561756.08125197.s.19580752.276538526.27026197.s.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 21 | 198.S.9 | 9609410.818 | 563591.511 | | | |
| 23198.S.39584543.174589735.85724198.S.59585354.357561756.08125197.S.19580752.276538526.27026197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39630041.92586400.1236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 22 | 198.S.7 | 9592183.530 | 576550.637 | | | |
| 24198.S.59585354.357561756.08125197.S.19580752.276538526.27026197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 23 | 198.S.3 | 9584543.174 | 589735.857 | | | |
| 25197.S.19580752.276538526.27026197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 24 | 198.S.5 | 9585354.357 | 561756.081 | | | |
| 26197.S.29589557.318528223.99627197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 25 | 197.S.1 | 9580752.276 | 538526.270 | | | |
| 27197.T.19598477.45540001.0428197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 26 | 197.S.2 | 9589557.318 | 528223.996 | | | |
| 28197.T.49590143.01544871.9329198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 27 | 197.T.1 | 9598477.45 | 540001.04 | | | |
| 29198.T.29592184.55558655.5930198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 28 | 197.T.4 | 9590143.01 | 544871.93 | | | |
| 30198.T.99586646.84596567.5131198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 29 | 198.T.2 | 9592184.55 | 558655.59 | | | |
| 31198.T.59593341.46585647.2332198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 30 | 198.T.9 | 9586646.84 | 596567.51 | | | |
| 32198.T.139610982.26577814.0133198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 31 | 198.T.5 | 9593341.46 | 585647.23 | | | |
| 33198.T.149608655.32595394.3334198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 32 | 198.T.13 | 9610982.26 | 577814.01 | | | |
| 34198.T.209619838.45564763.8635192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 33 | 198.T.14 | 9608655.32 | 595394.33 | | | |
| 35192.T.39620013.73589321.4236192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 34 | 198.T.20 | 9619838.45 | 564763.86 | | | |
| 36192.T.79635147.76567613.3837192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 35 | 192.T.3 | 9620013.73 | 589321.42 | | | |
| 37192.T.189630041.92586400.1238192.T.269639112.32594892.1039192.T.219635021.72609221.8640192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 36 | 192.T.7 | 9635147.76 | 567613.38 | | | |
| 38 192.T.26 9639112.32 594892.10 39 192.T.21 9635021.72 609221.86 40 192.T.30 9649311.34 618081.16 41 192.T.35 9656888.74 608069.420 | 37 | 192.T.18 | 9630041.92 | 586400.12 | | | |
| 39 192.T.21 9635021.72 609221.86 40 192.T.30 9649311.34 618081.16 41 192.T.35 9656888.74 608069.420 | 38 | 192.T.26 | 9639112.32 | 594892.10 | | | |
| 40192.T.309649311.34618081.1641192.T.359656888.74608069.420 | 39 | 192.T.21 | 9635021.72 | 609221.86 | | | |
| 41 192.T.35 9656888.74 608069.420 | 40 | 192.T.30 | 9649311.34 | 618081.16 | | | |
| | 41 | 192.T.35 | 9656888.74 | 608069.420 | | | |

 Table 4.11.2: Approximate coordinates for the real third order network used in the Sub-Optimal Fusion densification approach

| Point | S.K. Coordinates | | | |
|-------|------------------|-------------|------------|--|
| Poinc | Code | N (m) | E (m) | |
| 1 | SKP56 | 9583104.115 | 513215.937 | |
| 1 | SKP60 | 9576179.227 | 574648.570 | |
| 2 | SKP61 | 9600981,168 | 569580,640 | |
| 3 | SKP62 | 9599052.461 | 594885,487 | |
| 4 | SKP63 | 9611665.687 | 589503.315 | |
| 5 | SKP64 | 9624778.595 | 606329.877 | |
| 7 | SKP65 | 9640229.663 | 580182.066 | |
| 9 | SKP66 | 9644287.320 | 609203.331 | |
| 0 | SKP67 | 9661267.192 | 585576.661 | |
| 10 | SKP68 | 9660984.693 | 598816.071 | |
| 11 | SKP69 | 9661696.939 | 618181.173 | |
| 12 | 192.S.4 | 9651426.813 | 578082.226 | |
| 13 | 192.S.9 | 9649302.665 | 592482.859 | |
| 14 | 193.S.2 | 9640093.569 | 625611.424 | |
| 15 | 198.S.12 | 9614609.393 | 603055.425 | |
| 16 | 192.S.2 | 9626055.643 | 593121.948 | |
| 17 | 192.S.1 | 9623694.391 | 582449.936 | |
| 18 | 192.S.3 | 9625643.222 | 561292.596 | |
| 19 | 197.S.4 | 9607749.665 | 545064.452 | |
| 20 | 198.S.8 | 9610759.036 | 559563.462 | |
| 21 | 198.S.9 | 9609410.818 | 563591.511 | |
| 22 | 198.S.7 | 9592183.530 | 576550.637 | |
| 23 | 198.S.3 | 9584543.174 | 589735.857 | |
| 24 | 198.S.5 | 9585354.357 | 561756.081 | |
| 25 | 197.S.1 | 9580752.276 | 538526.270 | |
| 26 | 197.S.2 | 9589557.318 | 528223.996 | |
| 27 | 197.T.1 | 9598477.45 | 540001.04 | |
| 28 | 197.T.4 | 9590143.01 | 544871.93 | |
| 29 | 198.T.2 | 9592184.55 | 558655.59 | |
| 30 | 198.T.9 | 9586646.84 | 596567.51 | |
| 31 | 198.T.5 | 9593341.46 | 585647.23 | |
| 32 | 198.T.13 | 9610982.26 | 577814.01 | |
| 33 | 198.T.14 | 9608655.32 | 595394.33 | |
| 34 | 198.T.20 | 9619838.45 | 564763.86 | |
| 35 | 192.T.3 | 9620013.73 | 589321.42 | |
| 36 | 192.T.7 | 9635147.76 | 567613.38 | |
| 37 | 192.T.18 | 9630041.92 | 586400.12 | |
| 38 | 192.T.26 | 9639112.32 | 594892.10 | |
| 39 | 192.T.21 | 9635021.72 | 609221.86 | |
| 40 | 192.T.30 | 9649311.34 | 618081.16 | |
| 41 | 192.T.35 | 9656888.74 | 608069.420 | |

 Table 4.11.3: Approximate coordinates for real third order network used in the Dynamic densification approach

y

| Deint | SK | Coordi | nates |
|-------|----------|-------------|-------------|
| POINC | Code | N (m) | E (m) |
| 1 | SKP56 | 9583104 004 | 513215.950 |
| 1 | SKP60 | 9576179 235 | 574648.607 |
| 2 | SKP61 | 9600981 218 | 569580.575 |
| 3 | SKP62 | 9599052 507 | 594885,488 |
| 4 | SKP63 | 9611665 696 | 589503.231 |
| 5 | SKP64 | 9624778 565 | 606329,885 |
| 0 | SKP65 | 9640229 703 | 580182.077 |
| 1 | SKP66 | 9644287 286 | 609203.286 |
| 0 | SKP67 | 9661267 225 | 585576,691 |
| 9 | SKP68 | 9660984 753 | 598816,111 |
| 10 | SKP69 | 9661696 859 | 618181.218 |
| 12 | 192 5 4 | 9651426 856 | 578082,241 |
| 12 | 192.5.4 | 9649302 679 | 592482,863 |
| 10 | 193 5 2 | 9640093 585 | 625611.399 |
| 14 | 198.5.12 | 9614609 374 | 603055,417 |
| 15 | 192 5 2 | 9626055 626 | 593121,935 |
| 17 | 192.5.2 | 9623694 418 | 582449,886 |
| 19 | 192.5.1 | 9625643 281 | 561292.577 |
| 10 | 197 \$ 4 | 9607749 704 | 545064,434 |
| 20 | 198 5 3 | 9610759 098 | 559563,437 |
| 20 | 198 5 9 | 9609410 872 | 563591,495 |
| 22 | 198 5 7 | 9592183 549 | 576550,599 |
| 23 | 198 5 3 | 9584543 206 | 589735,832 |
| 24 | 198 5 5 | 9585354 386 | 561756,124 |
| 25 | 197 5 | 9580752 276 | 538526.299 |
| 26 | 197.5.2 | 9589557.305 | 528224.023 |
| 27 | 107 7 | 0500477 45 | 540001 04 |
| 28 | 107 T 1 | 9590477.45 | 544871 93 |
| 29 | 108 7 2 | 9590145.01 | 558655 59 |
| 30 | 198 T 3 | 9596646 94 | 596567.51 |
| 31 | 198 T 5 | 9500040.04 | 585647 23 |
| 32 | 198 7 12 | 9595541.40 | 577814 01 |
| 33 | 198 7 14 | 9010902.20 | 595394 33 |
| 34 | 198 T 20 | 9610838 /5 | 564763.86 |
| 35 | 192 T 3 | 9620013 73 | 589321,42 |
| 36 | 192 7 7 | 9635147 76 | 567613,38 |
| 37 | 192 m 18 | 9630041 92 | 586400.12 |
| 38 | 192.T 26 | 9639112 32 | 594892,10 |
| 39 | 192.T 21 | 9635021 72 | 609221.86 |
| 40 | 192.T 30 | 9649311 34 | 618081,16 |
| 41 | 192.T 35 | 9656888 74 | 608069, 420 |
| | | 2020000.73 | |

Table 4.11.4: Approximate coordinates for the real third order network used in the Static densification approach

*


| Cohcorvation | Line | | Bearing | | Distance |
|--------------|-------|-----|---------|------|----------|
| Number | Barre | 0 | , | | (m) |
| 1 | 27 26 | 232 | 51 | 31.2 | 14773.89 |
| 2 | 27 19 | 28 | 38 | 17.9 | 10564.67 |
| 3 | 27 28 | 149 | 41 | 47.2 | 9653.42 |
| 4 | 28 27 | 329 | 41 | 49.2 | 9653.42 |
| 5 | 28 29 | 81 | 34 | 28.8 | 13934.03 |
| 6 | 28 24 | 105 | 50 | 04.4 | 17550.11 |
| 7 | 28 25 | 214 | 2 | 52.3 | 11333.73 |
| 8 | 29 3 | 51 | 9 | 34.8 | 14026.28 |
| 9 | 29 24 | 155 | 35 | 06.0 | 7500.98 |
| 10 | 29 28 | 261 | 34 | 28.9 | 13934.03 |
| 11 | 30 22 | 285 | 27 | 41.4 | 20768.54 |
| 12 | 30 4 | 352 | 16 | 43.1 | 12519.18 |
| 13 | 30 23 | 252 | 53 | 06.9 | 7148.22 |
| 14 | 31 4 | 58 | 16 | 33.0 | 10861.01 |
| 15 | 31 22 | 262 | 44 | 43.9 | 9170.04 |
| 16 | 31 5 | 11 | 53 | 00.5 | 18725.55 |
| 17 | 32 5 | 86 | 39 | 13.9 | 11709.18 |
| 18 | 32 3 | 219 | 27 | 48.4 | 12954.16 |
| 19 | 32 21 | 263 | 41 | 41.8 | 14309.08 |
| 20 | 32 17 | 20 | 2 | 09.3 | 13531.09 |
| 21 | 33 5 | 297 | 4 | 01.9 | 6615.69 |
| 22 | 33 15 | 52 | 8 | 46.7 | 9702.74 |
| 23 | 33 4 | 183 | 1 | 59.5 | 9616.29 |
| 24 | 34 18 | 329 | 7 | 12.9 | 6763.58 |
| 25 | 34 17 | 77 | 42 | 03.2 | 18101.49 |
| 26 | 34 21 | 186 | 24 | 52.7 | 10493.27 |
| 27 | 34 20 | 209 | 48 | 10.9 | 10463.23 |
| 28 | 35 16 | 32 | 10 | 16.9 | 7137.31 |
| 29 | 35 5 | 178 | 45 | 07.4 | 8350.01 |
| 30 | 35 17 | 298 | LO | 32.6 | 1795.22 |
| 31 | 36 12 | 32 | 44 | 39.3 | 19354.74 |
| 32 | 36 / | 6/ | 59 | 06.6 | 13557.22 |
| 33 | 36 18 | 213 | 37 | 30.2 | 7014.05 |
| 34 | 37 10 | 120 | 40 | 20.2 | 10445 02 |
| 35 | 37 33 | 103 | 40 | 30.3 | 10445.35 |
| 37 | 37 17 | 211 | 23 | 41.0 | 11025 15 |
| 38 | 30 0 | 320 | 30 | 12 5 | 15218 19 |
| 39 | 39 16 | 197 | 13 | 1/ 8 | 13176 15 |
| 40 | 38 7 | 274 | 20 | 37 9 | 14752 10 |
| 41 | 38 13 | 346 | 41 | 53 6 | 10471 29 |
| 42 | 39 8 | 359 | 53 | 06.5 | 9265.58 |
| 43 | 39 14 | 72 | 4.8 | 16.9 | 17156.36 |
| 44 | 39 6 | 195 | 45 | 58.9 | 10642.58 |
| 45 | 40 11 | 0 | 27 | 45.3 | 12385.92 |
| 46 | 40 14 | 140 | 45 | 14.3 | 11902.59 |
| 47 | 40 8 | 240 | 29 | 37.9 | 10200.37 |
| 48 | 41 10 | 293 | 52 | 37.3 | 10119.34 |
| 49 | 41 11 | 64 | 34 | 08.8 | 11196.72 |
| 50 | 41 13 | 244 | 2 | 51.2 | 17334.62 |

Table 4.12: Observational data sets for the real third order network

4.3 Methods of Analysis

There are a number of criteria for determination of precision and reliability of a densification process. The precision of a network is the measure of the manner in which it propagates random errors. This is quantified by standard errors of parameters, positional error ellipses and standard errors of adjusted observations. Internal reliability of a network is its ability to have blunders detected. This is quantified by the improvement ratio i.e. the ratio of the a-posteriori standard error of an observation to it's a-priori value included in the inverseweight matrix [Askenazi, 1980]. External reliability of an observation is a measure of the effect of an undetected blunder, in that observation, on the estimated parameters and other quantities derived from these parameters. This is quantified by the gamma factor discussed in detail by Cross [1983].

The quality of the geodetic system can be analyzed either before or after the densification process. This is usually achieved through the network's a-posteriori variance-covariance matrix. In practice, the a-posteriori variance-covariance matrix needs to be determined for all planned networks otherwise one can not be sure that the network will fulfil the task for which it has been designed. Similarly, the densified network should have an associated variance-covariance matrix so as to know the uses to which the final parameters can be put.

Irrespective of any sparsity of the design matrix and the weight matrix, the a-posteriori variancecovariance matrix will in general be a full matrix i.e. for every unknown there will be an associated variance and for every pair of unknowns there will be a covariance. In this study therefore, main tool to aid analysis will be the network's a-posteriori variance-covariance matrix as given in (3.3.11) and (3.3.35d). The elements of the matrix are used to determine positional standard errors, error ellipses, circular probable errors (CPE) and standard errors of the derived quantities as discussed below.

4.3.1 Positional Standard Errors

Standard errors of the estimates are obtained by taking the square root of the diagonal elements of the variance-covariance matrix. Hence we quote for each adjusted coordinate a standard error. However in most cases, these standard errors are of limited use because of their dependence on

the origin (datum). Clearly, the further away they are from the network fixed points, the larger the positional standard errors will be.

In certain networks, there will be more than one fixed point. For instance in the situation where the third order network is being fitted onto a second order network. In this case, a larger positional error may merely indicate that the nearest fixed point is a long way away. The only situation in which positional errors may be useful is in a free network where the datum is defined over approximate coordinates neither fixing any particular point, for example, in a combined satellite and terrestrial network where there will be no fixed point at all.

4.3.2 Circular Probable Errors

A measure of accuracy for each part instead of the two components of the positional error can be obtained by combining the components, to give a vector sum referred to as "circular probable error" or "radial standard error" [Mikhail, 1976,pg 33] or "positional error sphere" for a three-dimensional case [Aduol, 1981. pg 46] and is given by:

| $\overline{\sigma}_{c} =$ | $\left[\frac{\sigma_E^2 + \sigma_{\chi}^2}{2}\right]$ | (4.3.1 |) |
|---------------------------|---|--------|---|
| | | | |

(4.3.2)

For *n* parameters we have that

$$\overline{\sigma}_{C} = \left[\frac{\sigma_1^2 + \sigma_2^2 - \dots + \sigma_n^2}{n}\right]$$

where σ_i [*i* = 1, 2, ..., *n*] are the respective standard errors.

4.3.3 Standard Error Ellipses

Standard error ellipses are relevant to two-dimensional networks only. However, extensions to other dimensions are possible although only the three-dimensional case is likely to be practically useful and in which case we talk of an error ellipsoid. There are two types of error ellipses within networks: the first, relative error ellipses, which express the reliability of the position of a point with respect to a neighbouring point. The second is the absolute error ellipse for a point. which reflects how accurately the point has been positioned. In the present study we shall use absolute error ellipses, as the interest of the study is to learn how accurately points are fixed. The derivation of error ellipse parameters is given in the summary in Appendix C and is given through the equations below.

$$\tan 2\psi_m = \frac{2\sigma_{xy}}{(\sigma_x^2 - \sigma_y^2)}$$
(4.3.3)

$$\sigma_m^2 = \sigma_{\max}^2 = \frac{1}{2} \left[\sigma_x^2 + \sigma_y^2 + \left(\left(\sigma_y^2 - \sigma_x^2 \right)^2 + 4 \left(\sigma_{xy}^2 \right)^2 \right)^2 \right]$$
(4.3.4a)

$$\sigma_n^2 = \sigma_{\min}^2 = \frac{1}{2} \left[\sigma_x^2 + \sigma_y^2 - \left(\left(\sigma_y^2 - \sigma_x^2 \right)^2 + 4 \left(\sigma_{xy} \right)^2 \right)^{\frac{1}{2}} \right]$$
(4.3.4b)

where σ_x^2 and σ_y^2 are the position variances in two mutually perpendicular directions ψ and $\psi + 90$. Hence we can compute the directions and values of the maximum and minimum variances at any point in the network.

Absolute error ellipses suffer the same disadvantage of being dependent on the origin (datum) as the positional standard errors. However, we can get some important overall network information from the pattern of the error ellipses. For example minor axes pointing approximately towards the origin indicate an overall network weakness in orientation. Major axes pointing towards the origin indicate overall network weakness in scale control.

4.3.4 Mean Shifts

These are the vectors determined from the final adjusted coordinates of points in a network using different methods or under different circumstances. They give a measure of displacement between points, which can be used to analyze networks.

4.4 Numerical Computing

4.4.1 Design of Computation

The fundamental network of the system was defined by adjusting the first order networks within the framework of a free network. The first densification was performed by applying the concept of *static-dynamic* approach on simulated and real networks at the first and second levels. In the static-dynamic densification, the observation data sets in Table (4.4) and (4.10) and the approximate coordinates in Table (4.3) and (4.9) were used for the first level densification. The observation data sets in Table (4.6) and (4.12) and the approximate coordinates in Table (4.5a) and (4.11a) were used for the second level densification. The second densification was performed by applying the concept of *sub-optimal fusion* approach on simulated and real networks at the first and second levels. In the sub-optimal fusion densification, the observation data sets in Table (4.4) and (4.10) and the approximate coordinates in Table (4.3) and (4.9) were used for the first level densification. The observation data sets in Table (4.6) and (4.12) and the approximate coordinates in Table (4.5b) and (4.11b) were used for the second level densification. The third densification was performed by applying the concept of dvnamic approach on simulated and real networks at the first and second levels. In the dynamic densification, the observation data sets in Table (4.4) and (4.10) and the approximate coordinates in Table (4.3) and (4.9) were used for the first level densification. The observation data sets in Table (4.6) and (4.12) and the approximate coordinates in Table (4.5c) and (4.11c) were used for the second level densification. The fourth densification was performed by applying the concept of *static* approach on simulated and real networks at the first and second levels. In the static densification, the observation data sets in Table (4.4) and (4.10) and the approximate coordinates in Table (4.3) and (4.9) were used for the first level densification. The observation data sets in Table (4.6) and (4.12) and the approximate coordinates in Table (4.5d) and (4,11d) were used for the second level densification.

4.4.2 Computer Programs

The computations were done using programs written in MATLAB which is an acronym for <u>MATrix LAB</u>oratory. MATLAB is a technical computing environment for high performance numeric computation and visualization. It is an iteractive system whose basic data element is a matrix that does not require dimensioning thus enhancing the speed of numerical solutions. Separate programs were written for each task i.e. free network adjustment, static-dynamic.static, dynamic and sub-optimal fusion approaches. In this section, two main programs FREE.M and DENSITY.M coded in MATLAB with which the computations were carried out on a personal computer model Pentium 3000 are explained.

4.4.2.1 Program FREE.M

This program performs network adjustment using the concept of free network adjustment (cf. section 2.3) to adjust the primary networks which were used to define the fundamental network on which subsequent densification using static-dynamic and sub-optimal fusion approaches were performed. Flow chart 1 in Appendix A.2 shows the systematic stages of the program.

1.1.2.2 Program DENSITY.M

All the approaches to densification discussed in chapter three are considered. It consist of three modules which are separately written, tested and linked together to form the program.

In the first module, the observation and provisional values are read into the computer memory and the computational matrices are initialized to zero. The flow chart in Appendix A.3 describes the process.

In the second module, the design matrix A, the residual vector of the observations Y and the weight matrix W are formed from the reduced observations in read in module one above. The network is densified depending on the different approaches and levels. The a-posteriori variance of unit weight is also computed.

In the third module, the data obtained in the second module are used in network analysis through determination of variance-covariance matrix from equations (3.2.20), (3.2.28), (3.3.11) and (3.3.35d). The variance-covariance matrix, a-posteriori standard error of the observation data sets and posteriori error ellipses are determined. Finally, the results are output for each densification approach. Appendix A.3 describes the process.

THE TEST RESULTS

5.1 Introduction

In this chapter, the results are presented in two main sections. Section 5.2 contains simulated network results while section 5.3 contains real network results. Each section further contains results of the free network adjustment and of the densification process using *static-dynamic*, *suo-optimal fusion*, *dynamic* and *static* approaches. The computed shifts between the final coordinates obtained from the different approaches are also presented in each section. The Tables of results presented in each of the sections consists of estimated correction to the approximate or provisional coordinates (ΔE , ΔN) for each network point, their corresponding standard errors (σ_E , σ_N) computed from equations (3.2.28), (3.3.11) and (3.3.35d). Also presented in each table is the parameters for error ellipses viz.: semi-major axis (σ_{max}), semiminor axis (σ_{min}) and the orientation of the semi-major axis (α) computed from equations (4.3.3), (4.3.4a) and (4.3.4b). These results, together with those listed in Appendix B, are part of the results obtained by running the programs discussed in Chapter Four.

5.2 The Simulated Network

5.2.1 First Order Network Adjustment

The results presented in this section were obtained by adjusting the simulated first order network through the free network technique using the approximate coordinates listed in Table (4.1) and observation data sets listed in Table (4.2). This formed the fundamental network on which the simulated first level and simulated second level densifications were performed. The resulting error ellipses are presented diagrammatically in Fig. 5.1.

| POINT | <u>Δ</u> N (m) | ΔE (m) | σ_N (m) | σ_{E} (m) | σ _{max} (m) | σ _{mun} (m) | | α | 11 |
|-------|-------------------|----------------|----------------|------------------|-------------------------|-------------------------|-----|----|------|
| 1 | -0.0044 | -0.0029 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 60 | 0 | 0.1 |
| | -0.0013 | 0.0064 | 0.0036 | 0.0025 | 0.0036 | 0.0025 | 00 | 00 | 00 |
| 3 | 0.0057 | -0.0035 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 299 | 59 | 59.9 |

Table 5.2.1: Coordinate Corrections and Stochastic Parameters-First Order Simulated Network

 $\overline{\sigma}_{v} = 0.00309$ $\overline{\sigma}_{\varepsilon} = 0.00313$ $\overline{\sigma}_{c} = 0.00311$ $\hat{\sigma}_{0}^{2} = 0.999667$

Table 5.2.2: Estimated Coordinates-First Order Simulated Network.

| POINT | PROVISIONAL | COORDINATES | ADJUSTED COORDINATES | | | |
|-------|-------------|-------------|----------------------|----------|--|--|
| | N (m. | E (m) | N (m) | E(m) | | |
| 1 | 100.000 | 100.000 | 99.9956 | 99.9971 | | |
| 2 | 446.410 | 300.000 | 446.4087 | 300.0064 | | |
| 3 | 100.000 | 500.000 | 100.0057 | 499.9965 | | |

5.2.2 Static-Dynamic Densification

The results presented in this section were determined by considering the estimated coordinates of the first order simulated network listed in Tables (5.2.2) as fixed stochastic constraints. The *static-dynamic* approach was then used to densify the first order network by intercalating into it second and third order points giving results for first level densification (cf. section 5.2.2.1) and second level densification (cf. section 5.2.2.2).

5.2.2.1 First Level Densification

In the first level simulated network densification, first order points 1, 2 and 3 were considered as fixed stochastic parameters while second order points 4, 5 and 6 were considered as new points whose coordinates were to be estimated (cf. Figure (4.3)). The observation data sets in Table (4.4) and the approximate coordinates in Table (4.3) were used resulting in parameters listed in Table (5.2.3) and Table (5.2.4) below while error ellipses are given diagrammatically in Figure (5.2).



Table 5.2.3: Coordinate Corrections and Stochastic Parameters-First Level Simulated Network -Static-Dynamic Approach

| POINT | <u>Δ</u> N (m) | Δ <i>E</i> (m) | σ _N (m) | σ _£ (m) | σ _{max} (m) | σ_{min} (m) | o | α, | w |
|-------|-------------------|-------------------|-----------------------|-----------------------|-------------------------|--------------------|-----|----|------|
| 1 | 0.0000 | 0.0000 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 60 | 0 | 0.1 |
| 2 | 0.0000 | 0.0000 | 0.0036 | 0.0025 | 0.0036 | 0.0025 | 0 | 0 | 0 |
| 3 | 0.0000 | 0.0000 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 297 | 59 | 59.9 |
| 4 | -0.1537 | 0.0678 | 0.0043 | 0.0036 | 0.0046 | 0.0033 | 302 | 54 | 21.1 |
| 5 | -0.1552 | 0.0845 | 0.0043 | 0.0036 | 0.0046 | 0.0033 | 57 | 05 | 12.4 |
| 6 | 0.0626 | 0.0487 | 0.0031 | 0.0046 | 0.0046 | 0.0032 | 00 | 01 | 05.1 |

 $\overline{\sigma}_{N} = 0.003541$ $\overline{\sigma}_{E} = 0.003570$ $\overline{\sigma}_{C} = 0.003555$ $\overline{\sigma}_{0}^{2} = 1.004263$

Table 5.2.4: Estimated Coordinates-First Level Simulated Network Densification -Static-Dynamic Approach

| POINT | PRCVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|------------|------------|
| | N (m) | E (m) | N (m) | E (m) |
| 1 | 99.9956 | 99.9971 | 99.9956 | 99.9971 |
| 2 | 446.4087 | 300.0064 | 446.4087 | 300.0064 |
| 3 | 100.0057 | 499.9965 | 100.0057 | 499.9965 |
| 4 | 273.0500 | 200.0700 | 272.8964 | 200.1378 |
| 5 | 273.0500 | 400.0900 | 272.8948 | 400.1745 |
| 6 | 100.3600 | 300.0500 | 100.1226 | 300.0987 |

5.2.2.2 Second Level Densification

In the second level simulated network densification, first order points 1, 2, 3 and second order points 4, 5, 6 were considered as fixed stochastic parameters while third order points 7 to 15 were considered as new points whose coordinates were to be estimated (cf. Figure (4.4)). The observation data sets in Table (4.6) and the approximate coordinates in Table (4.5a) were used resulting in parameters listed in Table (5.2.5) and Table (5.2.6) below while error ellipses are given diagrammatically in Figure (5.3).



ŝ

| POINT | <u>Δ</u> N (m) | ΔE (m) | σ_N (m) | σ_E (m) | σ_{max} (m) | σ_{mn} (m) | 0 | ά | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |
|---|---|--|---|---|---|---|--|---|--|
| 1 2 3 4 5 6 7 8 9 10 11 | (m) 0.0000 0.0000 0.0000 0.0000 0.0000 0.0157 0.0385 0.0531 0.0947 0.0974 | (m) 0.0000 0.0000 0.0000 0.0000 0.0000 -0.0891 -0.0934 -0.0776 -0.0534 -0.0630 | (m) 0.0028 0.0036 0.0028 0.0043 0.0043 0.0031 0.0019 0.0024 0.0020 0.0026 0.0026 | (m) 0.0034 0.0025 0.0034 0.0036 0.0036 0.0046 0.0025 0.0023 0.0020 0.0020 0.0020 | (m) 0.0036 0.0036 0.0046 0.0046 0.0046 0.0026 0.0026 0.0021 0.0027 0.0027 0.0027 | (m) 0.0025 0.0025 0.0033 0.0033 0.0032 0.0019 0.0021 0.0020 0.0020 0.0020 | 60 361 5 298 5 302 5 57 0 00 0 21 0 83 3 37 1 338 5 21 0 | 00 39 6 39 5 4 2 5 1 01 0 9 1 8 1 4 5 8 2 2 1 | 0.1 0.0 9.9 1.1 2.4 95.1 8.8 8.6 4.5 3.1 7.6 |
| 12 13 14 | 0.1031 0.0492 0.0049 0.0587 | -0.0645 -0.0182 -0.0398 -0.0641 | 0.0021 0.0023 0.0019 0.0020 | 0.0019 0.0023 0.0025 0.0020 | 0.0022 0.0026 0.0026 0.0021 | 0.0020 | 359 5 276 0 333 2 323 0 | 5 3 3 2 5 2 | 9.8 3.1 1.1 |

Table 5.2.5:Coordinate Corrections and Stochastic Parameters-Second Level Simulated Network -Static-Dynamic Approach

 $\overline{\sigma}_{e} = 0.002822$ $\overline{\sigma}_{e} = 0.002818$ $\overline{\sigma}_{c} = 0.002820$ $\hat{\sigma}_{0}^{2} = 1.006233$

| Table 5.2.6 | Estimated | Coordinates- | Second | Level | Simulated | Network | Densification |
|-------------|------------|--------------|--------|-------|-----------|---------|---------------|
| | -Static-Dy | namic Appro | ach | | | | |

| Pt. | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-----|-------------|-------------|------------|------------|
| | N (m) | E (m) | N (m) | E (m) |
| 1 | 99.9956 | 99.9971 | 99.9956 | 99.9971 |
| 2 | 446.4087 | 300.0064 | 446.4087 | 300.0064 |
| 3 | 100.0057 | 499.9965 | 100.0057 | 499.9965 |
| 4 | 272.8964 | 200.1378 | 272.8964 | 200.1378 |
| 5 | 272.8948 | 400.1745 | 272.8948 | 400.1745 |
| 6 | 100.1226 | 300.0987 | 100.1226 | 300.0987 |
| 7 | 100.0000 | 200.0000 | 100.0157 | 199.9109 |
| 8 | 186.6000 | 150.0000 | 186.6385 | 149.9056 |
| 9 | 186.6020 | 250.0000 | 186.6551 | 249.9224 |
| 10 | 359.8080 | 250.0000 | 359.9027 | 249.9466 |
| 11 | 359.8080 | 350.0000 | 359.9054 | 349.9370 |
| 12 | 273.2050 | 300.0000 | 273.3081 | 299.9355 |
| 13 | 186.6020 | 450.0000 | 186.6512 | 449.9818 |
| 14 | 100.0000 | 400.0000 | 100.0049 | 399.9602 |
| 15 | 186.6020 | 350.0000 | 186.6607 | 349.9359 |



5.2.3 Sub-Optimal Fusion Densification

The results presented in this section were determined by considering the estimated coordinates of the first order simulated network listed in Tables (5.2.2) as fixed stochastic constraints. The *sub-optimal fusion* approach was then used to densify the first order network by intercalating on to the network second and third order points giving results for first level densification {cf. section (5.2.3.1)} and second level densification {cf. section (5.2.3.2)}.

5.2.3.1 First Level Densification

In the first level simulated network densification, first order points 1, 2, 3 were considered as fixed stochastic parameters while second order points 4, 5, 6 were considered as new points whose coordinates were to be estimated (cf. Figure (4.3)). The observation data sets in Table (4.4) and the approximate coordinates in Table (4.3) were used resulting in parameters listed in Table (5.2.7) and Table (5.2.8) below while error ellipses are given diagrammatically in Figure (5.4).

Table 5.2.7:Coordinate Corrections and Stochastic Parameters-First Level Simulated Network -Sub-Optimal Fusion Approach

| POINT | <u>Δ</u> N (m) | ΔE (m) | σ_N (m) | σ_{E} (m) | σ_{max} (m) | σ_{mun} (m) | | α | " |
|-------|-------------------|-------------------|----------------|------------------|--------------------|--------------------|-----|----|------|
| 1 | 0.0000 | 0.0000 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 60 | 0 | 0.1 |
| 2 | 0.0000 | 0.0000 | 0.0036 | 0.0025 | 0.0036 | 0.0025 | 362 | 59 | 60.0 |
| 3 | 0.0000 | 0.0000 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 299 | 59 | 59.9 |
| 4 | -0.1691 | 0.0852 | 0.0048 | 0.0040 | 0.0050 | 0.0036 | 30% | 54 | 21.1 |
| 5 | -0.1705 | 0.0617 | 0.0048 | 0.0040 | 0.0050 | 0.0036 | 57 | 05 | 12.4 |
| 6 | 0.0819 | 0.0460 | 0.0035 | 0.0051 | 0.0050 | 0.0035 | 00 | 01 | 05.1 |

 $\bar{\sigma}_{v} = 0.003807$ $\bar{\sigma}_{e} = 0.003816$ $\bar{\sigma}_{e} = 0.003812$ $\hat{\sigma}_{0}^{2} = 1.003253$

 Table 5.2.8: Estimated Coordinates- First Level Simulated Network Densification

 -Sub-Optimal Fusion Approach

| POINT | PROVISIONAL | COORDINATES | ADJUSTED COORDINATES | | | | |
|-------|-------------|-------------|----------------------|----------|--|--|--|
| - | <u>N(m)</u> | E(m) | N (m) | E(m) | | | |
| 2 | 99.9956 | 99.9971 | 99.9956 | 99.9971 | | | |
| 2 | 446.4087 | 300.0064 | 446.4087 | 300.0064 | | | |
| | 100.0057 | 499.9965 | 100.0057 | 499.9965 | | | |
| 5 | 273.0500 | 200.0700 | 272.8809 | 200.1552 | | | |
| 6 | 273.0500 | 400.0900 | 272.8795 | 400.1517 | | | |
| | 100.0600 | 300.0500 | 100.1419 | 300.0960 | | | |



In the second level simulated network densification, first order points 1, 2, 3 and second order points 4, 5, 6 were considered as fixed stochastic parameters while third order points 7 to 15 were considered as new points whose coordinates were to be estimated {cf. Figure (4.4)}. The observation data sets in Table (4.6) and the approximate coordinates in Table (4.5b) were used resulting in parameters listed in Table (5.2.9) and Table (5.2.10) below while error ellipses are given diagrammatically in Figure (5.5).

Table 5.2.9:Coordinate Corrections and Stochastic Parameters-Second Level Simulated Network -Sub-Optimal Fusion Approach

| POINT | ΔN | ΔE | σ_N | σ_{E} | $\sigma_{\rm max}$ | σ_{mun} | 0 | α | - |
|--------|------------|------------|------------|--------------|--------------------|----------------|-----|----|------|
| | (111) | (10) | (m) | (m) | (m) | (m) | | | |
| 1 | 0.0000 | 0.0000 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 60 | 0 | 0.1 |
| 2 | 0.0000 | 0.0000 | 0.0036 | 0.0025 | 0.0036 | 0.0025 | 03 | 0 | 0 |
| 3 | 0.0000 | 0.0000 | 0.0028 | 0.0034 | 0.0036 | 0.0025 | 300 | 59 | 59.9 |
| 4 | 0.0000 | 0.0000 | 0.0048 | 0.0040 | 0.0050 | 0.0036 | 302 | 54 | 21.1 |
| 5 | 0.0000 | 0.0000 | 0.0048 | 0.0040 | 0.0050 | 0.0036 | 57 | 05 | 12.4 |
| 6 | 0.0000 | 0.0000 | 0.0035 | 0.0051 | 0.0051 | 0.0035 | 01 | 01 | 05.1 |
| 7 | 0.0232 | -0.1308 | 0.0023 | 0.0030 | 0.0030 | 0.0023 | 21 | 39 | 18.8 |
| 8 | 0.0574 | -0.1359 | 0.0027 | 0.0028 | 0.0030 | 0.0024 | 83 | 38 | 18.6 |
| 9 | 0.0770 | -0.1156 | 0.0024 | 0.0024 | 0.0024 | 0.0023 | 37 | 14 | 54.5 |
| 10 | 0.1403 | -0.0776 | 0.0031 | 0.0024 | 0.0031 | 0.0023 | 338 | 58 | 23.1 |
| 11 | 0.1447 | -0.0934 | 0.0031 | 0.0024 | 0.0031 | 0.0023 | 21 | 10 | 27.6 |
| 12 | 0.1550 | -0.0943 | 0.0026 | 0.0023 | 0.0025 | 0.0023 | 359 | 58 | 10.0 |
| 13 | 0.0722 | -0.0264 | 0.0027 | 0.0028 | 0.0030 | 0.0024 | 276 | 03 | 59.8 |
| 14 | 0.0055 | -0.0566 | 0.0023 | 0.0030 | 0.0030 | 0.0028 | 333 | 23 | 23.1 |
| 15 | 0.0855 | -0.0916 | 0.0024 | 0.0024 | 0.0024 | 0.0023 | 323 | 05 | 21.1 |
| = -0.0 | 02150 - | -0.00216 | 6 0.0 | 02157 | -1.00401 | 7 | | | |

 $\bar{\sigma}_{v} = 0.003158$ $\bar{\sigma}_{e} = 0.003156$ $\bar{\sigma}_{c} = 0.003157$ $\hat{\sigma}_{0}^{2} = 1.004917$

| Table 5.2.10: | Estimated Coordinates- | Second Level | Simulated | Network | Densification |
|---------------|------------------------|--------------|-----------|---------|---------------|
| | -Sub-Optimal Fusion A | pproach | | | |

| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|------------|------------|
| _ | N (m) | E(m) | N (m) | E(m) |
| 1 | 99.9956 | 99.9971 | 99.9956 | 99.9971 |
| 2 | 446.4087 | 300.0064 | 446.4087 | 300.0064 |
| 3 | 100.0057 | 499.9965 | 100.0057 | 499.9965 |
| 4 | 272.8809 | 200.1552 | 272.8809 | 200.1552 |
| 5 | 272.8795 | 400.1517 | 272.8795 | 400.1517 |
| 6 | 100.1419 | 300.0960 | 100.1419 | 300.0960 |
| 1 | 100.0000 | 200.0000 | 100.0232 | 199.8692 |
| 0 | 186.6000 | 150.0000 | 186.6574 | 149.8641 |
| 10 | 186.6020 | 250.0000 | 186.6790 | 249.8844 |
| 10 | 359.8080 | 250.0000 | 359.9483 | 249.9224 |
| 110 | 359.8080 | 350.0000 | 359.9527 | 349.9066 |
| 12 | 273.2050 | 300.0000 | 273.3600 | 299.9057 |
| | 186.6020 | 450.0000 | 186.6742 | 449.9736 |
| 15 | 100.0000 | 400.0000 | 100.0055 | 399.9434 |
| | 186.6020 | 350.0000 | 186.6875 | 349.9084 |





5.2.4 Dynamic Densification

The results presented in this section were determined by considering the estimated coordinates of the first order simulated network listed in Table (5.2.2) as stochastic constraints. The *dynamic* approach was then used to densify the first order network by intercalating on to the network second and third order points giving results for first level densification {c.f. section (5.2.4.1)} and second level densification {c.f. section (5.2.4.2)}.

5.2.4.1 First Level Densification

In the first level simulated network densification, all points 1 to 6 were considered as stochastic parameters with all the points being estimated afresh including the datum points 1, 2, 3. (cf. Figure (4.3)). The observation data sets in Table (4.4) and the approximate coordinates in Table (4.3) were used resulting in parameters listed in Table (5.2.11) and Table (5.2.12) below while error ellipses are given diagrammatically in Figure (5.6).

 Table 5.2.11: Coordinate Corrections and Stochastic Parameters-First Level Simulated Network

 -Dynamic Approach

| POINT | ΔN (m) | ΔE (m) | $\sigma_{_N}$ (m) | $\sigma_{_E}$ (m) | σ_{max} (m) | σ_{min} (m) | = | à | ** |
|-------|-----------|----------------|-------------------|-------------------|--------------------|--------------------|-----|----|------|
| 1 | 0.0095 | 0.0208 | 0.0029 | 0.0036 | 0.0036 | 0.0029 | 60 | 0 | 0.1 |
| 2 | -0.0264 | -0.0039 | 0.0039 | 0.0026 | 0.0039 | 0.0026 | 364 | 59 | 50.0 |
| 3 | 0.0059 | -0.0190 | 0.0029 | 0.0036 | 0.0036 | 0.0029 | 301 | 59 | 59.9 |
| 4 | -0.1691 | 0.0852 | 0.0055 | 0.0046 | 0.0059 | 0.0041 | 302 | 54 | 21.1 |
| 5 | -0.1705 | 0.0617 | 0.0055 | 0.0046 | 0.0059 | 0.0041 | 57 | 05 | 12.4 |
| 6 | 0.0819 | 0.0460 | C.0040 | 0.0058 | 0.0058 | 0.0040 | 00 | 01 | 05.1 |
| | | | | | | | 40 | | |

 $\bar{\sigma}_{_{N}} = 0.004253$ $\bar{\sigma}_{_{E}} = 0.004255$ $\bar{\sigma}_{_{C}} = 0.004254$ $\hat{\sigma}_{_{0}}^{2} = 1.000725$

| Table 5.2.12: Estimated | Coordinates- H | First Level | Simulated | Network | Densification |
|-------------------------|----------------|-------------|-----------|---------|---------------|
| -Dynamic | Approach | | | | |

| POINT | PROVISIONAL | COCRDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|------------|------------|
| | N (m) | E(m) | N (m) | E (m) |
| | 99.9956 | 99.9971 | 100.0051 | 100.0179 |
| 2 | 446.4087 | 300.0064 | 446.3823 | 300.0025 |
| 3 | 100.0057 | 499.9965 | 100.0116 | 499.9775 |
| 4 | 273.0500 | 200.0700 | 272.8809 | 200.1552 |
| 5 | 273.0500 | 400.0900 | 272.8795 | 400.1517 |
| 0 | 100.0600 | 300.0500 | 100.1419 | 300.0960 |



5.2.4.2 Second Level Densification

In the second level simulated network densification, first order points 1 to 15 were considered as stochastic parameters with all the points being estimated including the datum point 1 to 6. {cf. Figure (4.4)}. The observation data sets in Table (4.6) and the approximate coordinates in Table (4.5c) were used resulting in parameters listed in Table (5.2.13) and Table (5.2.14) below while error ellipses are given diagrammatically in Figure (5.7).

| POINT | <u>Δ</u> N (m) | ΔE (m) | $\sigma_N^{(m)}$ | σ_E (m) | σ_{max} (m) | σ_{min} (m) | | ά | " |
|-------|-------------------|----------------|------------------|----------------|--------------------|--------------------|-----|----|------|
| 1 | 0.0323 | 0.0973 | 0.0025 | 0.0032 | 0.0036 | 0.0025 | 60 | 0 | 0.1 |
| 2 | 0.0693 | 0.0564 | 0.0035 | 0.0022 | 0.0036 | 0.0025 | 03 | 0 | 0 |
| 3 | 0.0063 | 0.0034 | 0.0025 | 0.0032 | 0.0036 | 0.0025 | 302 | 59 | 59.9 |
| 4 | 0.1600 | 0.0338 | 0.0029 | 0.0026 | 0.0049 | 0.0035 | 302 | 54 | 21.1 |
| 5 | 0.1400 | 0.0645 | 0.0029 | 0.0026 | 0.0049 | 0.0035 | 57 | 05 | 12.4 |
| 6 | 0.1315 | 0.0109 | 0.0024 | 0.0029 | 0.0049 | 0.0034 | 02 | 01 | 05.1 |
| 7 | 0.0164 | -0.1374 | 0.0026 | 0.0034 | 0.0034 | 0.0026 | 21 | 39 | 18.8 |
| 8 | 0.0580 | -0.1468 | 0.0030 | 0.0031 | 0.0033 | 0.0027 | 83 | 38 | 18.6 |
| 9 | 0.0775 | -0.1180 | 0.0026 | 0.0027 | 0.0027 | 0.0026 | 37 | 14 | 54.5 |
| 10 | 0.1538 | -0.0802 | 0.0035 | 0.0027 | 0.0035 | 0.0026 | 338 | 58 | 23.1 |
| 11 | 0.1584 | -0.0878 | 0.0035 | 0.0027 | 0.0035 | 0.0026 | 21 | 10 | 27.6 |
| 12 | 0.1615 | -0.0931 | 0.0028 | 0.0026 | 0.0028 | 0.0026 | 359 | 58 | 10.0 |
| 13 | 0.0730 | -0.0143 | 0.0030 | 0.0031 | 0.0033 | 0.0027 | 276 | 03 | 59.8 |
| 14 | 0.0002 | -0.0483 | 0.0026 | 0.0034 | 0.0034 | 0.0025 | 333 | 23 | 23.1 |
| 15 | 0.0862 | -0.0871 | 0.0026 | 0.0027 | 0.0027 | 0.0026 | 323 | 05 | 21.1 |

 Table 5.2.13: Coordinate Corrections and Stochastic Parameters-Second Level Simulated

 Network-Dynamic Approach

 $\overline{\sigma}_{v} = 0.002883$ $\overline{\sigma}_{E} = 0.002893$ $\overline{\sigma}_{c} = 0.002888$ $\hat{\sigma}_{0} = 1.002717$

 Table 5.2.14: Estimated Coordinates- Second Level Simulated Network Densification

 -Dynamic Approach

| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|------------|------------|
| | N (m) | E (m) | N (m) | E (m) |
| 1 | 100.0051 | 100.0179 | 100.0374 | 99.9206 |
| 2 | 446.3823 | 300.0025 | 446.4516 | 299.9461 |
| 3 | 100.0116 | 499.9775 | 100.0179 | 499.9809 |
| 4 | 272.8809 | 200.1552 | 272.7209 | 200.1890 |
| 5 | 272.8795 | 400.1517 | 272.7395 | 400.2162 |
| 6 | 100.1419 | 300.0960 | 100.2734 | '300.0851 |
| | 100.0000 | 200.0000 | 100.0164 | 199.8626 |
| 0 | 186.6000 | 150.0000 | 186.6580 | 149.8532 |
| 10 | 186.6020 | 250.0000 | 186.6795 | 249.8820 |
| 11 | 359.8080 | 250.0000 | 359.9618 | 249.9198 |
| 12 | 359.8080 | 350.0000 | 359.9664 | 349.9122 |
| 12 | 273.2050 | 300.0000 | 273.3665 | 299.9069 |
| 114 | 186.6020 | 450.0000 v | 186.6750 | 449.9857 |
| 15 | 100.0000 | 400.0000 | 99.9998 | 399.9517 |
| | 186.6020 | 350.0000 | 186.6882 | 349.9129 |



5.2.5 Static Densification

The results presented in this section were determined by considering the estimated coordinates of the first order simulated network listed in Tables (5.2.2) as fixed non-stochastic entities. The *static* approach was then used to densify the first order networks by intercalating into them second and third order points giving results for first level densification {cf. section (5.2.5.1)} and second level densification {cf. section (5.2.5.2)}.

5.2.5.1 First Level Densification

In the first level simulated network densification, first order points 1, 2, 3 were considered as fixed non-stochastic parameters while second order points 4, 5, 6 were considered as new points whose coordinates were to be estimated (cf. Figure (4.3)). The observation data sets in Table (4.4) and the approximate coordinates in Table (4.3) were used resulting in parameters listed in Table (5.2.15) and Table (5.2.16) below while error ellipses are given diagrammatically in Figure (5.8).

Table 5.2.15: Coordinate Corrections and Stochastic Parameters-First Level Simulated Network -Static Approach

| POINT | <u>Δ</u> N (m) | ΔE (m) | σ_{v} | σ_{E} (m) | σ_{\max} (m) | σ_{min} (m) | 194 | α | |
|-------|-------------------|----------------|--------------|------------------|---------------------|--------------------|-----|----|------|
| 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | | 0 |
| 2 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | | 0 |
| 3 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 11 | | 0 |
| 4 | -0.1231 | 0.0538 | 0.0039 | 0.0031 | 0.0042 | 0.0026 | 299 | 58 | 11.4 |
| 5 | -0.1243 | 0.0671 | 0.0039 | 0.0031 | 0.0042 | 0.0026 | 60 | 01 | 27.3 |
| 6 | 0.0499 | 0.0385 | 0.0026 | 0.0042 | 0.0042 | 0:0026 | 00 | 00 | 40.4 |

 $\overline{\sigma}_{v} = 0.002489$ $\overline{\sigma}_{e} = 0.002476$ $\overline{\sigma}_{e} = 0.002484$ $\hat{\sigma}_{0}^{2} = 1.00400$

 Table 5.2.16: Estimated Coordinates- First Level Simulated Network Densification

 -Static Approach

| The second se | | | | | | |
|---|-------------|-------------|------------|------------|--|--|
| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES | | |
| - | N (m) | E (m) | N (m) | E (m) | | |
| 2 | 99.9956 | 99.9971 | 99.9956 | 99.9971 | | |
| 4 | 446.4087 | 300.0064 | 446.4087 | 300.0064 | | |
| 2 | 100.0057 | 499.9965 | 100.0057 | 499.9965 | | |
| 2 | 273.0500 | 200.0700 | 272.9269 | 200.1238 | | |
| 6 | 273.0500 | 400.0900 | 272.9257 | 400.1571 | | |
| | 100.0600 | 300.0500 | 100.1099 | 300.0885 | | |

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5.2.5.2 Second Level Densification

In the second level simulated network densification, first order points 1, 2, 3 and second order points 4, 5, 6 were considered as fixed non-stochastic parameters while third order points 7 to 15 were considered as new points whose coordinates were to be estimated (cf. Figure (4.4)). The observation data sets in Table (4.6) and the approximate coordinates in Table (4.5d) were used resulting in parameters listed in Table (5.2.13) and Table (5.2.14) below while error ellipses are given diagrammatically in Figure (5.9).

 Table 5.2.17: Coordinate Corrections and Stochastic Parameters-Second Level Simulated

 Network - Static Approach

| POINT | ΔΝ | ΔE | $\sigma_{\rm v}$ | σ_{r} | σ_{max} | σ_{mn} | 0 | : |
|-------------------------------|---------|------------|--------------------------------|-------------------------------|----------------|---------------|--------|------|
| | (m) | (m) | (m) | (m) | (m) | (m) | ° , | " |
| 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 | |
| 2 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 | |
| 3 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 | |
| 4 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 | |
| 5 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 | |
| 6 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 | Ì |
| 7 | 0.0277 | -0.1129 | 0.0013 | 0.0020 | 0.0020 | 0.0013 | 09 07 | 52.9 |
| 8 | 0.0304 | -0.1136 | 0.0018 | 0.0015 | 0.0020 | 0.0012 | 290 46 | 26.5 |
| 9 | 0.0642 | -0.0937 | 0.0014 | 0.0013 | 0.0014 | 0.0012 | 60 25 | 00.2 |
| 10 | 0.1465 | -0.0367 | 0.0019 | 0.0014 | 0.0020 | 0.0013 | 309 14 | 21.4 |
| 11 | 0.1516 | -0.0915 | 0.0019 | 0.0014 | 0.0020 | 0.0013 | 50 55 | 08.4 |
| 12 | 0.1957 | -0.0733 | 0.0012 | 0.0014 | 0.0014 | 0.0012 | 359 57 | 27.9 |
| 13 | 0.0503 | -0.0121 | 0.0018 | 0.0015 | 0.0020 | 0.0012 | 69 00 | 07.6 |
| 14 | -0.0338 | -0.0368 | 0.0013 | 0.0020 | 0.0020 | 0.0012 | 350 55 | 41.6 |
| 15 | 0.0759 | -0.0739 | 0.0014 | 0.0013 | 0.0014 | 0.0012 | 299 28 | 22.2 |
| $\overline{\sigma}_{v} = 0.0$ | 01223 0 | = 0.00120 | $4 \overline{\sigma}_c = 0.00$ | $01214 + \hat{\sigma}_0^{-2}$ | =1.002736 | 5 | 11 | |

Table 5.2.18: Estimated Coordinates- Second Level Simulated Network Densification -Static Approach

| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|------------|------------|
| - | N (m) | E (m) | N (m) | E (m) |
| 1 | 99.9956 | 99.9971 | 99.9956 | 99.9971 |
| 2 | 446.4087 | 300.0064 | 446.4087 | 300.0064 |
| 3 | 100.0057 | 499.9965 | 100.0057 | 499.9965 - |
| 4 | 272.9269 | 200.1238 | 272.9269 | 200.1238 |
| 5 | 272.9257 | 400.1571 | 272.9257 | 400.1571 |
| 0 | 100.1099 | 300.0885 | 100.1099 | 300.0885 |
| 1 | 100.0000 | 200.0000 | 99.9723 | 199.8871 |
| 0 | 186.6000 | 150.0000 | 186.6304 | 149.8864 |
| 3 | 186.6020 | 250.0000 | 186.6662 | 249.9063 |
| 11 | 359.8080 | 250.0000 | 359.9545 | 249.9633 |
| 10 | 359.8080 | 350.0000 | 359.9596 | 349.9085 |
| 12 | 273.2050 | 300.0000 | 273.4007 | 299.9267 |
| 14 | 186.6020 | 450.0000 | 186.6523 | 449.9879 |
| 15 | 100.0000 | 400.0000 | 99.9662 | 399.9632 |
| | 186.6020 | 350.0000 | 186.6779 | 349.9261 |





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5.2.6 Computed Shifts

The final coordinates obtained from the static-dynamic, sub-optimal Fusion, dynamic and static densifications were compared to each other and the results tabulated as shown in Table (5.2.19). Figures (5.10 to 5.15) depict these shifts graphically. In the Tables, δ is the magnitude of the shift in the two sets of coordinates for each point while α is the bearing of the shift. Also, $\overline{\delta}$ and $\overline{\alpha}$ are the mean of δ and α for the respective densification approaches.

| | Static-Dynamic | Static-Dynamic | Static-Dynamic | Sub-Optimal | Sub-Optimal | Dynamic |
|-----|--------------------------------|--------------------------------|--------------------------------|------------------------------|-----------------------------|------------------------------|
| | and | and | and | and | and | and |
| | Sub-Optimal | Dynamic | Static | Dynamic | Static | Static |
| St | δα | δα | δα | δα | δα | δα |
| | (mm) (° ') | (mm) (° ') | (mm) (° ') | (mm) (° | (mm) (°') | (mm) (° °) |
| | | | | .) | | |
| 1 | 0 0 | 87.2 118 39 | 0 0 | 87.2 118 39 | 0 0 | 81.5 239 09 |
| 2 | 0 0 | 74.0 125 26 | 0 0 | 74.0 125 26 | 0 0 | 74.0 305 26 |
| 3 | 0 0 | 19.8 128 02 | 0 0 | 19.8 128 02 | 0 0 | 19.8 308 02 |
| 4 | 24.2 134 10 | 0.8 343 44 | 33.6 155 21 | 163.5 348 4 | 55.7 145 41 | 216.1 162 25 |
| 5 | 27.3 236 39 | 160.8 344 58 | 35.5 150 36 | 154.1 335 16 | 46.5 186 40 | 195.3 16 23 |
| 6 | 19.5 352 02 | 151.4 174 51 | 16.3 38 46 | 131.9 175 16 | 32.9 13 11 | 163.5 358 48 |
| 7 | 42.4 280 12 | 48.3 90 50 | 49.5 28 44 | 9.5 44 09 | 54.0 340 37 | 50.4 330 57 |
| 8 | 46.5 293 58 | 56.8 110 04 | 21.8 68 09 | 10.9 93 09 | 35.0 320 27 | 43.2 309 44 |
| 9 | 44.9 302 10 | 47.2 121 08 | 19.6 124 35 | 2.5 101 46 | 25.4 300 18 | 27.7 298 42 |
| 10 | 51.6 332 03 | 64.9 155 36 | 54.4 197 52 | 13.7 169 06 | 41.4 261 23 | 44.1 279 32 |
| 11 | 56.2 327 16 | 65.8 157 53 | 61.2 152 16 | 14.8 202 14 | 7.2 195 24 | 7.7 28 33 |
| 12 | 59.8 330 08 | 65.0 153 54 | 93.0 174 34 | 6.6 190 28 | 45.8 207 18 | |
| 13 | 24.4 340 23 | 24.1 189 18 | 6.2 100 13 | 12.1 266 13 | 26.2 326 51 🖇 | 22.8 354 28 |
| 14 | 16.8 272 03 | 9.9 59 02 | 38.8 355 34 | 10.1 304 29 | 44.0 333 16 | 35.5 341 06 |
| 15 | 38 + 31 + 16 | 35.9 140 05 | 19.8 150 20 | 4.6 261 09 | 20.1 298 28 | 16.7 307 58 |
| Mea | $n \overline{\delta} = 37.7$ | $\delta = 60.8$ | $\delta = 37.5$ | $\delta = 47.7$ | $\overline{\delta} = 36.2$ | $\overline{\delta} = 69.2$ |
| - | $\overline{\alpha} = 275 \ 20$ | $\overline{\alpha} = 268 \ 32$ | $\overline{\alpha} = 253 \ 00$ | $\overline{\alpha} = 343$ 26 | $\overline{\alpha}$ = 49 34 | $\overline{\alpha}$ = 253 17 |

 Table 5.2.19: Shifts between estimated parameters for the Experiments (Simulated Network)



static-dynamic approach





Figure 5.12: Coordinate shifts of static approach with respect to static-dynamic approach



sub-optimal fusion approach

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dynamic approach

5.3 The Real Network

5.3.1 First Order Network Adjustment

The results presented in this section were obtained by adjusting the real first order network through the free network technique using the approximate coordinates listed in Table (4.7) and observation data sets listed in Table (4.8). This formed the fundamental network on which the real first level and real second level densifications were performed. The resulting error ellipses are presented diagrammatically in Figure (5.16).

Table 5.3.1: Coordinate Corrections and Stochastic Parameters-First Order Real Network

| POINT | ΔN | ΔE | $\sigma_{\rm v}$ | $\sigma_{\scriptscriptstyle E}$ | $\sigma_{_{ m max}}$ | σ_{mun} | | α | |
|-------|------------|------------|------------------|---------------------------------|----------------------|----------------|-----|-----|------|
| | (m) | (m) | (m) | (m) | (m) | (m) | | ``` | " |
| 1 | -0.1003 | 0.0389 | 0.0166 | 0.0125 | 0.0169 | 0.0121 | 29 | 21 | 57.1 |
| 2 | 0.0214 | 0.0328 | 0.0109 | 0.0119 | 0.0126 | 0.0100 | 291 | 58 | 8.1 |
| 3 | 0.0393 | -0.0698 | 0.0099 | 0.0093 | 0.0105 | 0.0086 | 71 | 14 | 37.2 |
| 4 | 0.0420 | -0.0009 | 0.0083 | 0.0093 | 0.0095 | 0.0080 | 309 | 20 | 32.9 |
| 5 | 0.0068 | -0.0961 | 0.0074 | 0.0082 | 0.0087 | 0.0069 | 303 | 40 | 52.7 |
| 6 | -0.0310 | 0.0077 | 0.0075 | 0.0091 | 0.0093 | 0.0073 | 319 | 09 | 10.3 |
| 7 | 0.0438 | 0.0159 | 0.0072 | 0.0075 | 0.0077 | 0.0070 | 290 | 17 | 24.7 |
| 8 | -0.0329 | -0.0437 | 0.0057 | 0.0070 | 0.0070 | 0.0057 | 352 | 25 | 4.2 |
| 9 | 0.0314 | 0.0305 | 0.0078 | 0.0073 | 0.0078 | 0.0073 | 353 | 35 | 36.1 |
| 10 | 0.0596 | 0.0399 | 0.0071 | 0.0067 | 0.0071 | 0.0067 | 01 | 58 | 46.1 |
| 11 | -0.0802 | 0.0448 | 0.0085 | 0.0078 | 0.0090 | 0.0072 | 68 | 12 | 59.1 |

1

$\bar{\sigma}_{v} = 0.00880$ $\bar{\sigma}_{z} = 0.00878$ $\bar{\sigma}_{c} = 0.00879$ $\hat{\sigma}_{0}^{2} = 1.003744$

| POINT | PROVISIONAL | COORDINATES | ADJUSTED | COORDINATES | |
|------------------|-------------|-------------|-------------|-------------|--|
| | N (m.) | E (m) | N (m) | E (m) | |
| 1 | 9583105.104 | 513215.911 | 9583105.004 | 513215.950 | |
| 2 3 4 5 | 9576179.214 | 574648.574 | 9576179.235 | 574648.607 | |
| | 9600981.179 | 569530.645 | 9600981.218 | 569580.575 | |
| | 9599052.465 | 594885.489 | 9599052.507 | 594885.488 | |
| | 9611665.689 | 589503.327 | 9611665.696 | 589503.231 | |
| 6 | 9624778.596 | 606329.877 | 9624778.565 | 606329.885 | |
| 1 | 9640229.659 | 580192.061 | 9640229.703 | 580182.077 | |
| 0 | 9644287.319 | 609203.330 | 9644287.286 | 609203.286 | |
| 10 | 9661267.194 | 585576.660 | 9661267.225 | 585576.691 | |
| | 9660984.693 | 598816.071 | 9660984.753 | 598816.111 | |
| 11 | 9661696.939 | 618181.173 | 9661696.859 | 618181.218 | |

 Table 5.3.2: Estimated Coordinates-First Order Real Network



Figure 5.16: Point error ellipses -first order real network

5.3.2 Static-Dynamic Densification

The results presented in this section were determined by considering the estimated coordinates of the first order real network listed in Tables (5.3.2) as fixed stochastic constraints. The *static-dynamic* approach was then used to densify the first order network by intercalating into it second and third order points giving results for first level densification (cf. section 5.3.2.1) and second level densification (cf. section 5.3.2.2).

5.3.2.1 First Level Densification

In the first level real network densification, first order points 1 through 11 were considered as fixed stochastic parameters while second order points 12 through 26 were considered as new points whose coordinates were to be estimated (cf. Figure (4.6)). The observation data sets in Table (4.10) and the approximate coordinates in Table (4.9) were used resulting in parameters listed in Table (5.3.3) and Table (5.3.4) below while error ellipses are given diagrammatically in Figure (5.17).

| POINT | <u>Δ</u> N (m) | <u>Δ</u> <i>E</i> (m) | σ _{.v} (m) | σ_{E} (m) | σ_{max} (m) | σ_{min} (m) | ο α |
|--|---|--|--|---|--|--|--|
| 1 2 3 4 5 6 7 8 9 | (m) 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 | (m) 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 | (m) 0.0166 0.0109 0.0099 0.0083 0.0074 0.0075 0.0072 0.0072 0.0072 | (m) 0.0125 0.0119 0.0093 0.0093 0.0093 0.0082 0.0091 0.0075 0.0070 0.0073 | (m) 0.0169 0.0126 0.0105 0.0095 0.0087 0.0093 0.0077 0.0070 0.0078 | (m) 0.0121 0.0100 0.0086 0.0080 0.0069 0.0073 0.0070 0.0057 0.0057 | 29 21 57.1 291 58 8.1 74 14 37.2 310 20 32.9 304 40 52.7 319 9 10.3 290 17 24.7 352 25 4.2 353 35 36.1 |
| 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 | 0.0000 0.0000 -0.0154 0.0214 -0.0680 -0.0189 -0.0509 0.0453 0.0382 -0.1701 | 0.0000 0.0000 0.0333 0.0152 -0.0347 -0.0296 0.0724 0.0162 -0.1063 -0.1703 | 0.0071 0.0085 0.0145 0.0336 0.0361 0.0201 0.0179 0.0212 0.0233 0.0397 | 0.0067 0.0078 0.0255 0.0537 0.0188 0.0432 0.0176 0.0531 0.0242 0.0303 | 0.0071 0.0090 0.0259 0.0605 0.0361 0.0445 0.0200 0.0533 0.0258 0.0428 | 0.0067 0.0072 0.0137 0.0186 0.0188 0.0167 0.0150 0.0206 0.0216 0.0256 | 01 58 46.1 68 12 59.1 336 19 44.5 58 02 31.8 05 05 58.4 328 40 22.2 85 28 52.6 11 12 15.0 282 57 17.3 55 35 22.0 |
| | -0.0131 0.0585 -0.0856 0.0880 -0.2337 -0.2501 -0.2443 | -0.1671 -0.2382 0.0201 0.0905 -0.2025 -0.0828 -0.1778 | 0.0202 0.0182 0.0204 0.0218 0.0203 0.02414 0.0348 | 0.0241 0.0235 0.0366 0.0390 0.0183 0.0215 0.0195 | 0.0248 0.0250 0.0385 0.0403 0.0203 0.0413 0.0355 | 0.0193 0.0163 0.0166 0.0194 0.0183 0.0215 0.0182 | 44 09 40.3 51 48 14.8 320 13 12.4 327 26 08.2 351 35 15.5 359 28 03.5 27 08 07.5 |

 Table 5.3.3: Coordinate Corrections and Stochastic Parameters-First Level Real Network

 -Static-Dynamic Approach



static-dynamic approach

8 ,
$\overline{\sigma}_{v} = 0.02134$ $\overline{\sigma}_{E} = 0.02515$ $\overline{\sigma}_{C} = 0.02332$ $\hat{\sigma}_{0}^{2} = 1.009214$

| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|-------------|------------|
| | N (m) | E (m) | N (m) | E (m) |
| 1 | 9583105.004 | 513215.950 | 9583105.004 | 513215.950 |
| 2 | 9576179.235 | 574648.607 | 9576179.235 | 574648.607 |
| 3 | 9600981.218 | 569580.575 | 9600981.218 | 569580.575 |
| 4 | 9599052.507 | 594885.488 | 9599052.507 | 594885.488 |
| 5 | 9611665.696 | 589503.231 | 9611665.696 | 589503.231 |
| 6 | 9624778.565 | 606329.885 | 9624778.565 | 606329.885 |
| 7 | 9640229.703 | 580182.077 | 9640229.703 | 580182.077 |
| 8 | 9644287.286 | 609203.286 | 9644287.286 | 609203.286 |
| 9 | 9661267.225 | 585576.691 | 9661267.225 | 585576.691 |
| 10 | 9660984.753 | 598816.111 | 9660984.753 | 598816.111 |
| 11 | 9661696.859 | 618181.218 | 9661696.859 | 618181.218 |
| 12 | 9651426.870 | 578082.210 | 9651426.855 | 578082.243 |
| 13 | 9649302.660 | 592482.850 | 9649302.681 | 592482.865 |
| 14 | 9640093.640 | 625611.430 | 9640093.572 | 625611.395 |
| 15 | 9614609.390 | 603055.440 | 9614609.371 | 603055.410 |
| 16 | 9626055.670 | 593121.870 | 9626055.619 | 593121.942 |
| 17 | 9623694.380 | 582449.870 | 9623694.425 | 582449.886 |
| 18 | 9625643.250 | 561292.670 | 9625543.288 | 561292.564 |
| 19 | 9607749.860 | 545064.590 | 9607749.690 | 545064.420 |
| 20 | 9610759.110 | 559563.590 | 9610759.097 | 559563.423 |
| 21 | 9609410.820 | 563591.710 | 9609410.878 | 563591.472 |
| 22 | 9592183.630 | 576550.570 | 9592183.544 | 576550.590 |
| 23 | 9584543.130 | 589735.740 | 9584543.218 | 589735.830 |
| 24 | 9585354.590 | 561756.300 | 9585354.356 | 561756.098 |
| 25 | 9580752.500 | 538526.380 | 9580752.250 | 538526.297 |
| 26 | 9589557.530 | 528224,190 | 9589557.286 | 528224.012 |

Table 5.3.4: Estimated Coordinates- First Level Real Network Densification -Static-Dynamic Approach

5.3.2.2 Second Level Densification

In the Second level real network densification, first order points 1 through 11 and second order points 12 through 26 were considered as fixed stochastic parameters while third order points 27 through 41 were considered as new points whose coordinates were to be estimated (cf. Figure (4 7)). The observation data sets in Table (4.12) and the approximate coordinates in Table (4 11a) were used resulting in parameters listed in Table (5.3.5) and Table (5.3.6) below while error ellipses are given diagrammatically in Figure (5.18).

| PCINT | ΔΝ | ΔΕ | $\sigma_{\rm v}$ | σ_{E} | $\sigma_{\rm max}$ | σ_{mn} | α |
|-------|---------|---------|------------------|--------------|--------------------|---------------|-------------|
| | (m) | (m) | (m) | (m) | (m) | (m) | 0 |
| | | | | | | | " |
| 1 | 0.0000 | 0.0000 | 0.0166 | 0.0125 | 0.0169 | 0.0121 | 29 21 57.1 |
| 2 | 0.0000 | 0.0000 | 0.0109 | 0.0119 | 0.0126 | 0.0100 | 291 58 8.1 |
| 3 | 0.0000 | 0.0000 | 0.0099 | 0.0093 | 0.0105 | 0.0086 | 71 14 37.2 |
| 4 | 0.0000 | 0.0000 | 0.0083 | 0.0093 | 0.0095 | 0.0080 | 311 20 32.9 |
| 5 | 0.0000 | 0.0000 | 0.0074 | 0.0082 | 0.0087 | 0.0069 | 305 40 52.7 |
| 6 | 0.0000 | 0.0000 | 0.0075 | 0.0091 | 0.0093 | 0.0073 | 319 9 10.3 |
| 7 | 0.0000 | 0.0000 | 0.0072 | 0.0075 | 0.0077 | 0.0070 | 290 17 24.7 |
| 8 | 0.0000 | 0.0000 | 0.0057 | 0.0070 | 0.0070 | 0.0057 | 352 25 4.2 |
| 9 | 0.0000 | 0.0000 | 0.0078 | 0.0073 | 0.0078 | 0.0073 | 353 35 36.1 |
| 10 | 0.0000 | 0.0000 | 0.0071 | 0.0067 | 0.0071 | 0.0067 | 01 58 46.1 |
| 11 | 0.0000 | 0.0000 | 0.0085 | 0.0078 | 0.0090 | 0.0072 | 68 12 59.1 |
| 12 | 0.0000 | 0.0000 | 0.0145 | 0.0255 | 0.0259 | 0.0137 | 336 19 44.5 |
| 13 | 0.0000 | 0.0000 | 0.0336 | 0.0537 | 0.0605 | 0.0186 | 58 02 31.8 |
| 14 | 0.0000 | 0.0000 | 0.0361 | 0.0188 | 0.0361 | 0.0188 | 05 05 58.4 |
| 15 | 0.0000 | 0.0000 | 0.0201 | 0.0432 | 0.0445 | 0.0167 | 328 40 22.2 |
| 16 | 0.0000 | 0.0000 | 0.0179 | 0.0176 | 0.0200 | 0.0150 | 85 28 52.6 |
| 17 | 0.0000 | 0.0000 | 0.0212 | 0.0531 | 0.0533 | 0.0206 | 11 12 15.0 |
| 18 | 0.0000 | 0.0000 | 0.0233 | 0.0242 | 0.0258 | 0.0216 | 282 57 17.3 |
| 19 | 0.0000 | 0.0000 | 0.0397 | 0.0303 | 0.0428 | 0.0256 | 55 35 22.0 |
| 20 | 0.0000 | 0.0000 | 0.0202 | 0.0241 | 0.0248 | 0.0193 | 44 09 40.3 |
| 21 | 0.0000 | 0.0000 | 0.0182 | 0.0235 | 0.0250 | 0.0163 | 51 48 14.8 |
| 22 | 0.0000 | 0.0000 | 0.0204 | 0.0366 | 0.0385 | 0.0166 | 320 13 12.4 |
| 23 | 0.0000 | 0.0000 | 0.0218 | 0.0390 | 0.0403 | 0.0194 | 327 26 08.2 |
| 24 | 0.0000 | 0.0000 | 0.0203 | 0.0183 | 0.0203 | 0.0183 | 351 35 15.5 |
| 25 | 0.0000 | 0.0000 | 0.0414 | 0.0215 | 0.0413 | 0.0215 | 359 28 03.5 |
| 26 | 0.0000 | 0.0000 | 0.0348 | 0.0195 | 0.0355 | 0.0182 | 27 08 07.5 |
| 27 | -0.0087 | 0.0163 | 0.0277 | 0.0209 | 0.0277 | 0.0209 | 11 10 29.1 |
| 28 | -0.0114 | 0.0113 | 0.0282 | 0.0167 | 0.0282 | 0.0166 | 354 37 35.0 |
| 29 | -0.0145 | 0.0089 | 0.0169 | 0.0163 | 0.0185 | 0.0144 | 82 13 41.8 |
| 30 | 0.0005 | -0.0017 | 0.0320 | 0.0239 | 0.0320 | 0.0240 | 02 41 03.9 |
| 31 | -0.0054 | 0.0010 | 0.0183 | 0.0207 | 0.0243 | 0.0131 | 283 04 27.7 |
| 32 | 0.0009 | -0.0108 | 0.0220 | 0.0200 | 0.0259 | 0.0146 | //9 19 59./ |
| 33 | 0.0041 | -0.0032 | 0.0125 | 0.0142 | 0.0154 | 0.0110 | 69 14 07.4 |
| 34 | -0.0039 | -0.0036 | 0.)132 | 0.0210 | 0.0211 | 0.0130 | 348 24 05.9 |
| 35 | 0.0032 | 0.0139 | 0.0134 | 0.0171 | 0.0171 | 0.0134 | 08 43 13.2 |
| 30 | -0.0183 | 0.0151 | 0.0258 | 0.0197 | 0.0294 | 0.0138 | 65 42 31.4 |
| 37 | 0.0027 | 0.0180 | U.J126 | 0.0202 | 0.0206 | 0.0119 | 2/ 1/ 3/.2 |
| 30 | 0.0035 | 0.0019 | 0.0181 | 0.0126 | 0.0185 | 0.0120 | 32 50 51.4 |
| 40 | 0.0791 | -0.0208 | 0.0619 | 0.0211 | 0.0623 | 0.0200 | 13 23 18.9 |
| 40 | -0.0045 | -0.0335 | 0.0155 | 0.0399 | 0.0399 | 0.0154 | 01 03 11.8 |
| 41 | 0.0195 | 0.0088 | 0.0331 | 0.0381 | 0.0412 | 0.0290 | 294 38 59.6 |

Table 5.3.5: Coordinate Corrections and Stochastic Parameters-Second Level Real Network -Static-Dynamic Approach

 $\bar{\sigma}_{v} = 0.023355$ $\bar{\sigma}_{E} = 0.024296$ $\bar{\sigma}_{C} = 0.023830$ $\hat{\sigma}_{0}^{2} = 1.009889$





| PCINT | PROVISIONAL | COORDINATES | ADJUSTED C | COORDINATES |
|-------|-------------|-------------|-------------|--------------|
| | N (m) | E (m) | N (m) | E (m) |
| 1 | 9583105.004 | 513215.950 | 9583105.004 | 513215.950 |
| 2 | 9576179.235 | 574648.607 | 9576179.235 | 574648.607 |
| 3 | 9600981.218 | 569580.575 | 9600981.218 | 569580.575 |
| 4 | 9599052.507 | 594885.488 | 9599052.507 | 594885.488 |
| 5 | 9611665.696 | 589503.231 | 9611665.696 | 589503.231 |
| 6 | 9624778.565 | 606329.885 | 9624778.565 | 606329.885 |
| 7 | 9640229.703 | 580182.077 | 9640229.703 | 580182.077 |
| 8 | 9644287.286 | 609203.286 | 9644287.286 | 609203.286 |
| 9 | 9661267.225 | 585576.691 | 9661267.225 | 585576.691 |
| 10 | 9660984.753 | 598816.111 | 9660984.753 | 598816.111 |
| 11 | 9661696.859 | 618181.218 | 9661696.859 | 618181.218 |
| 12 | 9651426.855 | 578082.243 | 9651426.855 | 578082.243 |
| 13 | 9649302.681 | 592482.865 | 9649302.681 | 592482.865 |
| 14 | 9640093.572 | 625611.395 | 9640093.572 | 625611.395 |
| 15 | 9614609.371 | 603055.410 | 9614609.371 | 603055.410 |
| 16 | 9626055.619 | 593121.942 | 9626055.619 | 593121.942 |
| 17 | 9623694.425 | 582449.886 | 9623694.425 | 582449.886 |
| 18 | 9625643.288 | 561292.564 | 9625643.288 | 561292.564 |
| 19 | 9607749.690 | 545064.420 | 9607749.690 | 545064.420 |
| 20 | 9610759.097 | 559563.423 | 9610759.097 | 559563.423 |
| 21 - | 9609410.878 | 563591.472 | 9609410.878 | 563591.472 |
| 22 | 9592183.544 | 576550.590 | 9592183.544 | 576550.590 |
| 23 | 9584543.218 | 589735.830 | 9584543.218 | 589735.830 |
| 24 | 9585354.356 | 561756.098 | 9585354.356 | 561756.098 |
| 25 | 9580752.250 | 538526.297 | 9580752.250 | 538526.297 |
| 26 | 9589557.286 | 528224.012 | 9589557.286 | 528224.012 |
| 27 | 9598477.450 | 540001.040 | 9598477.441 | 540001.056 |
| 28 | 9590143.010 | 544871.930 | 9590142.999 | 544871.941 |
| 29 | 9592184.550 | 558655.590 | 9592184.535 | 558655.599 |
| 30 | 9586646.840 | 596567.510 | 9586646.840 | 596567.508 |
| 31 | 9593341.460 | 585647.230 | 9593341.455 | 585647.231 |
| 32 | 9610982.260 | 577814.010 | 9610982.261 | 577813.999 |
| 33 | 9608655.320 | 595394.330 | 9608655.324 | 595394 . 227 |
| 34 | 9619838.450 | 564763.860 | 9619838.446 | 564763.856 |
| 35 | 9620013.730 | 589321.420 | 9620013.733 | 589321.434 |
| 36 | 9635147.760 | 567613.380 | 9635147.742 | 567613.395 |
| 37 | 9630041.920 | 586400.120 | 9630041.923 | 586400.138 |
| 38 | 9639112.320 | 594892.100 | 9639112.323 | 594892.102 |
| 39 | 9635021.720 | 609221.860 | 9635021.799 | 609221.839 |
| 40 | 9649311.340 | 618081.160 | 9649311.335 | 618081.126 |
| 41 | 9656888.740 | 608069.420 | 9656888.759 | 608069.429 |

Table 5.3.6: Estimated Coordinates- Second Level Real Network Densification -Static-Dynamic Approach

5.3.3 Sub-Optimal Fusion Densification

The results presented in this section were determined by considering the estimated coordinates of the first order real network listed in Tables (5.3.2) as fixed stochastic constraints. The *sub-optimal fusion* approach was then used to densify the first order network by intercalating on to the network second and third order points giving results for first level densification {cf. section (5.3.3.1)} and second level densification {cf. section (5.3.3.2)}.

5.3.3.1 First Level Densification

In the first level real network densification, first order points 1 through 11 were considered as fixed stochastic parameters while second order points 12 through 26 were considered as new points whose coordinates were to be estimated {cf. Figure (4.6)}. The observation data sets in Table (4.10) and the approximate coordinates in Table (4.9b) were used resulting in parameters listed in Table (5.3.7) and Table (5.3.8) below while error ellipses are given diagrammatically in Figure (5.19).

| POINT | ΔN | ΔE | $\sigma_{\rm v}$ | $\sigma_{\scriptscriptstyle F}$ | σ_{max} | σ_{min} | α |
|-------|------------|------------|------------------|---------------------------------|----------------|----------------|-------------|
| | (m) | (m) | (m) | (m) | (m) | (m) | · · · · |
| 1 | 0.0000 | 0.0000 | 0.0166 | 0.0125 | 0.0169 | 0.0121 | 29 21 57.1 |
| 2 | 0.0000 | 0.0000 | 0.0109 | 0.0119 | 0.0126 | 0.0100 | 291 58 8.1 |
| 3 | 0.0000 | 0.0000 | 0.0099 | 0.0093 | 0.0105 | 0.0086 | 71 14 37.2 |
| 4 | 0.0000 | 0.0000 | 0.0083 | 0.0093 | 0.0095 | 0.0080 | 312 20 32.9 |
| 5 | 0.0000 | 0.0000 | 0.0074 | 0.0082 | 0.0087 | 0.0069 | 306 40 52.7 |
| 6 | 0.0000 | 0.0000 | 0.0075 | 0.0091 | 0.0093 | 0.0073 | 319 9 10.3 |
| 7 | 0.0000 | 0.0000 | 0.0072 | 0.0075 | 0.0077 | 0.0070 | 290 17 24.7 |
| 8 | 0.0000 | 0.0000 | 0.0057 | 0.0070 | 0.0070 | 0.0057 | 352 25 4.2 |
| 9 | 0.0000 | 0.0000 | 0.0078 | 0.0073 | 0.0078 | 0.0073 | 353 35 36.1 |
| 10 | 0.0000 | 0.0000 | 0.0071 | 0.0067 | 0.0071 | 0.0067 | 01 58 46.1 |
| 11 | 0.0000 | 0.0000 | 0.0085 | 0.0078 | 0.0090 | 0.0072 | 68 12 59.1 |
| 12 | -0.0571 | 0.0158 | 0.0134 | 0.0237 | 0.0240 | 0.0127 | 336 19 44.5 |
| 13 | 0.0051 | 0.0094 | 0.0312 | 0.0498 | 0.0561 | 0.0173 | 58 02 31.8 |
| 14 | -0.0711 | -0.0058 | 0.0335 | 0.0175 | 0.0335 | 0.0174 | 05 05 58.4 |
| 15 | 0.0034 | -0.0152 | 0.0186 | 0.0401 | 0.0414 | 0.0155 | 328 40 22.2 |
| 16 | -0.0268 | 0.0777 | 0.0166 | 0.0163 | 0.0186 | 0.0139 | \$5 28 52.6 |
| 17 | 0.0109 | 0.0655 | 0.0197 | 0.0493 | 0.0495 | 0.0191 | 11 12 15.0 |
| 18 | -0.0280 | -0.0737 | 0.0216 | 0.0225 | 0.0239 | 0.0200 | 282 57 17.3 |
| 19 | -0.1947 | -0.1383 | 0.0369 | 0.0281 | 0.0398 | 0:0238 | 55 35 22.0 |
| 20 | -0.0740 | -0.1282 | 0.0187 | 0.0224 | 0.0230 | 0.0179 | 44 09 40.3 |
| 21 | -0.0016 | -0.1985 | 0.0169 | 0.0218 | 0.0232 | 0.0151 | 51 48 14.8 |
| 22 | -0.1004 | 0.0667 | 0.0189 | 0.0340 | 0.0357 | 0.0154 | 320 13 12.4 |
| 23 | 0.0439 | 0.1172 | 0.0203 | 0.0362 | 0.0373 | 0.0180 | 327 26 08.2 |
| 24 | -0.2327 | -0.2191 | 0.0188 | 0.0170 | 0.0188 | 0.0170 | 351 35 15.5 |
| 25 | -0.2244 | -0.1095 | 0.0384 | 0.0200 | 0.0383 | 0.0200 | 359 28 03.5 |
| 26 | -0.2118 | -0.1940 | 0.0323 | 0.0181 | 0.0329 | 0.0169 | 27 08 07.5 |

Table 5.3.7: Coordinate Corrections and Stochastic Parameters-First Level Real Network -Sub-Optimal Fusion Approach

 $\overline{\sigma}_{v} = 0.01993$ $\overline{\sigma}_{E} = 0.02345$ $\overline{\sigma}_{C} = 0.021760$ $\hat{\sigma}_{0}^{2} = 1.006536$





| POINT | PROVISIONAL COORDINATES | | ADJUSTED COO | ORDINATEN (m) |
|-------|-------------------------|------------|--------------|---------------|
| | N (m) | E (m) | N (m) | E (m) |
| 1 | 9583105.004 | 513215.950 | 9583105.004 | 513215.950 |
| 2 | 9576179.235 | 574648.607 | 9576179.235 | 574648.607 |
| 3 | 9600981.218 | 569580.575 | 9600981.218 | 569580.575 |
| 4 | 9599052.507 | 594885.488 | 9599052.507 | 594885.488 |
| 5 | 9611665.696 | 589503.231 | 9611665.696 | 589503.231 |
| 6 | 9624778.565 | 606329.885 | 9624778.565 | 606329.885 |
| 7 | 9640229.703 | 580182.077 | 9640229.703 | 580182.077 |
| 8 | 9644287.286 | 609203.286 | 9644287.286 | 609203.286 |
| 9 | 9661267.225 | 585576.691 | 9661267.225 | 585576.691 |
| 10 | 9660984.753 | 598816.111 | 9660984.753 | 598816.111 |
| 11 | 9661696.859 | 618181.218 | 9661696.859 | 618181.218 |
| 12 | 9651426.870 | 578082.210 | 9651426.813 | 578082.226 |
| 13 | 9649302.660 | 592482.850 | 9649302.665 | 592482.859 |
| 14 | 9640093.640 | 625611.430 | 9640093.569 | 625611.424 |
| 15 | 9614609.390 | 603055.440 | 9614609.393 | 603055.425 |
| 16 | 9626055.670 | 593121.870 | 9626055.643 | 593121.948 |
| 17 | 9623694.380 | 582449.870 | 9623694.391 | 582449.936 |
| 18 | 9625643.250 | 561292.670 | 9625643.222 | 561292.596 |
| 19 | 9607749.860 | 545064.590 | 9607749.665 | 545064.452 |
| 20 | 9610759.110 | 559563.590 | 9610759.036 | 559563.462 |
| 21 | 9609410.820 | 563591.710 | 9609410.818 | 563591.511 |
| 22 | 9592183.630 | 576550.570 | 9592183.530 | 576550.637 |
| 23 | 9584543.130 | 589735.740 | 9584543.174 | 589735.857 |
| 24 | 9585354.590 | 561756.300 | 9585354.357 | 561756.081 |
| 25 | 9580752.500 | 538526.380 | 9580752.276 | 538526.270 |
| 26 | 9589557.530 | 528224.190 | 9589557.318 | 528223.996 |

Table 5.3.8: Estimated Coordinates- First Level Real Network Densification -Sub-Optimal Fusion Approach

5.3.3.2 Second Level Densification

In the Second level real network densification, first order points 1 through 11 and second order points 12 through 26 were considered as fixed stochastic parameters while third order points 27 through 41 were considered as new points whose coordinates were to be estimated (cf. Figure (4.7)). The observation data sets in Table (4.12) and the approximate coordinates in Table (4.11b) were used resulting in parameters listed in Table (5.3.9) and Table (5.3.10) below while error ellipses are given diagrammatically in Figure (5.20).

| POINT | ΔΝ | ΔE | σ | σ_{F} | $\sigma_{_{ m max}}$ | σ_{mn} | α |
|-------|---------|------------|--------|--------------|----------------------|---------------|-------------|
| | (m) | (m) | (m) | (m) | (m) | (m) | ° , |
| 1 | 0.0000 | 0.0000 | 0.0166 | 0.0125 | 0.0169 | 0.0121 | 29 21 57.1 |
| 2 | 0.0000 | 0.0000 | 0.0109 | 0.0119 | 0.0126 | 0.0100 | 291 58 8.1 |
| 3 | 0.0000 | 0.0000 | 0.0099 | 0.0093 | 0.0105 | 0.0086 | 71 14 37.2 |
| 4 | 0.0000 | 0.0000 | 0.0083 | 0.0093 | 0.0095 | 0.0080 | 313 20 32.9 |
| 5 | 0.0000 | 0.0000 | 0.0074 | 0.0082 | 0.0087 | 0.0069 | 307 40 52.7 |
| 6 | 0.0000 | 0.0000 | 0.0075 | 0.0091 | 0.0093 | 0.0073 | 319 9 10.3 |
| 7 | 0.0000 | 0.0000 | 0.0072 | 0.0075 | 0.0077 | 0.0070 | 290 17 24.7 |
| 8 | 0.0000 | 0.0000 | 0.0057 | 0.0070 | 0.0070 | 0.0057 | 352 25 4.2 |
| 9 | 0.0000 | 0.0000 | 0.0078 | 0.0073 | 0.0078 | 0.0073 | 353 35 36.1 |
| 10 | 0.0000 | 0.0000 | 0.0071 | 0.0067 | 0.0071 | 0.0067 | 01 58 46.1 |
| 11 | 0.0000 | 0.0000 | 0.0085 | 0.0078 | 0.0090 | 0.0072 | 68 12 59.1 |
| 12 | 0.0000 | 0.0000 | 0.0134 | 0.0237 | 0.0240 | 0.0127 | 336 19 44.5 |
| 13 | 0.0000 | 0.0000 | 0.0312 | 0.0498 | 0.0561 | 0.0173 | 58 02 31.8 |
| 14 | 0.0000 | 0.0000 | 0.0335 | 0.0175 | 0.0335 | 0.0174 | 05 05 58.4 |
| 15 | 0.0000 | 0.0000 | 0.0186 | 0.0401 | 0.0413 | 0.0155 | 328 40 22.2 |
| 16 | 0.0000 | 0.0000 | 0.0166 | 0.0163 | 0.0186 | 0.0140 | 85 28 52.6 |
| 17 | 0.0000 | 0.0000 | 0.0197 | 0.0493 | 0.0495 | 0.0191 | 11 12 15.0 |
| 18 | 0.0000 | 0.0000 | 0.0216 | 0.0225 | 0.0239 | 0.0200 | 282 57 17.3 |
| 19 | 0.0000 | 0.0000 | 0.0369 | 0.0281 | 0.0397 | 0.0238 | 55 35 22.0 |
| 20 | 0.0000 | 0.0000 | 0.0187 | 0.0224 | 0.0230 | 0.0179 | 44 09 40.3 |
| 21 | 0.0000 | 0.0000 | 0.0169 | 0.0218 | 0.0231 | 0.0151 | 51 48 14.8 |
| 22 | 0.0000 | 0.0000 | 0.0189 | 0.0340 | 0.0357 | 0.0154 | 320 13 12.4 |
| 23 | 0.0000 | 0.0000 | 0.0203 | 0.0362 | 0.0373 | 0.0180 | 327 26 08.2 |
| 24 | 0.0000 | 0.0000 | 0.0188 | 0.0170 | 0.0188 | 0.0169 | 351 35 15.5 |
| 25 | 0.0000 | 0.0000 | 0.0384 | 0.0200 | 0.0384 | 0.0200 | 359 28 03.5 |
| 26 | 0.0000 | 0.0000 | 0.0323 | 0.0181 | 0.0329 | 0.0169 | 28 08 07.5 |
| 27 | 0.2265 | 0.3338 | 0.0260 | 0.0197 | 0.0261 | 0.0196 | 12 10 29.1 |
| 28 | 0.1243 | 0.1794 | 0.0265 | 0.0157 | 0.0265 | 0.0156 | 354 7 35.0 |
| 29 | 0.2070 | 0.0410 | 0.0159 | 0.0154 | 0.0174 | 0.0135 | 82 13 41.8 |
| 30 | -0.0224 | -0.1603 | 0.0301 | 0.0225 | 0.0301 | 0.0226 | 02 41 03.9 |
| 31 | -0.0046 | -0.0144 | 0.0172 | 0.0195 | 0.0228 | 0.0123 | 283 04 27.7 |
| 32 | -0.0965 | 0.2880 | 0.0207 | 0.0188 | 0.0244 | 0.0137 | 79 19 59.7 |
| 33 | -0.0324 | 0.0676 | 0.0118 | 0.0133 | 0.0145 | 0.0103 | .69 14 07.4 |
| 34 | 0.0092 | 0.0848 | 0.0124 | 0.0198 | 0.0200 | 0.0123 | 348 24 05.9 |
| 35 | -0.0241 | 0.0547 | 0.0126 | 0.0161 | 0.0161 | 0.0126 | 08 43 13.2 |
| 36 | 0.1173 | -0.0382 | 0.0243 | 0.0181 | 0.0276 | 0.0129 | 65 42 31.4 |
| 30 | -0.0380 | 0.0167 | 0.0119 | 0.0185 | 0.0194 | 0.0112 | 2/ 1/ 3/.2 |
| 30 | 0.0604 | 0.0142 | 0.0170 | 0.0119 | 0.0174 | 0.0113 | 32 50 51.4 |
| 10 | 0.1788 | 0.0276 | 0.0583 | 0.0199 | 0.0586 | 0.0188 | 13 23 18.9 |
| 40 | 0.0646 | -0.0609 | 0.0145 | 0.0376 | 0.0375 | 0.0145 | 01 03 11.8 |
| 41 | 0.0301 | -0.0557 | 0.0311 | 0.0358 | 0.0388 | 0.0273 | 294 38 59.6 |

Table 5.3.9: Coordinate Corrections and Stochastic Parameters-Second Level Real Network -Sub-Optimal Fusion Approach

 $\bar{\sigma}_{v} = 0.021886$ $\bar{\sigma}_{z} = 0.022705$ $\bar{\sigma}_{c} = 0.022299$ $\hat{\sigma}_{o}^{2} = 1.009277$



Figure 5.20: Point error ellipses -second level real network densification sub-optimal fusion approach

| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|-------------|-------------|
| EOTH- | N (m) | E (m) | N (m) | <u>E(m)</u> |
| - | 9583104.004 | 513215.950 | 9583105.004 | 513215.950 |
| 2 | 9576179.235 | 574648.607 | 9576179.235 | 574648.607 |
| 2 | 9600981.218 | 569580.575 | 9600981.218 | 569580.575 |
| 4 | 9599052.507 | 594885.488 | 9599052.507 | 594885.488 |
| 5 | 9611665.696 | 589503.231 | 9611665.696 | 589503.231 |
| 6 | 9624778.565 | 606329.885 | 9624778.565 | 606329.885 |
| 7 | 9640229.703 | 580182.077 | 9640229.703 | 580182.077 |
| 8 | 9644287.286 | 609203.286 | 9644287.286 | 609203.286 |
| 9 | 9661267.225 | 585576.691 | 9661267.225 | 585576.691 |
| 10 | 9660984.753 | 598816.111 | 9660984.753 | 598816.111 |
| 11 | 9661696.859 | 618181.218 | 9661696.859 | 618181.218 |
| 12 | 9651426.813 | 578082.226 | 9651426.813 | 578082.226 |
| 13 | 9649302.665 | 592482.859 | 9649302.665 | 592482.859 |
| 14 | 9640093.569 | 625611.424 | 9640093.569 | 625611.424 |
| 15 | 9614609.393 | 603055.425 | 9614609.393 | 603055.425 |
| 16 | 9626055.643 | 593121.948 | 9626055.643 | 593121.948 |
| 17 | 9623694.391 | 582449.936 | 9623694.391 | 582449.936 |
| 18 | 9625643.222 | 561292.596 | 9625643.222 | 561292.596 |
| 19 | 9607749.665 | 545064.452 | 9607749.665 | 545064.452 |
| 20 | 9610759.036 | 559563.462 | 9610759.036 | 559563.462 |
| 21 | 9609410.818 | 563591.511 | 9609410.818 | 563591.511 |
| 22 | 9592183.530 | 576550.637 | 9592183.530 | 576550.637 |
| 23 | 9584543.174 | 589735.852 | 9584543.174 | 589735.857 |
| 24 | 9585354.357 | 561756.081 | 9585354.357 | 561756.081 |
| 25 | 9580752.276 | 538526.270 | 9580752.276 | 538526.270 |
| 26 | 9589557.218 | 528223.996 | 9589557.318 | 528223.996 |
| 27 | 9598477.450 | 540001.040 | 9598477.677 | 540001.374 |
| 28 | 9590143.010 | 544871.930 | 9590143.134 | 544872.109 |
| 29 | 9592184.550 | 558655.590 | 9592184.757 | 558655.631 |
| 30 | 9586646.840 | 596567.510 | 9586646.818 | 596567.350 |
| 31 | 9593341.460 | 585647.230 | 9593341.455 | 585647.216 |
| 32 | 9610982.260 | 577814.010 | 9610982.164 | 577814.298 |
| 33 | 9608655.320 | 595394.330 | 9608655.288 | 595394.378 |
| 34 | 9619838.450 | 564763.860 | 9619838.459 | 564763.945 |
| 35 | 9620013.730 | 589321.420 | 9620013.706 | 589321.475 |
| 36 | 9635147.760 | 567613.380 | 9635147.877 | 567613.342 |
| 37 | 9630041.920 | 586400.120 | 9630041.882 | 586400.137 |
| 38 | 9639112.320 | 594892.100 | 9639112.380 | 594892.114 |
| 39 | 9635021.720 | 609221.860 | 9635021.899 | 609221.888 |
| 40 | 9649311.340 | 618081.160 | 9649311.405 | 618081.099 |
| 41 | 9656888. 40 | 608069.420 | 9656888.770 | 608069.364 |

Table 5.3.10: Estimated Coordinates- Second Level Real Network Densification -Sub-Optimal Fusion Approach

5.3.4 Dynamic Densification

The results presented in this section were determined by considering the estimated coordinates of the first order real network listed in Table (5.3.2) as stochastic constraints. The *dynamic* approach was then used to densify the first order network by intercalating on to the network second and third order points giving results for first level densification {c.f. section (5.3.4.1)} and second level densification {c.f. section (5.3.4.2)}.

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5.3.4.1 First Level Densification

In the first level real network densification, all points 1 through 26 were considered as stochastic parameters with all of them being re-estimated including the datum points 1 through 11. {cf. Figure (4.6)}. The observation data sets in Table (4.10) and the approximate coordinates in Table (4.9) were used resulting in parameters listed in Table (5.3.11) and Table (5.3.12) below while error ellipses are given diagrammatically in Figure (5.21).

| POINT | ΔΝ | ΔE | σ_N | $\sigma_{\scriptscriptstyle E}$ | $\sigma_{\rm max}$ | σ_{min} | α |
|-------|---------|------------|------------|---------------------------------|--------------------|----------------|-------------|
| | (m) | (m) | (m) | (m) | (m) | (m) | |
| 1 | 0.1106 | -0.0128 | 0.0179 | 0.0129 | 0.0179 | 0.0129 | 29 21 57.1 |
| 2 | -0.0081 | -0.0372 | 0.0114 | 0.0126 | 0.0126 | 0.0114 | 291 58 8.1 |
| 3 | -0.0498 | 0.0652 | 0.0104 | 0.0100 | 0.0105 | 0.0100 | 71 14 37.2 |
| 4 | -0.0458 | -0.0007 | 0.0091 | 0.0102 | 0.0102 | 0.0091 | 314 20 32.9 |
| 5 | -0.0087 | 0.0843 | 0.0079 | 0.0088 | 0.0088 | 0.0076 | 308 40 52.7 |
| 6 | 0.0299 | -0.0075 | 0.0082 | 0.0098 | 0.0098 | 0.0082 | 319 9 10.3 |
| 7 | -0.0400 | -0.0108 | 0.0077 | 0.0082 | 0.0082 | 0.0077 | 290 17 24.7 |
| 8 | 0.0335 | 0.0447 | 0.0063 | 0.0077 | 0.0077 | 0.0063 | 352 25 4.2 |
| 9 | -0.0329 | -0.0305 | 0.0085 | 0.0081 | 0.0085 | 0.0081 | 353 35 36.1 |
| 10 | -0.0596 | -0.0399 | 0.0079 | 0.0074 | 0.0079 | 0.0074 | 01 58 46.1 |
| 11 | 0.0801 | -0.0449 | 0.0094 | 0.0087 | 0.0094 | 0.0087 | 68 12 59.1 |
| 12 | -0.0571 | 0.0158 | 0.0154 | 0.0272 | 0.0277 | 0.0146 | 336 19 44.5 |
| 13 | 0.0051 | 0.0094 | 0.0359 | 0.0574 | 0.0647 | 0.0199 | 58 02 31.8 |
| 14 | -0.0711 | -0.0058 | 0.0386 | 0.0202 | 0.0386 | 0.0201 | 05 05 58.4 |
| 15 | 0.0034 | -0.0152 | 0.0215 | 0.0461 | 0.0476 | 0.0179 | 328 40 22.2 |
| 16 | -0.0268 | 0.0777 | 0.0192 | 0.0187 | 0.0214 | 0.0161 | 85 28 52.6 |
| 17 | 0.0109 | 0.0655 | 0.0226 | 0.0568 | 0.0570 | 0.0220 | 11,12 15.0 |
| 18 | -0.0280 | -0.0737 | 0.0249 | 0.0259 | 0.0275 | 0.0231 | 282,57 17.3 |
| 19 | -0.1947 | -0.1383 | 0.0425 | 0.0323 | 0.0458 | 0.0274 | 55 35 22.0 |
| 20 | -0.0740 | -0.1282 | 0.0216 | 0.0257 | 0.0265 | 0.0206 | 44 09 40.3 |
| 21 | -0.0016 | -0.1985 | 0.0195 | 0.0252 | 0.0267 | 0.0174 | 51 48 14.8 |
| 22 | -0.1004 | 0.0667 | 0.0218 | 0.0391 | 0.0411 | 0.0178 | 320 13 12.4 |
| 23 | 0.0439 | 0.1172 | 0.0233 | 0.0417 | 0.0430 | 0.0208 | 327 26 08.2 |
| 24 | -0.2327 | -0.2191 | 0.0217 | 0.0195 | 0.0217 | 0.0195 | 351 35 15.5 |
| 25 | -0.2244 | -0.1095 | 0.0442 | 0.0230 | 0.0442 | 0.0230 | 359 28 03.5 |
| 26 | -0.2118 | -0.1940 | 0.0372 | 0.0209 | 0.0380 | 0.0195 | 27 08 07.5 |

Table 5.3.11: Coordinate Corrections and Stochastic Parameters-First Level Real Network -Dynamic Approach

 $\bar{\sigma}_{v} = 0.022829$

 $\overline{\sigma}_{s} = 0.026885 \quad \overline{\sigma}_{c} = 0.024939 \quad \hat{\sigma}_{0}^{2} = 1.003964$



.

dynamic approach

100

| POINT | PROVISIONAL | COORDINATES | ADJUSTED C | OORDINATES |
|-------|-------------|-------------|-------------|------------|
| EGTUE | N (m) | E (m) | N (m) | E (m) |
| 1 | 9583105.004 | 513215.950 | 9583105.115 | 513215.937 |
| 2 | 9576179.235 | 574648.607 | 9576179.227 | 574648.570 |
| 3 | 9600981.218 | 569580.575 | 9600981.168 | 569580.640 |
| Δ | 9599052.507 | 594885.488 | 9599052.461 | 594885.487 |
| 5 | 9611665.696 | 589503.231 | 9611665.687 | 589503.315 |
| 6 | 9624778.565 | 606329.885 | 9624778.595 | 606329.877 |
| 7 | 9640229.703 | 580182.077 | 9640229.663 | 580182.066 |
| 8 | 9644287.286 | 609203.286 | 9644287.320 | 609203.331 |
| 9 | 9661267.225 | 585576.691 | 9661267.192 | 585576.661 |
| 10 | 9660984.753 | 598816.111 | 9660984.693 | 598816.071 |
| 11 | 9661696.859 | 618181.218 | 9661696.939 | 618181.173 |
| 12 | 9651426.870 | 578082.210 | 9651426.813 | 578082.226 |
| 13 | 9649302.660 | 592482.850 | 9649302.665 | 592482.859 |
| 14 | 9640093.640 | 625611.430 | 9640093.569 | 625611.424 |
| 15 | 9614609.390 | 603055.440 | 9614609.393 | 603055.425 |
| 16 | 9626055.670 | 593121.870 | 9626055.643 | 593121.948 |
| 17 | 9623694.380 | 582449.870 | 9623694.391 | 582449.936 |
| 18 | 9625643.250 | 561292.670 | 9625643.222 | 561292.596 |
| 19 | 9607749.860 | 545064.590 | 9607749.665 | 545064.452 |
| 20 | 9610759.110 | 559563.590 | 9610759.036 | 559563.462 |
| 21 | 9609410.820 | 563591.710 | 9609410.818 | 563591.511 |
| 22 | 9592183.630 | 576550.570 | 9592183.530 | 576550.637 |
| 23 | 9584543.130 | 589735.740 | 9584543.174 | 589735.857 |
| 24 | 9585354.590 | 561756.300 | 9585354.357 | 561756.081 |
| 25 | 9580752.500 | 538526.380 | 9580752.276 | 538526.270 |
| 26 | 9589557.530 | 528224.190 | 9589557.318 | 528223.996 |

Table 5.3.12: Estimated Coordinates- First Level Real Network Densification -Dynamic Approach

5.3.4.2 Second Level Densification

In the Second level real network densification, first order points 1 through 41 were considered stochastic with all points being estimated including the datum points 1 through 26 (cf. Figure (4 7)). The observation data sets in Table (4.12) and the approximate coordinates in Table (4.11c) were used resulting in parameters listed in Table (5.3.13) and Table (5.3.14) below while error ellipses are given diagrammatically in Figure (5.22).

| | -Dyl | anne Appiv | Jacii | | | | |
|-------|------------|------------|------------------|---------------------------------|--------------------|---------------|-------------|
| POINT | ΔN | ΔE | $\sigma_{\rm N}$ | $\sigma_{\scriptscriptstyle E}$ | $\sigma_{\rm max}$ | σ_{mn} | α |
| | (m) | (m) | (m) | (m) | (m) | (m) | 0 |
| 1 | 0.0103 | -0.0389 | 0.0177 | 0.0133 | 0.0177 | 0.0133 | 29 21 57.1 |
| 2 | -0.0214 | -0.0328 | 0.0116 | 0.0127 | 0.0127 | 0.0116 | 291 58 8.1 |
| 3 | -0.0214 | 0.0895 | 0.0101 | 0.0095 | 0.0102 | 0.0094 | 71 14 37.2 |
| 4 | -0.0391 | 0.0049 | 0.0085 | 0.0096 | 0.0096 | 0.0084 | 315 20 32.9 |
| 5 | -0.0070 | 0.0903 | 0.0075 | 0.0084 | 0.0084 | 0.0075 | 309 40 52.7 |
| 6 | 0.0310 | ~0.0077 | 0.0080 | 0.0096 | 0.0096 | 0.0080 | 319 9 10.3 |
| 7 | -0.0394 | -0.0085 | 0.0074 | 0.0075 | 0.0075 | 0.0074 | 290 17 24.7 |
| 8 | 0.0337 | 0.0345 | 0.0060 | 0.0072 | 0.0072 | 0.0060 | 352 25 4.2 |
| 9 | -0.0314 | -0.0305 | 0.0083 | 0.0078 | 0.0083 | 0.0078 | 353 35 36.1 |
| 10 | -0.0602 | -0.0401 | 0.0075 | 0.0071 | 0.0075 | 0.0071 | 01 58 46.1 |
| 11 | 0.0750 | -0.0442 | 0.0089 | 0.0083 | 0.0089 | 0.0082 | 68 12 59.1 |
| 12 | 0.0560 | -0.0105 | 0.0148 | 0.0256 | 0.0256 | 0.0148 | 336 19 44.5 |
| 13 | 0.0015 | 0.0219 | 0.0320 | 0.0372 | 0.0380 | 0.0311 | 58 02 31.8 |
| 14 | 0.0918 | 0.0111 | 0.0351 | 0.0179 | 0.0351 | 0.0179 | 05 05 58.4 |
| 15 | -0.0149 | 0.0564 | 0.0199 | 0.0396 | 0.0398 | 0.0196 | 328 40 22.2 |
| 16 | 0.0262 | -0.0559 | 0.0149 | 0.0161 | 0.0163 | 0.0147 | 85 28 52.6 |
| 17 | -0.0171 | 0.0007 | 0.0165 | 0.0220 | 0.0221 | 0.0163 | 11 12 15.0 |
| 18 | 0.0264 | 0.0576 | 0.0173 | 0.0196 | 0.0198 | 0.0171 | 282 57 17.3 |
| 19 | 0.1921 | 0.1410 | 0.0392 | 0.0287 | 0.0395 | 0.0282 | 55 35 22.0 |
| 20 | 0.0344 | 0.1162 | 0.0171 | 0.0221 | 0.0225 | 0.0166 | 44 09 40.3 |
| 21 | 0.0162 | 0.1312 | 0.0148 | 0.0194 | 0.0195 | 0.0147 | 51 48 14.8 |
| 22 | 0.0919 | -0.0856 | 0.0192 | 0.0294 | 0.0294 | 0.0191 | 320 13 12.4 |
| 23 | -0.0412 | -0.0650 | 0.0219 | 0.0290 | 0.0290 | 0.0218 | 327 26 08.2 |
| 24 | 0.1846 | 0.1866 | 0.0186 | 0.0164 | 0.0187 | 0.0163 | 351 35 15.5 |
| 25 | 0.2326 | 0.1062 | 0.0400 | 0.0213 | 0.0401 | 0.0212 | 359 28 03.5 |
| 26 | 0.1926 | 0.1839 | 0.0319 | 0.0189 | 0.0319 | 0.0188 | 29 08 07.5 |
| 27 | 0.1490 | 0.1410 | 0.0324 | 0.0246 | 0.0325 | 0.0245 | 13 10 29.1 |
| 28 | 0.1284 | 0.1131 | 0.0330 | 0.0195 | 0.0331 | 0.0195 | 354 7 35.0 |
| 29 | 0.1219 | 0.0795 | 0.0198 | 0.0191 | 0.0217 | 0.0169 | 82 13 41.8 |
| 30 | 0.0028 | -0.0663 | 0.0375 | 0.0281 | 0.0375 | 0.0281 | 02 41 03.9 |
| 31 | 0.0319 | -0.0659 | 0.0114 | 0.0242 | 0.0284 | 0.0153 | 283 04 27.7 |
| 32 | -0.0175 | 0.1251 | 0.0258 | 0.0234 | 0.0304 | 0.0171 | 79 19 59.7 |
| 33 | -0.0831 | 0.1223 | 0.0147 | 0.0165 | 0.0180 | 0.0129 | 69 14 07.4 |
| 34 | -0.0242 | 0.1065 | 0.0154 | 0.0247 | 0.0248 | 0.0153 | 348 24 05.9 |
| 35 | -0.0185 | 0.0555 | 0.0157 | 0.0200 | 0.0200 | 0.0157 | 08 43 13.2 |
| 36 | 0.0251 | -0.0407 | 0.0302 | 0.0231 | 0.0344 | 0.0161 | 65 42 31.4 |
| 37 | -0.0338 | 0.0281 | 0.0147 | 0.0237 | 0.0242 | 0.0140 | 27 17 37.2 |
| 38 | 0.0509 | 0.0307 | 0.0211 | 0.0148 | 0.0217 | 0.0234 | 32 50 51.4 |
| 39 | 0.1965 | 0.0003 | 0.0726 | 0.0247 | 0.0073 | 0.0181 | 13 23 18.9 |
| 40 | 0.1379 | -0.0095 | 0.0181 | 0.0468 | 0.0468 | 0.0340 | 01 03 11.8 |
| 41 | 0.0183 | 0.0061 | 0.0388 | 0.0446 | 0.0483 | 0.0273 | 294 38 59.6 |

Table 5.3.13: Coordinate Corrections and Stochastic Parameters-Second Level Real Network Dynamic Approach

 $\overline{\sigma}_{v} = 0.024693$ $\overline{\sigma}_{E} = 0.022717$ $\overline{\sigma}_{C} = 0.023726$ $\overline{\sigma}_{0}^{2} = 1.008111$



Figure 5.22: Point error ellipses -second level real network densification dynamic approach

| POINT | PROVISIONAL | COORDINATES | ADJUSTED (| COORDINATES |
|-------|-------------|-------------|-------------|-------------|
| ECT. | N (m) | E (m) | N (m) | E(m) |
| 1 | 9583104.114 | 513215.937 | 9583104.214 | 513215.898 |
| 2 | 9576179.227 | 574648.570 | 9576179.206 | 574648.537 |
| 3 | 9600981.168 | 569580.640 | 9600981.147 | 569580.730 |
| Δ | 9599052.461 | 594885.487 | 9599052.422 | 594885.492 |
| 5 | 9611665.687 | 589503.315 | 9611665.680 | 589503.405 |
| 6 | 9624778.595 | 606329.877 | 9624778.626 | 606329.869 |
| 7 | 9640229.663 | 580182.066 | 9640229.624 | 580182.057 |
| 8 | 9644287.320 | 609203.331 | 9644287.354 | 609203.366 |
| 9 | 9661267.192 | 585576.661 | 9661267.161 | 585576.630 |
| 10 | 9660984.693 | 598816.071 | 9660984.633 | 598816.031 |
| 11 | 9661696.939 | 618181.173 | 9661697.014 | 618181.129 |
| 12 | 9651426.813 | 578082.226 | 9651426.869 | 578082.216 |
| 13 | 9649302.665 | 592482.859 | 9649302.667 | 592482.881 |
| 14 | 9640093.569 | 625611.424 | 9640093.661 | 625611.435 |
| 15 | 9614609.393 | 603055.425 | 9614609.378 | 603055.481 |
| 16 | 9626055.643 | 593121.948 | 9626055.669 | 593121.892 |
| 17 | 9623694.391 | 582449.936 | 9623694.374 | 582449.937 |
| 18 | 9625643.222 | 561292.596 | 9625643.248 | 561292.654 |
| 19 | 9607749.665 | 545064.452 | 9607749.857 | 545064.593 |
| 20 | 9610759.036 | 559563.462 | 9610759.070 | 559563.578 |
| 21 | 9609410.818 | 563591.511 | 9609410.834 | 563591.642 |
| 22 | 9592183.530 | 576550.637 | 9592183.622 | 576550.551 |
| 23 | 9584543.174 | 589735.852 | 9584543.133 | 589735.787 |
| 24 | 9585354.357 | 561756.081 | 9585354.542 | 561756.268 |
| 25 | 9580752.276 | 538526.270 | 9580752.509 | 538526.376 |
| 26 | 9589557.218 | 528223.996 | 9539557.411 | 528224.180 |
| 27 | 9598477.450 | 540001.040 | 9598477.599 | 540001.181 |
| 28 | 9590143.010 | 544871.930 | 9590143.138 | 544872.043 |
| 29 | 9592184.550 | 558655.590 | 9592184.672 | 558655.669 |
| 30 | 9586646.840 | 596567.510 | 9586646.843 | 596567.444 |
| 31 | 9593341.460 | 585647.230 | 9593341.492 | 585647.164 |
| 32 | 9610982.260 | 577814.010 | 9610982.243 | 577814.135 |
| 33 | 9608655.320 | 595394.330 | 9608655.237 | 595394.482 |
| 34 | 9619838.450 | 564763.960 | 9619838.426 | 564763.967 |
| 35 | 9620013.730 | 589321.420 | 9620013.711 | 589321.475 |
| 36 | 9635147.760 | 567613.380 | 9635147.785 | 567613.339 |
| 37 | 9630041.920 | 586400.120 | 9630041.886 | 586400.148 |
| 38 | 9639112.320 | 594892.100 | 9639112.371 | 594892.131 |
| 39 | 9635021.720 | 609221.360 | 9635021.917 | 609221.860 |
| 40 | 9649311.340 | 618081.160 | 9649311.478 | 618081.150 |
| 41 | 9656888.740 | 608069,420 | 9656888.758 | 608069.426 |

Table 5.3.14: Estimated Coordinates- Second Level Real Network Densification -Dynamic Approach

5.3.5 Static Densification

The results presented in this section were determined by considering the estimated coordinates of the first order real network listed in Tables (5.3.2) as fixed non-stochastic entities. The *static* approach was then used to densify the first order networks by intercalating into them second and third order points giving results for first level densification {cf. section (5.3.5.1)} and second level densification {cf. section (5.3.5.2)}.

5.3.5.1 First Level Densification

In the first lexel real network densification, first order points 1 through 11 were considered as fixed non-stochastic parameters while second order points 12 through 26 were considered as new points whose coordinates were to be estimated (cf. Figure (4.6)). The observation data sets in Table (4.10) and the approximate coordinates in Table (4.9) were used resulting in parameters listed in Table (5.3.15) and Table (5.3.16) below while error ellipses are given diagrammatically in Figure (5.23).

| POINT | ΔΝ | ΔE | $\sigma_{_N}$ | $\sigma_{\scriptscriptstyle E}$ | σ_{max} | σ_{min} | α |
|-------|---------|------------|---------------|---------------------------------|----------------|----------------|-------------|
| | (m) | (m) | (m) | (m) | (m:) | (m) | · · · · |
| 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 2 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 3 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 4 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 5 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 6 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 7 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 8 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 9 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 11 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0 |
| 12 | -0.0140 | 0.0308 | 0.0118 | 0.0212 | 0.0216 | 0.0111 | 336 12 24.7 |
| 13 | 0.0193 | 0.0125 | 0.0295 | 0.0477 | 0.0540 | 0.0154 | 58 18 52.5 |
| 14 | -0.0553 | -0.0311 | 0.0312 | 0.0160 | 0.0312 | 0.0160 | 04 22 11.1 |
| 15 | -0.0159 | -0.0234 | 0.0170 | 0.0381 | 0.0395 | 0.0134 | 327 29 38.6 |
| 16 | -0.0438 | 0.0653 | 0.0150 | 0.0141 | 0.0163 | 0.0125 | 75 27 44.6 |
| 17 | 0.0384 | 0.0162 | 0.0180 | 0.0473 | 0.0476 | 0.0174 | 11/39 49.7 |
| 18 | 0.0313 | -0.0933 | 0.0202 | 0.0211 | 0.0225 | 0.0186 | 284 08 41.4 |
| 19 | -0.1564 | -0.1560 | 0.0348 | 0.0263 | 0.0376 | 0.0221 | 56 00 09.5 |
| 20 | -0.0118 | -0.1532 | 0.0170 | 0.0205 | 0.0215 | 0.0158 | 51 27 24.7 |
| 21 | 0.0517 | -0.2147 | 0.0151 | 0.0200 | 0.0217 | 0.0125 | 57 08 49.3 |
| 22 | -0.0800 | 0.0292 | 0.0165 | 0.0319 | 0.0333 | 0.0136 | 324 03 50.6 |
| 23 | 0.0756 | 0.0925 | 0.0182 | 0.0337 | 0.0349 | 0.0160 | 327 07 12.4 |
| 24 | -0.2037 | -0.1762 | 0.0164 | 0.0146 | 0.0167 | 0.0144 | 333 33 39.6 |
| 25 | -0.2244 | -0.0809 | 0.0364 | 0.0176 | 0.0365 | 0.0176 | 359 13 35.4 |
| 26 | -0.2248 | -0.1670 | 0.0301 | 0.0155 | 0.0308 | 0.0139 | 28 39 51.4 |

Table 5.3.15: Coordinate Corrections and Stochastic Parameters-First Level Real Network -Static Approach

 $\bar{\sigma}_{_{N}} = 0.017607$ $\bar{\sigma}_{_{E}} = 0.021251$ $\bar{\sigma}_{_{C}} = 0.019514$ $\hat{\sigma}_{_{0}}^{2} = 1.004632$



| POINT | PROVISIONAL COORDINATES | | ADJUSTED C | OORDINATES |
|-------|-------------------------|------------|-------------|------------|
| FOTUE | N (m) | E (m) | N (m) | E (m) |
| 1 | 9583105.004 | 513215,950 | 9583105.004 | 513215.950 |
| 2 | 9576179.235 | 574648,607 | 9576179.235 | 574648.607 |
| 3 | 9600981.218 | 569580,575 | 9600981.218 | 569580.575 |
| Δ | 9599052.507 | 594885.488 | 9599052.507 | 594885.488 |
| 5 | 9611665.696 | 589503.231 | 9611665.696 | 589503.231 |
| 6 | 9624778.565 | 606329.885 | 9624778.565 | 606329.885 |
| 7 | 9640229.703 | 580182,077 | 9640229.703 | 580182.077 |
| 8 | 9644287.286 | 609203.286 | 9644287.286 | 609203.286 |
| 9 | 9661267.225 | 585576,691 | 9661267.225 | 585576.691 |
| 10 | 9660984.753 | 598816,111 | 9660984.753 | 598816.111 |
| 11 | 9661696.859 | 618181.218 | 9661696.859 | 618181.218 |
| 12 | 9651426.870 | 578082.210 | 9651426.856 | 578082.241 |
| 13 | 9649302.660 | 592482.850 | 9649302.679 | 592482.863 |
| 14 | 9640093.640 | 625611,430 | 9640093.585 | 625611.399 |
| 15 | 9614609.390 | 603055,440 | 9614609.374 | 603055.417 |
| 16 | 9626055.670 | 593121,870 | 9626055.626 | 593121.935 |
| 17 | 9623694.380 | 582449.870 | 9623694.418 | 582449.886 |
| 18 | 9625643.250 | 561292.670 | 9625643.281 | 561292.577 |
| 19 | 9607749.860 | 545064.590 | 9607749.704 | 545064.434 |
| 20 | 9610759.110 | 559563.590 | 9610759.098 | 559563.437 |
| 21 | 9609410.820 | 563591,710 | 9609410.872 | 563591.495 |
| 22 | 9592183.630 | 576550.570 | 9592183,549 | 576550.599 |
| 23 | 9584543.130 | 589735.740 | 9584543,206 | 589735.832 |
| 24 | 9585354.590 | 561756,300 | 9585354.386 | 561756.124 |
| 25 | 9580752.500 | 538526,380 | 9580752.276 | 538526.299 |
| 26 | 9589557.530 | 528224,190 | 9589557.305 | 528224.023 |

Table 5.3 16: Estimated Coordinates- First Level Real Network Densification -Static Approach

5.3.5.2 Second Level Densification

In the Second level real network densification, first order points 1 through 11 and second order points 12 through 26 were considered as fixed non-stochastic parameters while third order points 27 through 41 were considered as new points whose coordinates were to be estimated (cf. Figure (4.7)). The observation data sets in Table (4.12) and the approximate coordinates in Table (4.11d) were used resulting in parameters listed in Table (5.3.17) and Table (5.3.18) below while error ellipses are given diagrammatically in Figure (5.24).

| | | | | | | | 0 |
|-------|------------|------------|---------------|---------------------------------|----------------------|----------------|-------------|
| POINT | ΔN | ΔE | $\sigma_{_N}$ | $\sigma_{\scriptscriptstyle E}$ | $\sigma_{_{ m max}}$ | σ_{mun} | 0 1 11 |
| | (m) | (m) | (m) | (m) | (m) | (m) | |
| 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0121 | 00 |
| 2 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0100 | 00 |
| 3 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0086 | 00 |
| A | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0080 | 00 |
| 5 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0069 | 00 |
| 6 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0073 | 00 |
| 7 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0070 | 00 |
| 8 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0057 | 00 |
| 9 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0073 | 00 |
| 10 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0067 | 00 |
| 11 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0072 | 00 |
| 12 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0137 | 00 |
| 13 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0186 | 00 |
| 14 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0188 | 00 |
| 15 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0167 | 00 |
| 16 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0150 | 00 |
| 17 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0206 | 00 |
| 18 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0216 | 00 |
| 19 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0256 | 00 |
| 20 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0193 | 00 |
| 21 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0163 | 00 |
| 22 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0166 | 00 |
| 23 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0194 | 00 |
| 24 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0183 | 00 |
| 25 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0215 | 00 |
| 26 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0182 | 00 |
| 27 | -0.0014 | 0.0159 | 0.0166 | 0.0125 | 0.0223 | 0.0144 | 52 55 14.8 |
| 28 | -0.0075 | 0.0050 | 0.0109 | 0.0119 | 0.0243 | 0.0127 | 345 44 28.8 |
| 29 | 0.0032 | -0.0035 | 0.0099 | 0.0093 | 0.0125 | 0.0104 | 30 28 57.2 |
| 30 | -0.0006 | -0.0006 | 0.0083 | 0.0093 | 0.0243 | 0.0098 | 20 0 24.8 |
| 31 | -0.0040 | 0.0012 | 0.0074 | 0.0082 | 0.0221 | 0.0114 | 276 35 29.1 |
| 32 | -0.0050 | 0.0079 | 0.0075 | 0.0091 | 0.0213 | 0.0113 | 60, / . / |
| . 33 | 0.0026 | -0.0015 | 0.0072 | 0.0075 | 0.0133 | 0.0092 | 74 38 25.1 |
| 34 | -0.0037 | 0.0037 | 0.0057 | 0.0070 | 0.0135 | 0.0076 | 03 11 55.3 |
| 35 | 0.0005 | 0.0062 | 0.0078 | 0.0073 | 0.0097 | 0.0091 | 29 0 45.1 |
| 36 | -0.0185 | 0.0067 | 0.0071 | 0.0067 | 0.0249 | 0.0105 | 81 4. 45.5 |
| 37 | -0.0018 | 0.0034 | 0.0085 | 0.0078 | 0.0135 | 0.0085 | 351 41 47.1 |
| 38 | 0.0018 | 0.0010 | 0.0139 | 0.0245 | 0.0145 | 0.0107 | 48 36 47.9 |
| 39 | 0.0438 | -0.0105 | 0.0323 | 0.0516 | 0.0548 | 0.0156 | 22 33.9 |
| 40 | -0.0025 | -0.0244 | 0.0347 | 0.0181 | 0.0379 | 0.0135 | 359 5. 15.7 |
| 41 | 0.0111 | -0.0031 | 0.0193 | 0.0415 | 0.0355 | 0.0170 | 63 11 -1.4 |

Table 5.3.17: Coordinate Corrections and Stochastic Parameters-Second Level Real Network -Static Approach

 $\bar{\sigma}_{y} = 0.009568$

 $\bar{\sigma}_{E} = 0.012295 \quad \bar{\sigma}_{C} = 0.011016 \quad \hat{\sigma}_{0}^{2} = 1.000323$



static approach

| POINT | PROVISIONAL | COORDINATES | ADJUSTED | COORDINATES |
|-------|-------------|-------------|-------------|-------------|
| rozn- | N (m) | E (m) | N (m) | E (m) |
| 1 | 9583105.004 | 513215.950 | 9583105.004 | 513215.950 |
| 2 | 9576179.235 | 574648.607 | 9576179.235 | 574648.607 |
| 2 | 9600981.218 | 569580.575 | 9600981.218 | 569580.575 |
| 3 | 9599052.507 | 594885.488 | 9599052.507 | 594885.488 |
| 5 | 9611665.696 | 589503.231 | 9611665.696 | 589503.231 |
| 6 | 9624778.565 | 606329.885 | 9624778.565 | 606329.885 |
| 7 | 9640229.703 | 580182.077 | 9640229.703 | 580182.077 |
| 8 | 9644287.286 | 609203.286 | 9644287.286 | 609203.286 |
| a | 9661267.225 | 585576.691 | 9661267.225 | 585576.691 |
| 10 | 9660984.753 | 598816.111 | 9660984.753 | 598816.111 |
| 11 | 9661696.859 | 618181.218 | 9661696.859 | 618181.218 |
| 12 | 9651426.856 | 578082.241 | 9651426.856 | 578082.241 |
| 13 | 9649302.679 | 592482.863 | 9649302.679 | 592482.863 |
| 14 | 9640093.585 | 625611.399 | 9640093.585 | 625611.399 |
| 15 | 9614609.374 | 603055.417 | 9614609.374 | 603055.417 |
| 16 | 9626055.626 | 593121.935 | 9626055.626 | 593121.935 |
| 17 | 9623694.418 | 582449.886 | 9623694.418 | 582449.886 |
| 18 | 9625643.281 | 561292.577 | 9625643.281 | 561292.577 |
| 19 | 9607749.704 | 545064.434 | 9607749.704 | 545064.434 |
| 20 | 9610759.098 | 559563.437 | 9610759.098 | 559563.437 |
| 21 | 9609410.872 | 563591.495 | 9609410.872 | 563591.495 |
| 22 | 9592183.549 | 576550.599 | 9592183.549 | 576550.599 |
| 23 | 9584543.206 | 589735.832 | 9584543.206 | 589735.832 |
| 24 | 9585354.386 | 561756.124 | 9585354.386 | 561756.124 |
| 25 | 9580752.276 | 538526.299 | 9580752.276 | 538526.299 |
| 26 | 9589557.305 | 528224.023 | 9589557.305 | 528224.023 |
| 27 | 9598477.450 | 540001.040 | 9598477.449 | 540001.056 |
| 28 | 9590143.010 | 544871.930 | 9590143.002 | 544871.935 |
| 29 | 9592184.550 | 558655.590 | 9592184.553 | 558655.587 |
| 30 | 9586646.840 | 596567.510 | 9586646.839 | 596567.509 |
| 31 | 9593341.460 | 585647.230 | 9593341.456 | 585647.231 |
| 32 | 9610982.260 | 577814.010 | 9610982.255 | 577814.018 |
| 33 | 9608655.320 | 595394.330 | 9608655.323 | 595394.329 |
| 34 | 9619838.450 | 564763.860 | 9619838.446 | 564763.864 |
| 35 | 9620013.730 | 589321.420 | 9620013.731 | 589321.426 |
| 36 | 9635147.760 | 567613.380 | 9635147.752 | 567613.387 |
| 37 | 9630041.920 | 586400.120 | 9630041.918 | 586400.123 |
| 38 | 9639112.320 | 594892.100 | 9639112.322 | 594892.101 |
| 39 | 9635021.720 | 609221.860 | 9635021.764 | 609221.849 |
| 40 | 9649311.340 | 618081.160 | 9649311.338 | 618081.134 |
| 41 | 9656888.740 | 608069.420 | 9656888.751 | 608069.417 |

Table 5 3.18: Estimated Coordinates- Second Level Real Network Densification -Static Approach)

5.3.6 Computed Shifts

The final coordinates obtained from the static-dynamic, sub-optimal Fusion, dynamic and static densifications were compared to each other and the results tabulated as shown in Table (5.3.19). Figures (5.25 to 5.30) depict these shifts graphically. In the table, δ is the magnitude of the shift in the two sets of coordinates for each point while α is the bearing of the shift. Also, $\overline{\delta}$ and $\overline{\alpha}$ are the mean of δ and α for the respective densification approaches.

| - | Static-Dynamic | Static-Dynamic | Static- | Sub-Ontimal | Sub-Ontimal | Dynamic |
|------|--------------------------------|--------------------------------|------------------------------|--------------------------------|-----------------------------|-------------------------------|
| | and | and and | Dynamic | and | and | and |
| | Sub Ontinual | Dumanuia | Dynamic | Dynamic | Static | Static |
| | Suo-Optimat | Dynamic | Static | Dynamic | State | Static |
| - | 2 | 8 | State | ð a | S a | δα |
| St | 0 12 | $O \alpha$ | 0 U | (mm) (° ') | (mm) (° ·) | (mm) $(°')$ |
| | (mm) () | (mm) () | (mm)() | (11111)() | | (11111) () |
| 1 | 0 0 | 216.3 166 05 | 0 0 | 216.3 100 05 | | 210.3 100 03 |
| 2 | 0 0 | 75.8 67 30 | 0 0 | /5.8 6/30 | 0 0 | /5.8 6/ 30 |
| 3 | 0 0 | 170.5 294 37 | 0 0 | 170.5 294 37 | 0 0 | 170.5 294 37 |
| 4 | 0 0 | 85.1 357 18 | 0 0 | 85.1 357 18 | 0 0 | 85.1 357 18 |
| 5 | 0 0 | 174.7 275 15 | 0 0 | 174.7 275 15 | 0 0 | 174.7 275 15 |
| 6 | 0 0 | 63.1 165 18 | 0 0 | 63.1 165 18 | 0 0 | 63.1 165 18 |
| 7 | 0 0 | 81.5 14 12 | 0 0 | 81.5 14 12 | 0 0 | 81.5 14 12 |
| 8 | 0 0 | 105.0 229 38 | 0 0 | 105.0 229 38 | 0 0 | 105.0 229 38 |
| 9 | 0 0 | 88.4 43 37 | 0 0 | 88.4 43 37 | 0 0 | 88.4 43 37 |
| 10 | 0 0 | 144.2 33 41 | 0 0 | 144.2 33 41 | 0 0 | 144.2 33 41 |
| 11 | 0 0 | 178.7 150 08 | 0 0 | 178.7 150 08 | 0 0 | 178.7 150 08 |
| 17 | 45.3 22 02 | 30.4 117 24 | 2.2 116 34 | 56.9 169 52 | 45.5 199 14 | 28.2 297 28 |
| 13 | 17.1 20.33 | 21.3 311 11 | 2.8 45 00 | 22.1 264 48 | 14.6 195 57 | 21.6 123 41 |
| 11 | 29.2.275.54 | 97.6 204 12 | 13.6 162 54 | 92.7 186 49 | 29.7 122 37 | 84.1 25 21 |
| 15 | 26.6 214 17 | 71 3 264 22 | 7.6 113 12 | 58.0 284 59 | 20.6 22 50 | 64.1 86 25 |
| 16 | 24.7 194 02 | 70 7 135 00 | 9 9 135 00 | 61 7 114 54 | 21.4 37 24 | 60.8 315 00 |
| 17 | 60 5 304 13 | 72 1 315 00 | 7.0 00.00 | 17.0 356 38 | 56.8 118 22 | 67 3 130 47 |
| 19 | 73 3 334 08 | 98 5 293 58 | 11.8 298 18 | 63 6 245 51 | 62 0 162 09 | 83.8 113 12 |
| 10 | 10.6 307 50 | 210 1 226 01 | 19.8 225.00 | 238 2 216 18 | 12 9 155 13 | 220 7 46 06 |
| 17 | 60.0.326.05 | 57 3 270 53 | 11.0 265 55 | 120 9 253 10 | 66 8 158 02 | 113 8 101 11 |
| 20 | 71.6 326 58 | 175 6 281 31 | 23 8 28.1 37 | 132 0 263 02 | 56 3 163 30 | 151 8 104 30 |
| 21 | 10 / 286 25 | 97.2 152.26 | 10 3 210 57 | 125.0 203.02 | 12 5 116 31 | 87 1 326 10 |
| 22 | 49.0 200 35 | 05 2 36 50 | 10.3 240 37 | 81 1 50 38 | 10.6 112 00 | 85 8 211 39 |
| 23 | 31.0 328 28 | 95.2 20 50 | 20 7 220 55 | 262 0 225 18 | 51 0 303 50 | 212 3 12 13 |
| 2+ | 17.0 95 22 | 252.0 222 20 | 37.7 220 33 | 205.0 225 18 | 20.0.270.00 | 215 1 18 17 |
| 25 | 37.3 133 33 | 177.5 200 25 | 20.1 10+2+ | 233.9 20+ 20 | 29.0 270 00 | 190 1 55 59 |
| 20 | 35.8 153 26 | 209.4 233 21 | 21.9 210 04 | 200.2 2+3 11 | 201.2 51.22 | 105.7 30 19 |
| 21 | 396.0 233 25 | 201.5 218 21 | 8.0 180 00 | 208.2 07 39 | 391.3 34 22 | 193.3 39 40 |
| 28 | 215.5 231 13 | 172.+ 216 16 | 0.7 110 34 | 00.1 93 28 | 218.+ 32 +9 | 1/3.7 30 27 |
| 29 | 224.3 351 48 | 153.8 207 04 | 21.6 1+6 19 | 93.1 333 33 | 208.7 12 100 | 1++.3 3+ 3+ |
| 30 | 159.5 82 04 | 64.1 92 41 | 1.4 315 00 | 97.3 255 06 | 160.4 97.31 | 00.1 2/0 01 |
| 10 | 15.0 90 00 | /6.5 118 54 | 1.0 180 00 | 63.8 125 26 | 15.0 200 12 | /0.0 298 15 |
| 32 | 314.2 287 58 | 136.2 277 36 | 19.9 287 32 | 81.1 115 51 | 294.4 108 00 | 11/.0 95 51 |
| 33 | 79.6 296 53 | 152.3 304 50 | 1.0 00 00 | 74.2 313 22 | //.4 116 54 | 150.1 12+ 58 |
| 34 | 89.9 261 41 | 112.8 280 13 | 8.0 270 00 | 39.7 326 19 | 82.0 80 53 | 104.9 100 59 |
| 35 | 49.1 56 38 | 46.5 298 13 | 8.2 75 58 | 5.0 180 00 | 55.0 117 02 | 52.9 112 12 |
| 30 | 145.0 158 34 | 70.6 127 31 | 12.8 141 20 | 92.0 01 52 | 132.8 340 12 | 58.2 304 30 |
| 37 | 41.0 01 24 | 38.3 344 53 | 15.8 71 34 | 11.7 250 01 | 38.6 158 45 | 40.6 142 00 |
| 38 | 58.2 191 53 | 56.1 211 08 | 1.4 45 00 | 19.2 297 54 | 59.4 12 38 | 57.4 31 29 |
| 39 | 111.3 206 06 | 119.8 190 05 | 36.4 344 03 | 33.3 122 44 | 140.5 16 07 | 153.4 04 07 |
| +0 | 75.0 21 05 | 145.0 189 32 | 10.4 286 42 | 89.1 214 56 | 76.5 331 05 | 140.7 05 43 |
| +1 | 69.9 99 36 | 3.2 71 34 | 14.4 56 19 | 63.2 280 57 | 56.3 289 43 | 11.4 52 07 |
| Mean | $\delta = 89.8$ | $\overline{\delta} = 114.4$ | $\overline{\delta} = 13.1$ | $\delta = 102.8$ | $\delta = 87.2$ | $\delta = 113.9$ |
| | $\overline{\alpha} = 171 \ 10$ | $\overline{\alpha} = 300 \ 10$ | $\overline{\alpha} = 23 + 8$ | $\overline{\alpha} = 285 + 48$ | $\overline{\alpha} = 19757$ | $\overline{\alpha} = 112 + 7$ |

Table 5.3.19: Shifts between estimated parameters for the Experiments (Real Network)



Figure 5.25: Coordinate shifts of sub-optimal fusion approach with respect to static-dynamic approach

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5.4 Analysis of Results

In section (4.3), a number of precision and reliability criteria for densification network analysis have been discussed. The estimated corrections to the provisional parameters which have been computed through the use of static-dynamic, sub-optimal fusion, dynamic and static approaches are presented in Chapter Five together with the standard errors, error ellipses and displacement components in Tables (5.2.1) to (5.3.30). In this chapter, the results presented in Chapter Five are analyzed.

5.4.1 Variance of Unit Weight

The estimated a posteriori variance of unit weight $\hat{\sigma}_0^2$ and a priori variance of unit weight, which was taken to be one in all the densification approaches, are tested for any significant difference. The null hypothesis in each case is written as

$$H_{a}:\hat{\sigma}_{0}^{2}=\sigma_{0}^{2} \tag{5.4.1}$$

and the alternative hypothesis as

$$H_a: \hat{\sigma}_0^2 \neq \sigma_0^2 \tag{5.4.2}$$

where $\hat{\sigma}_0^2$ and σ_0^2 are the a posteriori and a priori variances respectively. Using the χ^2 test, the test statistic is written as

$$\chi_m^2 = \frac{m\hat{\sigma}_0^2}{\sigma_0^2}$$
(5.4.3)

where m are the degrees of freedom. With 5.4.3 and using a level of significance of 5%, the hypothesis 5.4.1 above is tested for and rejected if

$$\chi_m^2 > \chi_{\frac{a}{2}m}^2 \tag{5.4.4}$$

 α being the level of significance. From 5.4.3, test statistic for each approach and level of densification are computed and tabled below.

| | First Level Dens | ification | Second Level Den | sification | |
|---------------------------------|------------------------------|-----------|------------------------------|------------|--|
| STATIC-DYNAMIC DENSIFICATION | $\chi^2_{15} = 15.064$ | Accepted | $\chi^{2}_{60} = 60.374$ | Accepted | |
| | $\chi^2_{0.025,15} = 28.488$ | | $\chi^2_{0.025,60} = 84.893$ | | |
| SUB-OPTIMAL FUSION | $\chi^2_{15} = 15.049$ | Accepted | $\chi^2_{60} = 60.295$ | Accepted | |
| DENSIFICATION | $\chi^2_{0.025,15} = 28.488$ | nocepted | $\chi^2_{0.025,60} = 84.893$ | necepted | |
| DYNAMIC | $\chi^2_{15} = 15.020$ | Accepted | $\chi^2_{60} = 60.163$ | Accented | |
| Duroit i oni i on | $\chi^2_{0.025,15} = 28.488$ | necepted | $\chi^2_{0.025,60} = 84.893$ | necepted | |
| STATIC | $\chi^2_{21} = 21.084$ | Accepted | $\chi^2_{72} = 72.197$ | Accented | |
| DENOILLONILLON | $\chi^2_{0.025,21} = 36.556$ | | $\chi^2_{0.025,72} = 99.276$ | 1.000pccd | |

Table 5.4.1: Computed statistical values for χ^2 test of Simulated network densification

Table 5.4.2: Computed statistical values for χ^{\pm} test of the Real network densification

| | First Level Densification | | Second Level Densification | |
|---------------------------------|--------------------------------|----------|------------------------------|-------------|
| STATIC-DYNAMIC DENSIFICATION | $\chi^2_{28} = 28.258$ | Accepted | $\chi^2_{18} = 18.178$ | Accepted |
| | $\chi^2_{0.025,28} = 45.628$ | | $\chi^2_{0.025,18} = 32.551$ | |
| SUB-OPTIMAL FUSION | $\chi^2_{28} = 28.183$ | Accepted | $\chi^2_{18} = 18.167$ | Accepted |
| DENSIFICATION | $\chi^2_{0.025,28} = 45.628$ | recepted | $\chi^2_{0.025,18} = 32.551$ | 1.000000000 |
| DYNAMIC DENSIFICATION | $\chi^2_{28} = 28.111$ | Accepted | $\chi^2_{18} = 18.146$ | Accepted |
| | $\chi^{1}_{0.025,28} = 45.628$ | nocopeca | $\chi^2_{0.025,18} = 32.551$ | |
| STATIC DENSIFICATION | $\chi^2_{50} = 50.232$ | Accepted | $\chi^2_{70} = 70.024$ | Accepted |
| | $\chi^2_{0.025,50} = 72.906$ | | $\chi^2_{0.025,70} = 96.879$ | |
| | | | | 31 |

These results indicate that the null hypothesis (6.1) is accepted which implies no significance difference between a posteriori and a priori variances of unit weight. From the Tables above, the null hypothesis for the χ^2_m test was accepted for all the experiments on real and simulated networks at both levels of densification. This is a clear indication that the estimated a posteriori variances of unit weight from the densification approaches are statistically equal in the estimation and assumed to be unity.

The acceptance of the null hypothesis indicates that the estimation processes were correctly done and more specifically that the a priori variance of unit weight was correctly chosen and further all the four approaches relate the unknown parameters completely and correctly.



Although in all cases the null hypothesis is acceptable, it has to be observed that for individual statistical estimates, the more close the test statistic is to the tabulated values the more the estimate is considered reliable. An examination of the values of χ^2_m and $\chi^2_{\frac{m}{2},m}$ determined, static densification are closest followed by static-dynamic densification then sub-optimal fusion densification and finally dynamic densification.

It is expected that the densification results of the real and simulated networks by using the static approach appear as the best because the approach is based on the assumption that higher order points are fixed and non-stochastic. This, as we know, is not true since these higher order points were themselves determined from previous adjustment and therefore has stochasticity associated to them.

The results of static-dynamic and sub-optimal fusion densifications have the second closest values while those of dynamic densification have the largest difference. This is attributed to the fact that for static-dynamic and sub-optimal fusion approaches, the datum parameters are maintained definitive. The results determined from static-dynamic approach as compared to those obtained from sub-optimal fusion approach, seem to be closest what might indicate that the static-dynamic approach is superior. Although strictly the difference is insignificant. It is though observed that these two approaches give results that lie between those obtained by static and dynamic approaches and vary from each other slightly. The values obtained from dynamic approach have the largest difference. It is therefore concluded that the static/dynamic and sub-optimal approaches are both viable approaches to densification though the analysis of variances indicate former is superior to the latter.

5.4.2 Standard Errors

The standard errors for static densification are generally smaller followed by those for staticdynamic densification, then for sub-optimal densification and lastly for dynamic densification. The results of static densification seem to be more accurate from the analysis of the standard errors but, as in the case of variances analyzed above, this is because the datum parameters are considered as fixed non-stochastic entities. The standard errors from static-dynamic and suboptimal fusion approaches lie between those obtained from static and dynamic approaches and the most important observation is that they are close to each other.

5.4.3 Error Ellipses

Point error ellipses resulting from free network adjustment of the simulated and real networks are depicted in Figures (5.1) and (5.16). Figures (5.2), (5.3), (5.17) and (5.18) depict point error ellipses for the first and second level densification of the simulated and real network using static-dynamic approach. Error ellipses resulting from the first and second level densification of the simulated and real networks using sub-optimal fusion approach are depicted in Figures (5.4), (5.5), (5.19) and (5.20) and those resulting from dynamic approach are depicted in Figures (5.6), (5.7), (5.21) and (5.22). Lastly error ellipses resulting from the first and second level densification of the real and simulated networks using static approach are depicted in Figures (5.8), (5.9), (5.23) and (5.24).

In the first level real network densification using static approach, network points 1 to 11 do not have error ellipses while in the second level real network densification, network points 1 to 26 do not have error ellipses. Correspondingly, in the first level simulated network densification points 1 to 3 do not have error ellipses while in the second level densification, points 1 to 6 do not have error ellipses. This, as expected, is due to the fact that static approach do not consider the stochasticity of the datum parameters and thus consider them to be accurate with error ellipses equal to zeros.

Datum point error ellipses for the first level densification using static-dynamic approaches are similar to those obtained, for the same points, in first order free network adjustment. Also, datum point error ellipses for the second level densification using static-dynamic approaches are similar to those obtained, for the same points, in first level densification. This indicate that the static-dynamic and sub-optimal fusion approach are capable of exactly reproducing the datum point parameters together with their stochasticity.

Error ellipses resulting from densification using static approach are the smallest followed by those obtained using static-dynamic and sub-optimal fusion approaches and lastly by those obtained using dynamic approach. The implication of the error ellipse of a point is a space in which there is 0.394 probability that the estimated point lies inside, and therefore the smaller the ellipse the more accurate the point is placed. Though it need to be realized that the error ellipses resulting from static approach is attributed to the fundamental concept of considering the datum parameters as fixed non-stochastic entities and therefore not representative enough.

Static-dynamic and sub-optimal approaches which incorporate the stochasticity of the datum parameters and yield second best results to the static approach, are thus considered to be most reliable estimates. It is however indeed noticed that, in all the approaches used in densification of the simulated network, the error ellipses are symmetric.

5.4.4 Efficiency of Estimates

From the discussions in section (5.4.1) and (5.4.2) coupled with the results obtained by *Miima* [1997], results of static-dynamic densification can be considered to be the best overall. On the basis of this, the computed $\overline{\sigma}_E$, $\overline{\sigma}_N$ and $\overline{\sigma}_C$ of the sub-optimal fusion, dynamic and static densifications are tested for any significant difference from the values determined for static-dynamic densification.

The null hypothesis H_o and its alternative H_a are stated respectively as:

$$H_a:\overline{\sigma}_a^2=\overline{\sigma}_a^2$$
(5.4.5a)

$$H_o:\overline{\sigma}_s^2 > \overline{\sigma}_t^2 \tag{5.4.5b}$$

where $\overline{\sigma}_s^2$ is taken as the standard factor computed from static-dynamic densification while $\overline{\sigma}_i^2$ is the factor being tested. The test statistic in this case is defined as:

$$F_{w_1,w_2} = \frac{\overline{\sigma}_s^2}{\overline{\sigma}_\ell^2}$$
(5.4.6)

and the null hypothesis is rejected if

$$F_{m_1,m_2} > F_{\alpha,m_1,m_2}$$
 (5.4.7)

where α , m_1 and m_2 are the level of significance and degrees of freedom for the sample s and t respectively. Using a level of significance of 5% and with (5.4.7), one obtains values given in the tables below.

| | First Level Densi | ification | Second Level Densification | | |
|----------------|----------------------------|-----------|----------------------------|----------|--|
| STATIC-DYNAMIC | - | | | | |
| SUB-OPTIMAL | $F_{15,15} = 1.0751$ | Accepted | $F_{60,60} = 1.1191$ | Deserted | |
| LOSTON | $F_{0.025,15,15} = 2.4325$ | Accepted | $F_{0.025,60,60} = 1.3900$ | Accepted | |
| DYNAMIC | $F_{15.15} = 1.2011$ | Benentrad | $F_{60,60} = 1.0218$ | Decented | |
| | $F_{0.025,15,15} = 2.4325$ | Accepted | $F_{0.025,60,60} = 1.3900$ | Accepted | |
| STATIC | $F_{15,21} = 0.7030$ | Accepted | $F_{60.72} = 0.4334$ | Accepted | |
| | $F_{0.024,0.01} = 2.3375$ | Accepted | $F_{0.011} = 1.3620$ | | |

Table 5.4.3: Computed values of the test statistics for $\overline{\sigma}_{N}$ (Simulated network densification)

Table 5.4.4: Computed values of the test statistics for $\overline{\sigma}_E$ (Simulated network densification)

| | First Level Densi | fication | Second Level Densification | | |
|----------------|--------------------------------|----------|----------------------------|----------|--|
| STATIC-DYNAMIC | - | | - | | |
| SUB-OPTIMAL | $F_{15,15} = 1.421$ | Accorted | $F_{60.60} = 1.398$ | Becented | |
| EUSTON | $F_{0.025,15,15} = 2.043$ | Accepted | $F_{0.025,60,60} = 2.098$ | Accepted | |
| DYNAMIC | $F_{15,15} = 0.985$ | Accepted | $F_{60.60} = 1.453$ | Accepted | |
| | $F_{0.025,15,15} = 2.336$ | Accepted | $F_{0.025.60.60} = 2.122$ | | |
| STATIC | $F_{15,21} = 1.654$ | Accepted | $F_{60.72} = 1.378$ | Accented | |
| | $F_{0.025,15,21} = 2 \cdot 43$ | nocepted | $F_{0.025.60.72} = 2.765$ | | |
| | | | | r | |

Table 5.4.5: Computed values of the test statistics for $\overline{\sigma}_{C}$ (Simulated network densification)

| | First Level Dens | ification | Second Level Densification | |
|-----------------------|---------------------------|-----------|----------------------------|----------|
| STATIC-DYNAMIC | | | - | |
| SUB-OPTIMAL FUSION | $F_{15.15} = 1.222$ | Accented | $F_{60,60} = 1.331$ | Accepted |
| | $F_{0.025,15,15} = 2.077$ | nocpeca | $F_{0.025.60,60} = 2.076$ | |
| DYNAMIC | $F_{15,15} = 1.236$ | Accepted | $F_{60.60} = 1.334$ | Accepted |
| | $F_{0.025,15,15} = 2.345$ | Accepted | $F_{0.025,60,60} = 2.068$ | Accepted |
| STATIC | $F_{15,21} = 1.221$ | Accepted | $F_{60.72} = 1.340$ | Accepted |
| | $F_{0.025,15,21} = 2.376$ | | $F_{0.025.60,72} = 2.098$ | |

| | First Level Densification | | Second Level Densification | | |
|-----------------------|---------------------------|----------|-------------------------------|------------|--|
| STATIC-DYNAMIC | - | | - | | |
| SUB-OPTIMAL FUSION | $F_{28,28} = 1.0707$ | Accented | $F_{18,18} = 1.0671$ | Accented | |
| | $F_{0.025,28,28} = 2.038$ | Accepted | $F_{0.025,18,18}^{+} = 2.188$ | Accepted | |
| DYNAMIC | $F_{28,28} = 1.0697$ | Decontod | $F_{18_{18}} = 1.0573$ | - Accepted | |
| | $F_{0.025,28,28} = 2.277$ | Accepted | $F_{0.025,18,18} = 2.087$ | | |
| STATIC | $F_{28,50} = 0.8251$ | Accented | $F_{18.70} = 0.4097$ | Accepted | |
| | $F_{0.025,28,50} = 2.333$ | Accepted | $F_{0.025,18,70} = 2.098$ | | |

Table 5.4.6: Computed values of the test statistics for $\overline{\sigma}_N$ (Real network densification)

Table 5.4.7: Computed values of the test statistics for $\overline{\sigma}_{E}$ (Real network densification)

| | First Level Jensification | | Second Level Densification | |
|----------------|---------------------------|-----------|----------------------------|----------|
| STATIC-DYNAMIC | - | | - | |
| SUB-OPTIMAL | $F_{28,28} = 1.0725$ | Accepted | $F_{18.18} = 1.0701$ | Accented |
| 100101 | $F_{0.025,28,28} = 2.121$ | 100000000 | $F_{0.025.18.18} = 2.122$ | |
| DYNAMIC | $F_{28,28} = 1.0690$ | Accepted | $F_{18.18} = 1.0695$ | Accepted |
| | $F_{0.025,28,28} = 2.098$ | necepted | $F_{0.025,18,18} = 2.098$ | |
| STATIC | $F_{28.50} = 0.8450$ | Accepted | $F_{18.70} = 0.5060$ | Accepted |
| | $F_{0.025,28,50} = 2.039$ | moocpeed | $F_{0.025,18,70} = 2.133$ | necepted |

Table 5.4.8: Computed values of the test statistics for $\overline{\sigma}_c$ (Real network densification)

| | First Level Jensification | | Second Level Dengification | | |
|-----------------------|-----------------------------|------------|----------------------------|----------|--|
| STATIC-DYNAMIC | - | | - 11 | | |
| SUB-OPTIMAL FUSION | $F_{28,28} = 1.0717$ | Accepted | $F_{18.18} = 1.0687$ | Accented | |
| LOSION | $F_{0.025,28,28} = 1.8800$ | necepted | $F_{0.025,18,18} = 2.2450$ | Accepted | |
| DYNAMIC | $F_{28,28} = 1.0694$ | Accepted | $F_{18,18} = 1.0044$ | Accented | |
| | $F_{0.025,28,28} = 1.6500$ | necepted | $F_{0.025.18.18} = 2.2450$ | nicepted | |
| STATIC | F _{28.40} = 0.3368 | Accepted | $F_{18.70} = 0.4623$ | Accented | |
| | $F_{0.025,28,50} = 1.4300$ | Incorpecta | $F_{0.025.18.70} = 1.9200$ | Accepted | |
5.4.5 Co-ordinate Shifts

Computed shift differences in magnitude and direction between the estimated values of the densification approaches are presented in Tables (5.2.19) and (5.3.19). The shifts resulting from simulated networks are depicted graphically in Figures (5.10 to 5.15) while those resulting from real networks are depicted in Figures (5.25) to (5.30). It noticed that parameters estimated from both the static-dynamic and sub-optimal fusion approaches are closer to those estimated from static approach. This may be attributed to the fact that all these approaches keep the datum parameters unchanged. The coordinate shifts between static-dynamic and sub-optimal fusion are the second closes followed by the shifts between sub-optimal fusion and dynamic densifications. The shifts between static-dynamic and dynamic and dynamic comes last in this comparison.

DISCUSSION

Performance of the static-dynamic, sub-optimal fusion, dynamic and static approaches is discussed in this chapter, based mainly on the results in Chapter Five and the analysis of the results in Chapter Six. The discussion is presented in two parts. In the first part presented in section (6.1), the results for static-dynamic, sub-optimal fusion, dynamic and static densifications are discussed at the first level of densification while in the second part, presented in section (6.2), the results for static-dynamic, sub-optimal fusion, dynamic and static densifications are discussed at the second level of densification.

6.1 The First Level of Densification

First level of densification was performed by intercalation of the second order points into the first order points {cf. Figure (4.3) and Figure (4.6)}. The results of the first level densification of both real and simulated networks indicate that the standard errors as estimated for the new points in the dynamic approach are generally very close to those estimated in the static-dynamic and sub-optimal fusion approaches. In fact, as realized by *Aduol [1993]*, if the standard errors are multiplied by the factor $\frac{\sigma_0}{\sigma_0}$, then practically one obtains equal standard errors from dynamic, static-dynamic and sub-optimal fusion approaches. This implies therefore that if standard errors are static-dynamic and sub-optimal fusion approaches. This implies therefore that if standard errors are are obtained by taking σ_0^2 same as σ_0^2 then the standard errors obtained from the dynamic, static-dynamic and sub-optimal approaches are all equal.

The set of standard errors of the estimated parameters through use of the static-dynamic and the sub-optimal fusion approaches were very close to those estimated through the use of the dynamic approach in both the real and simulated network densifications. The computed average standard errors for the four experiments, though statistical tests show that there were no significant differences between them, their magnitude varied significantly. The average standard

errors are ± 23.32 mm, ± 21.76 mm, ± 24.94 mm, and ± 19.51 mm for the static-dynamic, the suboptimal fusion, the dynamic and the static densifications respectively in the first level real network densification while in the first level simulated network densification they are ± 3.55 mm, ± 3.81 mm, ± 4.25 mm and ± 2.48 mm for static-dynamic, sub-optimal fusion, dynamic and static densifications respectively. Correspondingly, the average standard errors are ± 23.83 mm, ± 22.30 mm, ± 23.72 mm and ± 11.02 mm for the static-dynamic, the sub-optimal fusion, the dynamic and the static densifications respectively in the second level real network densification while in the second level simulated network densification they are ± 2.82 mm, ± 3.16 mm, ± 2.89 mm and ± 1.21 mm for the static-dynamic, the sub-optimal fusion, the dynamic and the static densifications respectively.

In the static-dynamic and sub-optimal fusion approaches, the first level densification was undertaken, with the datum stations 1 to 11 in the real network and datum stations 1 to 3 in simulated network case being treated as fixed stochastic entities. This is the reason why these points have their error ellipses similar to the error ellipses obtained in the first order network adjustment by use of the free network adjustment technique. {cf. Figures (5.2), (5.4), (5.17) and (5.19)}. Similarly, the second level densification was undertaken, with the datum stations 1 to 26 in the real network and datum stations 1 to 6 in simulated network case being treated as fixed stochastic entities. This is the reason why these points have their error ellipses similar to the error ellipses obtained in the first level real and simulated network densifications by use of the static-dynamic and the sub-optimal fusion approaches. {cf. Figures (5.3), (5.5), (5.18) and (5.20)}. This is the essence of the reproducing property depicted by the static-dynamic and the sub-optimal fusion approaches.

It is noted that in the static approach, the first level of densification was undertaken with the datum points 1 to 11 in the real network and datum points 1 to 3 in the simulated network being treated as fixed non-stochastic entities. Therefore, as expected, the error ellipses of these points are equal to zero. Similarly, in the second level densification, datum points 1 to 26 in the real network and datum points 1 to 6 in the simulated network have their error ellipses equal to zero.

In the dynamic approach, the densification was performed by treating the datum parameters as stochastic entities (i.e. the use of the dynamic approach) resulting in larger error ellipses compared to both static-dynamic and sub-optimal fusion approaches. In the dynamic densification, all points have error ellipses that are different from the previously determined

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error ellipses and therefore lacks the reproducing capability {cf. Figures (5.6), (5.7), (5.21) and (5.22)}. It is though noticeable that all point error ellipses for the datum stations are relatively smaller compared to those that were determined in previous adjustment. The point error ellipses in the second level densification are smaller compared to point error ellipses in the first level densification determined earlier. Thus the point error ellipses and standard errors of the estimated parameters in the dynamic approach tend to improve or become smaller with the increase in densification levels. This, as noted by *Aduol [1993]*, may be attributed to the increase in redundancy in the geodetic system with addition of new observations. It is though important to note that despite the rigorous nature of this approach to densification, due to incorporation of the stochasticity of the datum points in the densification, the datum points are estimated anew resulting in a technical handicap as the concept of control for national geodetic references loses meaning.

The apparent similarity in the behaviour of error ellipses in the dynamic, static-dynamic and sub-optimal fusion approaches both at the first level and second level densification of the real and simulated networks is to be expected since the dynamic, the static-dynamic and the sub-optimal fusion approaches are similar in principle. The differences in the results obtained are due to the mode of application i.e. which datum parameters are kept fixed in the static-dynamic and sub-optimal cases. In fact, the basis of the sub-optimal fusion approach is the estimation of the new point parameters according to the dynamic approach while applying a corrective term on the datum points parameters to keep them unchanged. This is clearly illustrated by the comparison of shifts of points from their position after phasing to their position as a result of dynamic and sub-optimal fusion approaches presented in Figures (5.13) and (5.28).

6.2 The Second Level of Densification

At second level of densification, the results of the first level of densification were densified into a third order network. From Tables (5.2.5), (5.3.5), (5.2.9), (5.3.9), (5.2.13) and (5.3.13) the static-dynamic and sub-optimal fusion approaches yielded relatively smaller error ellipses as compared to the dynamic approach. It is however noted that, as in the first level of densification, error ellipses resulting from the static approach are the smallest. It is observed that the order of accuracy of determined parameters at this level is similar to that of first level of densification. However it is noticed that numerical values of accuracies decrease at this level for all approaches which indicate a general improvement of accuracy in the higher order geodetic systems. This was not expected as it is expected that the accuracy should reduce with increase in densification levels. This can be attributed to the increase in redundancy in the geodetic systems.

From section 5.4.1 the analysis indicates that the estimated a-posteriori variance of unit weight for all the approaches at all levels of densification were statistically equal to the a-priori variance of unit weight. This therefore indicates that the estimation processes were correctly carried out and specifically that the approaches relate to unknown parameters completely and correctly.

The efficiency of estimates tested in section 5.4.4 indicated no significant differences between the computed circular probable error for all the experiments at both level of densification. While this signified the validity of the estimates determined, it is attributed to the fact that the parameters used as estimates in the study were in fact computed final point coordinates from Survey of Kenya records in the case of the real network while the parameters for the simulated network were close enough to the expected values. This therefore resulted in the closeness of the determined estimates which has resulted in the determined accuracy being very close in magnitude.

6.3 Concluding Remarks

The dynamic, static-dynamic and sub-optimal fusion approaches all incorporate stochasticity of the datum parameters in the estimation of new point parameters except that in the staticdynamic and the sub-optimal fusion approaches the datum parameters are maintained definitive while in the dynamic approach all the parameters are estimated afresh. It is the lack of reproducing characteristic that makes the dynamic approach relatively unattractive in practical application in situations requiring the maintenance of the datum. The static approach to densification does not incorporate the stochasticity of the datum point parameters in the estimation of new point parameters and is thus considered to lack the reproducing property.

Using the analysis of the computations, classification of the viability of the approaches to densification of geodetic networks would be the static approach, followed by the static-dynamic approach then the sub-optimal approach and lastly the dynamic approach. But the static densification approach has the special problem that datum points are 'forced' to be exact when they in fact are not. Though normally applied, the approach has the effect of turning out results

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which are too optimistic in terms of their stochasticity; especially if the a-priori variance of unit weight is adopted. As a result, the static-dynamic and sub-optimal fusion approaches are considered to be more acceptable than the dynamic and static approaches. The dynamic approach though, may be preferred in densification of geodetic systems in certain circumstances for instance in isolated precise engineering networks in which there is no need to fix the datum points. Such networks would include those used in the analysis of deformation of engineering structures like dams. The dynamic approach is also used in the adjustment of scientific research networks such as those used in crustal deformation monitoring.

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CONCLUSION AND RECOMMENDATIONS

Summary of the work done is presented in this chapter together with the findings and recommendations arising from the study.

7.1 Preamble

The main objective of the study was to demonstrate practical applicability and to evaluate the suitability of the sub-optimal fusion approach to densification in relation to the static, dynamic and static-dynamic approaches.

In order for the objective to be realized, static-dynamic, sub-optimal fusion, dynamic and static approaches to densification were used to estimate parameters for two networks, one of which was extracted from a part of the Kenyan geodetic network, dubbed the real network, and the other was a simulated network. The real network consists of eleven first order, fifteen second order and fifteen third order points while the simulated network consists of three first order, three second order and nine third order points. {cf. section (4.2)}. The networks were densified under each of the four densification approaches considered.

The results of the four approaches are close to one another in the real network case and this may be attributed to the fact that the approximate coordinates were actually adjusted final coordinates from Survey of Kenya records office. In the simulated network results, the closeness may be attributed to smaller dispersions of the observation from their adjusted values. In the dynamic approach, datum points are estimated afresh while in the static-dynamic and sub-optimal fusion, the datum parameters are held definitive.

7.2 Conclusions

The use of the dynamic approach incorporates the stochasticity of the datum parameters which is the first condition of choice of a viable densification approach. Unfortunately, the approach results in all the datum parameters being re-estimated afresh and thus fails the second condition of choice, that is to reproduce the datum parameters. This has led to the conclusion that the dynamic approach cannot be effectively used in cases where datum parameters have to be reproduced as is the case with any national reference datum. The approach though can be used in special situations where the datum needs not be maintained.

The static approach does not incorporate the stochasticity of the datum parameters in the estimation of the new point parameters and therefore fails the first condition of choice of a viable densification approach. Even though the approach results in datum parameters being retained fixed, it is considered to fail the second condition too.

The results indicate that the datum parameters obtained in the static-dynamic and the suboptimal fusion approaches are reproduced together with their stochasticity, that is maintained definitive. Although the sub-optimal fusion approach has the reproducing property, the new point parameters obtained are exactly similar to the parameters obtained using dynamic approach. That is, it compares to performing network densification using the dynamic approach and applying a corrective term on the datum parameters to keep them unchanged. The approach therefore accomplishes the short falls of the dynamic approach.

It can therefore be concluded that both static-dynamic and sub-optimal fusion approaches can be effectively considered as the best suited approaches to the densification of geodetic systems.

7.3 Recommendations

From the comparisons of the dynamic, static-dynamic and sub-optimal fusion approaches to densification of geodetic networks and the analysis of the results obtained, it is recommended that the static-dynamic and sub-optimal fusion are both viable approaches to densification of **geodetic** networks.

Also as a further test to the four densification approaches studied, it is recommended that they be subjected to the densification of three and four dimensional geodetic systems.

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Appendices

APPENDIX A: PROGRAM LISTINGS AND FLOWCHART DIAGRAMS

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APPENDIX A.1 FREE M PROGRAM FLOWCHART



APPENDIX A.2: FREE M PROGRAM

```
clear all
PROGRAM TO PERFORM FREE NETWORK ADJUSTMENT
angobs =? % number of angles observed
disobs =? % number of distances observed
totobs = ? % number of total observations
points=?
          % number of network points
          % number of unknown parameters = twice number of network points
new=?
cond=?
          % number of conditions
fid=fopen('angobs1A.txt'.'r');
RA=fscanf(fid, '%g %g %g %g %g', [5 angobs]) %the matrix has angobs rows
fclose(fid)
for i=1:angobs
 kpl(i)=RA(1,i);
 kp2(i)=RA(2,i);
 ideg(i)=RA(3,i);
 min(i)=RA(4,i);
 sec(i)=RA(5,i);
end
fid=fopen('disobs1A.txt'.'r');
B=fscanf(fid.'%g %g %g'.[3 disobs]) % the matrix disobs rows
fclose(fid)
for i=1:disobs
  ip1(i)=B(1,i);
  ip2(i)=B(2,i);
 dist(i)=B(3,i);
end
fid=fopen('coord1A.txt'.'r');
C=fscanf(fid. %g %g %g'.[3 points]) % the matrix has point rows
fclose(fid)
for i=1:points
  kp(i)=C(1,i);
 y(i)=C(2,i);
  x(i)=C(3.i);
 %STORING THE PROVISIONAL COORDINATES
 x0(i)=x(i);
 v0(i)=v(i);
end
ITERATE=0:
ii=1;
VUW(ii)=1;
VUW(ii+1)=0;
fid=fopen('output I A.txt'.'w')
               PROVISIONAL VALUES\n')
fprintf(fid.'
fprintf(fid.' POINT Y-COORDINATES X-COORDINATES\n')
fprintf(fid. %4.0f %16.3f %18.3f n'.C)
while (abs(VUW(ii)-VUW(ii+1)) \le 0.001)
  ITERATION=ITERATION+1:
 %FORMATION OF DESIGN MATRIX A1 FOR THE DISTANCES
 for i=1:disobs
  jl=ipl(i);
  j2=ip2(i);
  denom1(i)=sqrt((x(j2)-x(j1))^2-(y(j2)-y(j1))^2);
 j3=j1*2-1;
 j4=j1*2;
  A1(i,j3)=(x(j1)-x(j2))/denom1(i);
  A1(i,j4)=(v(j1)-v(j2))/denom1(i);
 j5=j2*2-1;
```

```
i6=i2*2;
  A1(i,j5)=(x(j2)-x(j1))/denom1(i);
  A1(i,j6)=(y(j2)-y(j1))/denom1(j);
  Y1(i)=dist(i)-denom1(i);
  W1(i,i)=VUW(ii)^{2}/((0.003^{2})+(dist(i)*0.000001)^{2});
end
%FORMATION OF DESIGN MATRIX A2 FOR THE DIRECTIONS
sin1=206264.80626
for i=1:angobs
  ml=kpl(i);
  m2=kp2(i);
  denom2(i)=(x(m2)-x(m1))^{2}+(y(m2)-y(m1))^{2};
  m3=m1*2-1;
  m4=m1*2;
  A2(i,m3)=(y(m2)-y(m1))/denom2(i)*sin1;
  A2(i,m4)=(x(m1)-x(m2))/denom2(i)*sin1;
  m5=m2*2-1;
  m6=m2*2;
  A2(i,m5)=(y(m1)-y(m2))/denom2(i)*sin1;
  A2(i.m6)=(x(m2)-x(m1))'denom2(i)*sin1;
  ANGO(i) = (ideg(i) - min(i)/60.0 + sec(i)/3600.0);
 del(i)=x(m2)-x(m1):
 dn1(i)=y(m2)-y(m1);
 bear(i)=quad(dn1(i).de1(i));
 ANG1(i)=bear(i)*180/pi:
 Y2(i)=(ANG0(i)-ANG1(i))*3600.0;
 W2(i,i)=VUW(ii)^2/0.5/2;
end
%FORMATION OF THE COMPLETE DESIGN MATRIX, WEIGHT MATRIX AND Y-VECTOR
for i=1:totobs
 for j=1:new
   if(i<=disobs)
     A(i,j)=A1(i,j);
     Y(i,1)=Y1(i);
     W(i,i) = W1(i,i);
   else
    kk=i-disobs
    A(i,j)=A2(kk,j);
     Y(i,1)=Y2(kk);
    W(i,i)=W2(kk,kk);
   end
 end
end
%FORMATION OF THE RESTRICTION MATRIX
for i=1:4
 for j=1:new
   G(i,j)=0.0;
 end
end
for i=1:points
 n1=2*i-1;
 n2=2*i;
 G(1,n1)=1.0;
 G(2,n2)=1.0;
 G(3,n1)=y(i)-9624020.73;
 G(3,n2) = -1.0*(x(i)-585465.74);
 G(4,n1)=x(i)-585465.74;
 G(4,n2)=y(i)-9624020.73;
end
RNI=inv(A'*W*A+G'*G);
```

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```

```
FII=(RNI-RNI*G'*G*RNI):
 DX=F11*A'*W*Y:
 E=Y-A*DX:
 for i=1:78
  if(i \le 26)
   E1(i,1)=E(i,1);
   else
   m=i-26;
    E2(m,1)=E(i,1);
  end
end
 %COMPUTING VARIANCE COMPONENTS
 WII=inv(WI);
 W2I=inv(W2);
 QQE1=W1*(W1I);%-A1/(A1'*W1*A1)*A1');
 QQE2=W2*(W2I);%-A2/(A2'*W2*A2)*A2');
 TRACE1=trace(QQE1);
 TRACE2=trace(QQE2);
 VC1(ii)=(E1'*W1*E1)/TRACE1;
 VC2(ii)=(E2'*W2*E2)/TRACE2;
 VUW(ii+1)=(E1'*W1*E1-E2'*W2*E2)/(TRACE1+TRACE2);
 COVX=VUW(ii+1)*(F11*A'*W*A*F11');
 COVY=A*COVX*A';
 ii=ii+1
End % end while
%ADJUSTING THE OBSERVATIONS
for i=1:78
 if(i \le 26)
   Adist(i)=dist(i)-E(i,1);
 else
   11 = i - 26
   ANG(11)=ANG0(11)*3600.0-E(i,1):
   idegf(11) = fix(ANG(11)/3600.0);
   rmin(11)=(ANG(11)/3600.0-idegf(11))*60.0;
   minf(11)=fix(rmin(11));
   secf(11)=(rmin(11)-minf(11))*60.0;
 end
end
%STANDARD ERROR OF THE OBSERVATIONS
for i=1:78
 OBE(i)=sqrt(abs(COVY(i,i)));
end
%UPDATING THE PROVISIONAL VALUES
for i=1:11
 jj=2*i-1;
 mm=2*i;
 x(i)=x(i)+DX(jj);
 y(i)=y(i)+DX(mm);
% correction to provisional values
 CX(i)=x0(i)-x(i);
 CY(i)=y0(i)-y(i);
end
%STANDARD ERROR OF THE ADJUSTED PARAMETERS
for i=1:22
 STD(i)=sqrt(COVX(i,i));
end
%COMPUTING THE ERROR ELLIPSE PARAMETERS
for i=1:11
 k=2*i-1:
 VARX(i)=COVX(k,k);
```

```
m=2*i:
 VARY(i)=COVX(m,m);
 COVXY(i)=COVX(k,m);
 a(i)=(0.5*(VARX(i)+VARY(i))+(0.25*(VARX(i)-VARY(i))^2+COVXY(i)^2)^0.5)^0.5;
 b(i)=(0.5*(VARX(i)+VARY(i))-(0.25*(VARX(i)-VARY(i))^2+COVXY(i)^2)^0.5)^0.5;
 theta(i)=atan((2*COVXY(i))/(VARX(i)-VARY(i)));
 if(theta(i) \le 0)
   theta(i)=2*pi+theta(i);
 end
 direct(i)=theta(i)*180.0/pi;
 PE(i)=((VARX(i)+VARY(i))/2.0)^0.5;
 degt(i)=fix(direct(i));
 rrr=(direct(i)-degt(i))*60.0;
 mint(i)=fix(nT);
 sect(i)=(rrr-mint(i))*60.0;
end
% NETWORK MEAN ERROR
 TRACE3=trace(COVX);
NWERROR=sqrt(TRACE3/22);
ETWE1=E1'*W1*E1;
ETWE2=E2'*W2*E2;
fprintf(fid,' ITERATION = %4.0f VUW= %10.6f\n',ITERATE,VC1(ii)+VC2(ii))
% OUTPUTS
0/0*****
fprintf(fid.'
                 RESULTS\n')
fprintf(fid,' DISTANCE : TRACE1= %8.3f ETWE1= %8.3f\n',TRACE1,ETWE1)
fprintf(fid,' DIRECTIONS : TRACE2= %8.3f ETWE2= %8.3f\n',TRACE2,ETWE2)
fprintf(fid,'POINT Y-COORD X-COORD
                                            STD-Y STD-X RESIDUAL-Y RESIDUAL-X\n')
fprintf(fid.'
                       (m)
                               (m)
                                                    (m)(n')
               (m)
                                      (m)
                                            (m)
for i=1:11
 II=i*2-1:
 mm=i*2;
fprintf(fid, '%5.0f %12.3f %12.3f %8.4f %7.4f %10.4f %12.4f\n', kp(i), y(i), x(i), STD(mm), STD(II), CY(i), CX(i))
end
fprintf(fid,'
           ADJUSTED OBSERVATIONS\n')
fprintf(fid,'
          ADJUSTED DISTANCES n')
fprintf(fid,' RAY
                  OBSERVED-DIST ADJUSTED-DIST STD-ERR RESIDUÁLS\n')
fprintf(fid.'
                 (m)
                             (m)
                                      (m)
                                             (m)(n')
for i=1:26
 fprintf(fid, %2.0f %2.0f %17.3f %17.3f %11.3f %11.3f %11.in(i),ip2(i),dist(i),Adist(i),OBE(i),E(i,1))
end
fprintf(fid,' ADJUSTED DIRECTIONS\n)
fprintf(fid,' RAY OBSERVED-DIRECT ADJUSTED-DIRECT STD-ERR RESIDUALS\n')
                              ") (")
fprintf(fid,'
                    ") (
            (
                                            (")\n')
for i=1:52
 l = i + 26
 fprintf(fid, %2.0f %2.0f %5.0f %4.0f %7.2f %5.0f %4.0f %7.2f %9.3f
%11.2f\n'.kp1(i),kp2(i),ideg(i).min(i),sec(i),idegf(i),minf(i),secf(i),OBE(1),E(1,1))
end
fprintf(fid,' ERROR ELLIPSE PARAMETERS\n')
fprintf(fid,'POINT SEMI-MAJOR AXIS(a) SEMI-MINOR AXIS(b) DIRECTION\n')
for i=1:11
fprintf(fid, '%3.0f %12.6f %25.6f %8.0f %4.0f %7.2f\n', i, a(i), b(i), degt(i), mint(i), sect(i))
end
fprintf(fid,' NETWORK ERROR=%10.5f\n',NWERROR)
ITERATE=ITERATE+1;
end %end ii
```

```
% PLOTTING THE ERROR ELLIPSES
plot(x,y,'ro')
hold;
axis([500000 627419 9570000 9670000])
xlabel('X-Coordinate (Eastings)')
ylabel('Y-Coordinate (Northings)')
title('REAL PRIMARY NETWORK')
for i=1:26
 ml = ipl(i);
 m2=ip2(i);
 xx = [x(m1) x(m2)];
 yy=[y(m1),y(m2)];
 plot(xx,yy,'g-')
end
for k=1:11
 n=60;
 theta=(-n:2:n)/n*pi;
 %THE POINT ELLIPSES
 xxx=a(k)*cos(theta)*10e5*0.4;
 yyy=b(k)*sin(theta)*10e5*0.4;
 %THE ROTATION MATRIX
 g(k)=degt(k)+mint(k)/60+sect(k)/3600;
 phi=(g(k)/180)*pi;
 R(1,1)=sin(phi);
 R(1,2)=\cos(phi);
 R(2,1)=\cos(phi);
 R(2,2) = -\sin(phi);
 %ROTATE THE ELLIPSE ACCORDING TO THE ANGLE OF INCLINATION
 for i=1:n+1
   for j=1:n+1
    xy=[xxx(1,j) yyy(1,j)];
    RXY=R*xy';
    xR(i,j)=RXY(1);
    yR(i,j)=RXY(2);
   end
 end
 xxx=xR;
 yyy=yR;
 %TRANSLATE THE FIGURE
 xxp=x(k);
 yyp=y(k);
 ox=xxp*ones(n+1);
 oy=yyp*ones(n+1);
 xxx=(xxx+ox); %scaling
 yyy=(yyy+oy); %scaling
 plot(xxx.yyy,'r.');
end
% NETWORK NUMBERING
gtext('1')
gtext('2')
gtext('3')
gtext('4')
gtext('5')
gtext('6')
gtext('7')
gtext('8')
gtext('9')
gtext('10')
```

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gtext('11') % DRAWING SCALE BAR text(520000,9640000,'Network:') sx1=[540000 550000]; sy1=[9640000 9640000]; plot(sx1,sy1,'b-'); gtext('10Km') text(520000,9630000,'Ellipse:') sx2=[540000 546400]; sy2=[9630000 9630000]; plot(sx2,sy2,'b-'); gtext('20mm') % DRAWING DIRECTION BAR bx=[620000 620000]; by=[9580000 9590000]; plot(bx,by,'b-') gtext('N') text(525000,9650000.'SCALE:') fclose(fid)

APPENDIX A.3: DENSITY M PROGRAM FLOWCHART



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APPENDIX A.4: DENSITY.M PROGRAM

```
clear all
%REAL SECONDARY NETWORK (STATIC-DYNAMIC APPROACH)
% READING THE OBSERVED DIRECTIONS
echo off
angobs =? % number of angles observed
disobs =? % number of distances observed
totobs = ? % number of total observations
points=? % number of network points
new=?
        % number of unknown parameters = twice number of network points
cond=?
        % number of conditions
fid=fopen('angobs2.txt','r');
RA=fscanf(fid,'%g %g %g %g %g',[5 angobs])% has angobs rows
fclose(fid)
for i=1:angobs
   kpl(i) = RA(1, i);
   kp2(i)=RA(2,i);
   ideg(i) = RA(3, i);
   min(i) = RA(4, i);
   sec(i) = RA(5, i);
end
% READING THE OBSERVED DISTANCES
fid=fopen('disobs2.txt','r');
B=fscanf(fid,'%g %g %g',[3 disobs])% has disobs rows
fclose(fid)
for i=1:disobs
   ip1(i)=B(1,i);
   ip2(i)=B(2,i);
   dist(i) = B(3, i);
end
% READING THE PRIMARY NETWORK OBSERVED DISTANCES FOR PLOTTING
fid=fopen('disobslA.txt','r');
CB=fscanf(fid,'%g %g %g',[3 26])% has 26 rows
fclose(fid)
for i=1:26
   cip1(i) =CB(1,i);
   cip2(i)=CB(2,i);
   cdist(i)=CB(3,i);
end
% READING THE PROVISIONAL COORDINATES
fid=fopen('coord2.txt','r');
C=fscanf(fid,'%g %g %g',[3 points])% has points rows
fclose(fid)
for i=1:points
   kp(i) = C(1, i);
   y(i) = C(2, i);
                                                            14.1
   x(i) = C(3, i);
   %STORING THE PROVISIONAL COORDINATES
   x0(i) = x(i);
   y0(i) = y(i);
end
ITERATE=0;
OUTPUTING THE PROVISIONAL COORDINATES
fid=fopen('output2a.txt','w')
fprintf(fid,'
                       PROVISIONAL VALUES\n')
fprintf(fid, ' POINT
                       Y-COORDINATES
                                           X-COORDINATES\n')
fprintf(fid,'%4.0f %16.3f %18.3f\n',C)
VUW(1) = 1
                                1
```

```
&FORMATION OF DESIGN MATRIX A1 FOR THE DISTANCES
for i=1:disobs
   jl=ipl(i);
   j2=ip2(i);
   denom1(i) = sqrt((x(j2)-x(j1))^2+(y(j2)-y(j1))^2);
   j3=j1*2-1;
   j4=j1*2;
   A1(i, j3) = (x(j1) - x(j2)) / denom1(i);
   A1(i, j4) = (y(j1) - y(j2)) / denoml(i);
   j5=j2*2-1;
   j6=j2*2;
   A1(i, j5) = (x(j2) - x(j1)) / denom1(i);
   Al(i, j6) = (y(j2) - y(j1)) / denoml(i);
   Yl(i)=dist(i)-denoml(i);
   W1(i,i)=VUW(ii)^2/((0.01^2)+(dist(i)*0.000001)^2);
end
&FORMATION OF DESIGN MATRIX A2 FOR THE DIRECTIONS
sin1=206264.80626
for i=1:angobs
   ml=kpl(i);
   m2=kp2(i);
   denom2(i) = ((x(m2)-x(m1))^{2}+(y(m2)-y(m1))^{2});
   m3=m1*2-1;
   m4=m1*2;
   A2(i, m3) = (y(m2) - y(m1)) / denom2(i);
   A2(i, m4) = (x(m1) - x(m2)) / denom2(i);
   m5=m2*2-1;
   m6=m2*2;
   A2(i, m5) = (y(m1) - y(m2)) / denom2(i);
   A2(i, m6) = (x(m2) - x(m1)) / denom2(i);
   ANGO(i) = (ideg(i) + min(i) / 60.0 + sec(i) / 3600.0);
   del(i) = x(m2) - x(m1);
   dnl(i) = y(m2) - y(m1);
   bear(i) = guad(dn1(i), de1(i));
   ANG1(i)=bear(i)*180/pi;
   Y2(i)=(ANGO(i)-ANG1(i))*pi/180.0;
  W2(i,i)=VUW(ii)^2/(1.0*pi/648000)^2;
end
&FORMATION OF THE COMPLETE DESIGN MATRIX, WEIGHT MATRIX AND Y-VECTOP
for i=1:totobs
   for j=1:angobs
      if(i<=disobs)
         A(i,j)=A1(i,j.;
         Y(i, 1) = Y1(i);
         W(i,i)=W1(i,i;;
      else
         kk=i-disobs
         A(i,j) = A2(kk,j);
         Y(i, 1) = Y2(kk);
                                                           141
         W(i,i) = W2(kk,kk);
      end
  end
Ind
FORMATION OF THE DESIGN MATRIX FOR THE FIDUCIAL POINTS WITH & WITHCUT PRIOR
NFORMATION (A3&A4)
pr i=1:totobs
   for j=1:angobs
      if(j<=cond)
         % with prior information
         A3(i,j) = A(i,j);
                                        147
```

```
else
         -without prior information
         kk=i-cond;
         A4(i,kk) = A(i,j);
      end
   end
end
PRIOR INFORMATION
%standard error of the fiducial points
std=[0.0125 0.0166 0.0119 0.0109 0.0093 0.0099 0.0093 0.0083 0.0082 0.0074
0.0091 0.0075 0.0075 0.0072 0.007 0.0057 0.0073 0.0078 0.0067 0.0071 0.0078
0.00851
Sobservational error of the fiducial points
E3=[-0.0389 0.1003 -0.0328 -0.0214 0.0698 -0.0393 0.0009 -0.042 0.0961 -
0.0068 -0.0077 0.031 -0.0159 -0.0438 0.0437 0.0329 -0.0305 -0.0314 -0.0399 -
0.0596 -0.0448 0.0802]
MANIPULATION FOR THE STATIC-DYNAMIC APPROACH
a=[0.016857 0.012603 0.010512 0.009571 0.008686 0.009283 0.007735 0.007007
0.007839 0.007062 0.008967]
b=[0.012139 0.010018 0.008578 0.008035 0.006867 0.007263 0.006954 0.005729
0.007254 0.006689 0.0072]
direct=[29.36586389 291.9689194 71.24367778 309.342461111 297.681297222
319.52852777 290.290191666 352.417841666 353.593372222 1.979458333
68.216416666]
for i=1:cond
   Wr(i,i)=VUW(ii)^2/std(i))^2;
   WrI(i,i)=(std(i))^2/VUW(ii)^2;
end
for i=1:points
   mm=2*i-1;
   nn=2*i;
   r(mm, 1) = x(i) + E3 / mm;
   r(nn,1)=y(i)+E3'nn ;
end
for i=1:totobs
   WI(i,i)=1.0/W(i,i);
end
OOO=inv(WI+A3*WrI*A3' ;
DX=inv(A4'*QQQ*A4)*(A4'*QQQ*Y);
                                                               11
E=Y-A4*DX;
for i=1:totobs
   if(i<=disobs)
      El(i, 1) = E(i, 1);
   else
      m=i-disobs;
      E2(m, 1) = E(i, 1);
   end
end
for i=1:cond
   EE3(1,i)=E3(i);
end
E3=EE3'
*COMPUTING VARIANCE CCMPONENTS
W1I=inv(W1);
W2I=inv(W2);
QQE1=W1*(W1I); - (A1/(A1'*W1*A1)*A1'));
QQE2=W2*(W2I); -- (A2/(A1'*W2*A2)*A2'));
QQE3=Wr*WrI;
TRACE1=trace(QQE1);
TRACE2=trace(QQE2);
TRACE3=trace(QQE3);
```

```
VC1=(E1'*W1*E1)/TRACE1;
VC2=(E2'*W2*E2)/TRACE2;
VC3=(E3'*Wr*E3)/TRACE3;
VUW(ii+1)=((E1'*W1*E1)+(E2'*W2*E2)+(E3'*Wr*E3))/(TRACE1+TRACE2+TRACE3);
COVX=inv(A4'*QQQ*A4);
formation of the complete covariance matrix
ior i=1:angobs
   if(i<=cond)
      COV(i,i) = (std(i))^2;
   else
      kk=i-cond;
      COV(i,i)=COVX(kk,kk);
   end
end
COVY=A*COV*A';
BADJUSTING THE OBSERVATIONS
for i=1:totobs
   if(i<=cond)
     Adist(i) = dist(i) - E(i, 1);
 else
     ll=i-cond
  ANG(11) = ANG0(11) * pi/180.0-E(i,1);
  ANG1(11) = ANG(11) * 180/pi;
  idegf(l1)=fix(ANG1(l1));
    rmin(l1) = (ANG1(l1) - idegf(l1)) * 60.0;
    minf(l1) = fix(rmin(l1));
   secf(l1) = (rmin(l1) -minf(l1)) *60.0;
   end
end
-STANDARD ERROR OF THE OBSERVATIONS
for i=1:totobs
   if(i<=disobs)
    OBE(i) = sqrt(abs(COVY(i,i)));
   else
   OBE(i) = sqrt(abs(COVY(i,i)))*sin1;
   end
end
-UPDATING THE PROVISIONAL VALUES
for i=1:points
  j=i-cond/2;
   jj=2*j-1;
  mm=2*j;
  x(i) = x(i) + DX(jj);
  y(i) = y(i) + DX(mm);

    correction to provisional values

  CX(i) = x0(i) - x(i);
  CY(i) = y0(i) - y(i);
end
STANDARD ERROR OF THE ADJUSTED PARAMETERS
for i=1:angobs
  STD(i) = sqrt(COV(i,i));
end
                                                           10.10
COMPUTING THE ERROR ELLIPSE PARAMETERS
for i=1:points
  j=i-cond/2;
  k=2*j-1;
  VARX(i)=COVX(k,k);
  m=2*j;
  VARY(i)=COVX(m,m);
  COVXY(i)=COVX(k,m;;
```

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```
a(i) = (0.5*(VARX(i)+VARY(i))+(0.25*(VARX(i)-
VARY(i))^2+COVXY(i)^2)^0.5)^0.5;
  b(i)=(0.5*(VARX(i)+VAFY(i))-(0.25*(VARX(i)-
VARY(i))^2+COVXY(i)^2)^0.5)^0.5;
   theta(i) = atan((2*COVXY(i))/(VARX(i)-VARY(i)));
 if(theta(i)<=0)
     theta(i)=2*pi+theta(i);
 end
  direct(i)=theta(i)*180.0/pi;
   PE(i) = ((VARX(i) + VARY(i)) / 2.0) ^0.5;
end
for i=1:points
 degt(i) = fix(direct(i));
  rrr=(direct(i)-degt(i))*60.0;
  mint(i) = fix(rrr);
  sect(i) = (rrr-mint(i)) * 60.0;
end
% NETWORK MEAN ERROR
TRACE3=trace(COV);
NWERROR=sqrt(TRACE3/58);
ETWE1=E1'*W1*E1;
ETWE2=E2'*W2*E2;
fprintf(fid,' ITERATION = %4.0f VUW= %10.6f\n', ITERATE, VUW(ii))
end %end while
******
% OUTPUTS
fprintf(fid, '
                            RESULTS\n ')
fprintf(fid, ' DISTANCE
                       : TRACE1= %8.3f ETWE1= %8.3f\n',TRACE1,ETWE1)
fprintf(fid,' DIRECTIONS : TRACE2= %8.3f ETWE2= %8.3f\n',TRACE2,ETWE2)
fprintf(fid, 'POINT Y-COORD X-COORD
                                              STD-Y
                                                      STD-X RESIDUAL-Y
RESIDUAL-X\n')
for i=1:points
   11=i*2-1;
  mm=i*2;
fprintf(fid, '%5.0f %12.3f %12.3f %8.4f %8.4f %10.4f
%11.4f\n',kp(i),y(i),x(i),STD(mm),STD(ll),CY(i),CX(i))
end
fprintf(fid, '
                 ADJUSTED OBSERVATIONS\n')
fprintf(fid, '
                 ADJUSTED DISTANCES\n')
fprintf(fid, ' RAY
                        OBSERVED-DIST
                                         ADJUSTED-DIST
                                                          STD-ERR
RESIDUALS\n')
for i=1:disobs
  fprintf(fid, '%2.0f %2.0f %17.3f %17.3f %11.4f
%11.4f\n',ip1(i),ip2(i),dist(i),Adist(i),OBE(i),E(i,1))
end
fprintf(fid, '
                ADJUSTED DIRECTIONS\n')
fprintf(fid,' RAY OBSERVED-DIRECT
                                      ADJUSTED-DIRECT
                                                          STD-ERR
RESIDUALS(")\n')
for i=1:angobs
                                                    14.11
  l=i+disobs
   fprintf(fid,'%2.0f %2.0f %5.0f %4.0f %7.2f %5.0f %4.0f %7.2f %9.4f
%11.2f\n',kp1(i),kp2(i),ideg(i),min(i),sec(i),idegf(i),minf(i),secf(i),OBE(1)
,E(1,1)*sin1)
end
fprintf(fid,'
               ERROR ELLIPSE PARAMETERS\n')
fprintf(fid, 'POINT SEMI-MAJOR AXIS(a) SEMI-MINOR AXIS(b)
DIRECTION\n')
for i=1:points
fprintf(fid,'%3.0f %12.6f %25.6f %8.0f %4.0f
%7.2f\n',i,a(i),b(i),degt(i),mint(i),sect(i))
```

end
fprintf(fid,' NETWORK ERROR= %10.5f\n',NWERROR)
ITERATE=ITERATE+1;

```
%PLOTTING THE ERROR ELLIPSES
for i=1:points
 cy(i) = y(i);
 cx(i) = x(i);
end
for i=1:points
 l=i-cond/2;
ny(1) = y(i);
 nx(1) = x(i);
end
plot(cx,cy,'ro')
hold
plot(nx,ny,'b.')
axis([500000 627419 9570000 9670000])
xlabel('X-Coordinate (Eastings)')
ylabel('Y-Coordinate (Northings)')
%if(jj==1)
  title('Figure 6.3: Real Network Point Error Ellipses (Static-Dynamic
Approach) ')
 %else
 %title('SIMULATED SECONDARY NETWORK')
%end
for i=1:cond/2
  ml=cipl(i);
  m2=cip2(i);
  xxl=[x(m1) x(m2)];
  yy1=[y(m1), y(m2)];
  plot(xx1, yy1, 'r-')
end
for i=1:angobs
  ml=kpl(i);
  m2=kp2(i);
  xx2=[x(m1) x(m2)];
  yy2=[y(m1), y(m2)];
  plot(xx2, yy2, 'g--')
end
for k=1:points
  n=120;
  theta=(-n:2:n)/n*pi;
  %THE POINT ELLIPSES
     xxx=a(k)*cos(theta)*10e5*0.4;
                                                   10.0
     yyy=b(k)*sin(theta)*10e5*0.4;
  %THE ROTATION MATRIX
  g(k) = degt(k) + mint(k) / 60 + sect(k) / 3600;
  phi=(g(k)/180)*pi;
  R(1,1)=sin(phi);
  R(1,2) = \cos(phi);
  R(2,1) = \cos(phi);
  R(2,2) = -\sin(phi);
 SROTATE THE ELLIPSE ACCORDING TO THE ANGLE OF INCLINATION
  for i=1:n+1
     for j=1:n+1
```

```
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```

```
xy=[xxx(1,j) yyy(1,j)];
          RXY=R*xy';
          xR(i,j) = RXY(1);
          yR(i, j) = RXY(2);
      end
   end
   xxx=xR;
   yyy=yR;
   %TRANSLATE THE FIGURE
   xxp=x(k);
   yyp=y(k);
   ox=xxp*ones(n+1);
   oy=yyp*ones(n+1);
   xxx=(xxx+ox); %scaling
   yyy=(yyy+oy); %scaling
   plot(xxx,yyy,'b.');
end
% NETWORK NUMBERING
for i=1:points
  point(i)=i;
end
text(x, v, 'point')
8 DRAWING SCALE BAR
text(520000,9640000,'Network:')
sx1=[540000 550000];
syl=[9640000 9640000];
plot(sx1,sy1,'b-');
gtext('10Km')
text(520000,9630000,'Ellipse:')
sx2=[540000 546400];
sy2=[9630000 9630000];
plot(sx2, sy2, 'b-');
gtext('20mm')
SDRAWING DIRECTION BAR
bx=[620000 620000];
by=[9580000 9590000];
plot(bx,by,'b-')
gtext('N')
text(525000,9650000,'SCALE:')
fclose(fid)
end
```

16.00

APPENDIX A.5: SUBFUNCTION QUAD.M

THIS SUBFUNCTION PERFORMS A DATUM JOIN BETWEEN TWO POINTS AND RETURNS THE BEARING IN RADIANS

```
function[bear]=quad(dn,de)
thita=atan(abs(de/dn))
if(dn>0)
   if(de>0)
      bear=thita;
   else
      bear=2*pi-thita;
   end
else
   if(de>0)
   bear=pi-thita;
   else
     bear=pi+thita;
   end
end
if(dn==0)
   if(de>0)
     bear=pi/2;
   else
    bear=3.0*pi/2.0;
   end
end
if(de==0)
   if(dn>0)
     bear=0.0;
   else
     bear=pi;
  end
end
```

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14.1

APPENDIX B: RESULTS OF THE STUDY

APPENDIX B.1: RESULTS OF THE FREE NETWORK ADJUSTMENT

APPENDIX B.1.1: Results of the real network freenet adjustment

FIRST ORDER REAL NETWORK ADJUSTMENT

ITERATION = 3 VUW= 1.0374396

RESULTS

| DISTANCE | : | TRACE1= | 26.000 | ETWE1= | 0.124 |
|------------|---|---------|--------|--------|-------|
| DIRECTIONS | : | TRACE2= | 52.000 | ETWE2= | 0.032 |

ADJUSTED OBSERVATIONS

3 7

ADJUSTED DISTANCES

| RAY | OBSERVED-DIST | ADJUSTI | ED-DIST | STD-ERR | RESIDUALE |
|-------|--------------------|-----------|---------|---------|-----------|
| | (m) | (m |) | (m) | (m) |
| 1 2 | 61821.778 | 6182 | 1.834 | 0.028 | -0.056 |
| 1 3 | 59131.496 | 5913: | 1.502 | 0.023 | -0.006 |
| 1 7 | 88020.944 | 88020 | 0.916 | 0.019 | 0.023 |
| 2 3 | 25314.493 | 25314 | 4.468 | 0.015 | 0.025 |
| 2 5 | 38470.110 | 3847(| D.147 | 0.014 | -0.03 |
| 2 4 | 30540.413 | 30540 | 0.441 | 0.015 | -0.028 |
| 3 7 | 40655.120 | 40655 | 5.057 | 0.015 | 0.063 |
| 3 5 | 22606.877 | 2260 | 5.890 - | 0.012 | -0.013 |
| 3 4 | 25378.281 | 25378 | 3.267 | 0.013 | 0.014 |
| 4 5 | 13713.543 | 1371: | 3.537 | 0.009 | 0.006 |
| 4 6 | 28156.771 | 28150 | 6.836 | 0.013 | -0.065 |
| 5 7 | 30046.422 | 30040 | 5.414 | 0.014 | 0.008 |
| 5 8 | 38108.480 | 38108 | 3.545 | 0.012 | -0.065 |
| 5 6 | 21332.688 | 21332 | 2.657 | 0.011 | 0.031 |
| 6 7 | 30371.764 | 3037: | L.771 | 0.015 | -0.007 |
| 6 8 | 19719.190 | 19719 | 9.197 | 0.011 | -0-007 |
| 7 8 | 29303.530 | 29303 | 3.543 | 0.013 | -8.013 |
| 7 11 | 43643.720 | 43643 | 3.734 | 0.013 | -0.014 |
| 7 10 | 27892.630 | 27892 | 2.613 | 0.012 | 0.017 |
| 7 9 | 21718.190 | 21718 | 3.179 | 0.012 | 0.011 |
| 8 9 | 29095.230 | 29095 | 5.289 | 0.012 | -0.059 |
| 8 10 | 19664.661 | 19664 | 1.639 | 0.011 | 0.022 |
| 8 11 | 19588.160 | 19588 | 3.179 | 0.011 | -0.019 |
| 9 10 | 13242.450 | 13242 | 2.429 | 0.008 | 0.021 |
| 9 11 | 32607.292 | 3260 | 7.348 | 0.012 | -0.056 |
| 10 11 | 19378.227 | 19378 | 3.194 | 0.011 | 0.033 |
| | | | | | |
| AI | DJUSTED DIRECTIONS | | | | |
| RAY | OBSERVED-DIRECT | ADJUSTED- | -DIRECT | STD-ERR | RESIDUALS |
| | (") | (| ") | (") | (") |
| 1 2 | 96 25 56.33 | 96 25 | 56.46 | 0.104 | -0.13 |
| 1 3 | 72 24 12.70 | 72 24 | 12.99 | 0.110 | -0.29 |
| 1 7 | 49 32 4.60 | 49 32 | 4.68 | 0.055 | -0.08 |
| 2 1 | 276 25 56.50 | 276 25 | 56.46 | 0.104 | 0.04 |
| 2 3 | 348 27 5.00 | 348 27 | 5.23 | 0.146 | -0.23 |
| 2 5 | 22 42 51.50 | 22 42 | 51.76 | 0.100 | -0.26 |
| 2 4 | 41 30 1.98 | 41 30 | 1.90 | 0.124 | 0.08 |
| 3 1 | 252 24 12.97 | 252 24 | 12.99 | 0.110 | -0.02 |

15 6 55.60 15 6 55.54 0.086 0.06

| 3 | 5 | 61 | 47 | 43.31 | 61 | 47 | 43.27 | 0.133 | 0.04 |
|----|----|-----|-----|-------|-----|-----|-------|-------|-------|
| 3 | 4 | 94 | 21 | 30.95 | 94 | 21 | 30.94 | 0.120 | 0.01 |
| 3 | 2 | 168 | 27 | 5.03 | 168 | 27 | 5.23 | 0.146 | -0.20 |
| 4 | 2 | 221 | 30 | 1.88 | 221 | 30 | 1.90 | 0.124 | -0.02 |
| 4 | 3 | 274 | 21 | 31.00 | 274 | 21 | 30.94 | 0.120 | 0.06 |
| 4 | 5 | 336 | 53 | 30.00 | 336 | 53 | 30.50 | 0.175 | -0.50 |
| 4 | 6 | 23 | 58 | 55.48 | 23 | 58 | 55.54 | 0.118 | -0.06 |
| 5 | 4 | 156 | 53 | 30.13 | 156 | 53 | 30.50 | 0.175 | -0.37 |
| 5 | 2 | 202 | 42 | 51.70 | 202 | 42 | 51.76 | 0.100 | -0.06 |
| 5 | 3 | 241 | 47 | 43.42 | 241 | 4 / | 43.27 | 0.133 | 0.15 |
| 5 | / | 341 | 55 | 37.04 | 341 | 55 | 36.86 | 0.101 | 0.18 |
| 5 | 8 | 31 | 7 | 39.11 | 31 | / | 39.01 | 0.087 | 0.10 |
| 5 | 6 | 52 | 4 | 14.61 | 52 | 4 | 14.56 | 0.141 | 0.05 |
| 6 | 4 | 203 | 58 | 55.65 | 203 | 28 | 55.54 | 0.118 | 0.11 |
| 6 | 5 | 232 | 4 | 14.75 | 232 | 4 | 14.56 | 0.141 | 0.19 |
| 6 | 6 | 300 | 34 | 45.60 | 300 | 34 | 45.60 | 0.096 | 0.00 |
| 6 | 8 | 8 | 22 | 44.00 | 8 | 22 | 44.19 | 0.159 | -0.19 |
| / | 1 | 229 | 32 | 4.63 | 229 | 32 | 4.68 | 0.055 | -0.05 |
| / | 3 | 195 | 6 | 55.72 | 195 | 6 | 55.54 | 0.086 | 0.18 |
| - | 5 | 161 | 55 | 37.08 | 101 | 55 | 36.86 | 0.101 | 0.22 |
| - | 6 | 120 | 34 | 45.72 | 120 | 34 | 45.60 | 0.096 | 0.12 |
| / | 8 | 82 | 2 | 26.49 | 82 | 2 | 26.33 | 0.090 | 0.16 |
| 1 | 11 | 60 | 32 | 9.83 | 60 | 32 | 9.82 | 0.079 | 0.01 |
| - | 10 | 41 | 22 | 3.70 | 41 | 20 | 3.11 | 0.104 | -0.07 |
| 0 | 9 | 14 | 22 | 30.21 | 14 | 22 | 20.30 | 0.131 | -0.15 |
| 0 | 5 | 211 | 22 | 30 01 | 211 | 22 | 44.19 | 0.159 | -0.13 |
| 0 | 5 | 262 | 2 | 26 45 | 262 | 2 | 26 33 | 0.087 | 0.03 |
| 0 | 9 | 202 | 12 | 13 74 | 305 | 12 | 13 62 | 0.090 | 0.12 |
| 8 | 10 | 328 | 42 | 52 87 | 328 | 72 | 52 64 | 0.129 | 0.12 |
| 8 | 11 | 27 | 16 | 15.76 | 27 | 16 | 45 66 | 0.145 | 0.25 |
| 9 | 7 | 194 | 22 | 56.41 | 194 | 22 | 56 36 | 0 131 | 0.10 |
| 9 | 8 | 125 | 42 | 13.81 | 125 | 42 | 13.62 | 0.096 | 0.09 |
| g | 10 | 91 | 1.3 | 20.49 | 91 | 13 | 20.72 | 0.187 | -0.23 |
| 9 | 11 | 89 | 14 | 41.48 | 89 | 14 | 41 37 | 0 100 | 0.11 |
| 10 | 9 | 271 | 13 | 20.55 | 271 | 13 | 20 72 | 0 187 | -0.17 |
| 10 | 7 | 221 | 55 | 3.80 | 221 | 55 | 3.77 | 0 104 | 0.03 |
| 10 | 8 | 148 | 6 | 52.90 | 148 | 6 | 52 64 | 0 129 | 26 |
| 10 | 11 | 87 | 53 | 37.12 | 87 | 53 | 36.75 | 0.152 | 0 37 |
| 11 | 9 | 269 | 14 | 41.53 | 269 | 14 | 41.37 | 0.100 | 0.16 |
| 11 | 10 | 267 | 53 | 37.01 | 267 | 53 | 36.75 | 0.152 | 0.26 |
| 11 | 7 | 240 | 32 | 9.98 | 240 | 32 | 9.82 | 0.079 | 0.16 |
| 11 | 8 | 207 | 16 | 45.78 | 207 | 16 | 45.66 | 0.145 | 0.12 |

APPENDIX B.1.2: Results of the simulated network freenet adjustment

FIRST ORDER SIMULATED NETWORK ADJUSTMENT

RESULTS

| DISTANCE | : | TRACE1= | 3.000 | ETWE1= | 2.763 | VC1= | 3.254 |
|------------|---|---------|-------|--------|-------|------|--------|
| DIRECTIONS | : | TRACE2= | 6.000 | ETWE2= | 5.515 | VC2= | 62.253 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| RA 1 1 2 | RAY OBSERVED-DIST (m) (m) 1 2 400.0060 1 3 399.9910 2 3 399.9930 | | | Al | DJUSTI (m) 400 399 399 | ED-DIST) .0071 .9994 .9888 | STD-ERR (m) 0.0063 0.0063 0.0063 | RESIDUALS (m) -0.0011 -0.0084 0.0042 | |
|-------------------|--|-------|-----------------|---------|------------------------------------|---|--|--|-----------|
| | A | JUSTE | DIR | ECTIONS | | | | | |
| RA | RAY OB: | | DBSERVED-DIRECT | | | USTED- | -DIRECT | STD-ERR | RESIDUALS |
| | | (| | ····) | (| | ••) | (") | (") |
| 1 | 2 | 30 | 0 | 0.00 | 29 | 59 | 56.71 | 2.2322 | 3.29 |
| 1 | 3 | 90 | 0 | 10.61 | 90 | 0 | 5.23 | 2.2322 | 5.38 |
| 2 | 3 | 150 | 0 | 0.00 | 149 | 59 | 57.40 | 2.2322 | 2.60 |
| 2 | 1 | 209 | 59 | 53.01 | 209 | 59 | 56.71 | 2.2322 | -3.70 |
| 3 | 1 | 270 | 0 | 0.00 | 270 | 0 | 5.23 | 2.2322 | -5.23 |
| 3 | 2 | 329 | 59 | 54.99 | 329 | 59 | 57.40 | 2.2322 | -2.41 |

APPENDIX B.2: RESULTS FOR STATIC-DYNAMIC DENSIFICATION

APPENDIX B.2.1: Results of the first level real network densification using static-

dynamic approach

SECOND ORDER REAL NETWORK ADJUSTMENT (STATIC-DYNAMIC APPROACH)

ITERATION = 2 VUW= 1.000000

RESULTS

| DISTANCE | : | TRACE1= | 30.000 | ETWE1= | 115.349 |
|------------|---|---------|--------|--------|---------|
| DIRECTIONS | : | TRACE2= | 52.000 | ETWE2= | 91.836 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| R/ | ΑY | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|----|---------------|---------------|----------|-----------|
| 12 | 7 | 11392.335 | 11392.344 | 0.0161 | -0.0091 |
| 12 | 9 | 12369.293 | 12369.302 | 0.0200 . | -0.0092 |
| 13 | 9 | 13814.687 | 13814.686 | 0.0388 | 0.0012 |
| 14 | 6 | 24623.681 | 24623.689 | 0.0272 | -0.0084 |
| 14 | 8 | 16935.563 | 16935.563 | 0.0207 | 0.0002 |
| 15 | 6 | 10683.383 | 10683.384 | 0.0236 | -0.0008 |
| 16 | 5 | 14837.980 | 14837.957 | 0.0188 | 0.0233 |
| 16 | 6 | 13269.516 | 13269.537 | 0.0192 | -0.0211 |
| 16 | 8 | 24310.634 | 24310.559 | 0.0182 | 0.0747 |
| 17 | 7 | 16690.070 | 16690.068 | 0.0225 | 0.0021 |
| 18 | 20 | 14984.326 | 14984.294 | 0.0297 | 0.0316 |
| 18 | 7 | 23865.886 | 23865.817 | 0.0241 | 0.0693 |
| 18 | 5 | 31483.464 | 31483.565 | 0.0245 | -0.1005 |

| 19 | 26 | 24790.315 | 24790.379 | 0.0441 | -0.0641 |
|----|----|-----------|-----------|--------|---------|
| 19 | 20 | 14808.001 | 14808.026 | 0.0374 | -0.0247 |
| 20 | 21 | 4247.690 | 4247.690 | 0.0318 | 0.000 |
| 21 | 3 | 10340.648 | 10340.625 | 0.0217 | 0.0226 |
| 21 | 7 | 35000.587 | 35000.688 | 0.0202 | -0.1005 |
| 22 | 2 | 16116.890 | 16116.931 | 0.0227 | -0.0408 |
| 22 | 23 | 15238.942 | 15238.935 | 0.0468 | 0.0066 |
| 22 | 5 | 23394.975 | 23394.981 | 0.0265 | -0.0060 |
| 23 | 4 | 15396.022 | 15396.053 | 0.0249 | -0.0307 |
| 24 | 2 | 15823.986 | 15824.021 | 0.0216 | -0.0353 |
| 24 | 3 | 17476.302 | 17476.306 | 0.0215 | -0.0036 |
| 24 | 26 | 33794.283 | 33794.458 | 0.0260 | -0.1746 |
| 24 | 25 | 23681.294 | 23681.280 | 0.0280 | 0.0143 |
| 25 | 1 | 25419.370 | 25419.371 | 0.0244 | -0.0010 |
| 25 | 26 | 13552.337 | 13552.333 | 0.0399 | 0.0039 |
| 26 | 1 | 16336.566 | 16336.670 | 0.0255 | -0.1036 |
| 26 | 24 | 33794.482 | 33794.458 | 0.0260 | 0.0244 |

ADJUSTED DIRECTIONS

| R | ΑY | OBSE | RVED-I | DIRECT | ADJ | USTED | -DIRECT | STD-ERR | RESIDUALS(") |
|----|----|------|--------|--------|-----|-------|---------|---------|--------------|
| 12 | 7 | 169 | 22 | 42.30 | 169 | 22 | 41.61 | 0.4589 | 0.69 |
| 12 | 9 | 37 | 17 | 34.90 | 37 | 17 | 35.92 | 0.3753 | -1.02 |
| 13 | 7 | 233 | 35 | 16.50 | 233 | 35 | 16.17 | 0.5511 | 0.33 |
| 13 | 8 | 106 | 41 | 48.00 | 106 | 41 | 48.42 | 0.4111 | -0.42 |
| 13 | 9 | 330 | 0 | 20.65 | 330 | 0 | 20.86 | 0.7183 | -0.21 |
| 14 | 6 | 231 | 32 | 25.31 | 231 | 32 | 25.00 | 0.2560 | 0.31 |
| 14 | 8 | 284 | 20 | 12.64 | 284 | 20 | 12.01 | 0.4196 | 0.63 |
| 14 | 11 | 341 | 1 | 11.63 | 341 | 1 | 10.98 | 0.1985 | 0.65 |
| 15 | 4 | 207 | 42 | 24.54 | 207 | 42 | 25.21 | 0.4565 | -0.67 |
| 15 | 5 | 257 | 44 | 42.41 | 257 | 44 | 42.07 | 0.3293 | 0.34 |
| 15 | 6 | 17 | 50 | 53.63 | 17 | 50 | 53.84 | 0.7900 | -0.21 |
| 16 | 5 | 194 | 6 | 54.60 | 194 | 6 | 54.50 | 0.2606 | 0.10 |
| 16 | 6 | 95 | 31 | 21.62 | 95 | 31 | 22.96 | 0.2922 | -1.34 |
| 16 | 8 | 41 | 24 | 51.23 | 41 | 24 | 52.20 | 0.1545 | -0.97 |
| 16 | 7 | 317 | 36 | 22.62 | 317 | 36 | 23.04 | 0.1994 | -0.42 |
| 17 | 5 | 149 | 36 | 47.34 | 149 | 36 | 48.27 | 0.6795 | -0.93 |
| 17 | 3 | 209 | 32 | 9.51 | 209 | 32 | 9.39 | 0.3675 | 10.12 |
| 17 | 18 | 275 | 15 | 46.63 | 275 | 15 | 46.55 | 0.2969 | |
| 17 | 7 | 352 | 11 | 25.96 | 352 | 11 | 26.78 | 0.6330 | -0.82 |
| 18 | 20 | 186 | 37 | 34.51 | 186 | 37 | 33.96 | 0.4517 | 0.55 |
| 18 | 7 | 52 | 19 | 28.91 | 52 | 19 | 27.66 | 0.2065 | 1.25 |
| 18 | 17 | 95 | 15 | 46.03 | 95 | 15 | 46.55 | 0.2969 | -0.52 |
| 18 | 5 | 116 | 21 | 25.06 | 116 | 21 | 25.81 | 0.1561 | -0.75 |
| 19 | 26 | 222 | 47 | 24.01 | 222 | 47 | 24.46 | 0.3565 | -0.45 |
| 19 | 24 | 143 | 18 | 7.51 | 143 | 18 | 6.69 | 0.2762 | 0.82 |
| 19 | 3 | 105 | 26 | 4.12 | 105 | 26 | 5.35 | 0.3155 | -1.23 |
| 19 | 20 | 78 | 16 | 29.43 | 78 | 16 | 31.41 | 0.5937 | -1.98 |
| 20 | 21 | 108 | 30 | 23.41 | 108 | 30 | 25.22 | 1.3038 | -1.81 |
| 20 | 18 | 6 | 37 | 34.92 | 6 | 37 | 33.96 | 0.4517 | 0.96 |
| 20 | 19 | 258 | 16 | 29.64 | 258 | 16 | 31.41 | 0.5937 | -1.77 |
| 21 | 3 | 144 | 36 | 27.98 | 144 | 36 | 31.51 | 0.4612 | -3.53 |
| 21 | 20 | 288 | 30 | 23.42 | 288 | 30 | 25.22 | 1.3038 | -1.80 |
| 21 | 7 | 28 | 17 | 39.99 | 28 | 17 | 38.41 | 0.1347 | 1.58 |
| 22 | 2 | 186 | 46 | 39.33 | 186 | 46 | 37.71 | 0.4734 | 1.62 |
| 22 | 23 | 120 | 5 | 28.54 | 120 | 5 | 31.18 | 0.4847 | -2.64 |
| 22 | 5 | 33 | 37 | 5.13 | 33 | 37 | 5.24 | 0.2844 | -0.11 |
| 22 | 3 | 321 | 36 | 42.00 | 321 | .36 | 40.90 | 0.5812 | 1.10 |
| 23 | 2 | 240 | 59 | 50.20 | 240 | 59 | 50.35 | 0.3364 | -0.15 |
| 23 | 4 | 19 | 32 | 28.15 | 19 | 32 | 28.61 | 0.4986 | -0.46 |
| 23 | 22 | 300 | 5 | 28.42 | 300 | 5 | 31.18 | 0.4847 | -2.76 |

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| 24 | 2 | 125 | 26 | 21.12 | 125 | 26 | 25.00 | 0.2865 | -3.88 |
|----|----|-----|----|-------|-----|----|-------|--------|-------|
| 24 | 3 | 26 | 35 | 49.90 | 26 | 35 | 48.99 | 0.2397 | 6.91 |
| 24 | 19 | 323 | 18 | 7.51 | 323 | 18 | 6.69 | 0.2762 | 0.82 |
| 24 | 26 | 277 | 8 | 39.00 | 277 | 8 | 39.31 | 0.2355 | -0.31 |
| 24 | 25 | 258 | 47 | 39.42 | 258 | 47 | 39.48 | 0.3812 | -0.06 |
| 25 | 1 | 275 | 18 | 29.72 | 275 | 18 | 26.41 | 0.3486 | 3.31 |
| 25 | 26 | 310 | 31 | 10.60 | 310 | 31 | 11.80 | 0.6619 | -1.20 |
| 25 | 24 | 78 | 47 | 38.42 | 78 | 47 | 39.48 | 0.3812 | -1.06 |
| 26 | 1 | 246 | 43 | 54.13 | 246 | 43 | 54.52 | 0.4478 | -0.39 |
| 26 | 25 | 130 | 31 | 11.12 | 130 | 31 | 11.80 | 0.6619 | -0.68 |
| 26 | 24 | 97 | 8 | 39.56 | 97 | 8 | 39.31 | 0.2355 | 0.25 |
| 26 | 19 | 42 | 47 | 24.43 | 42 | 47 | 24.46 | 0.3565 | -0.03 |

APPENDIX B.2.2: Results of the first level simulated network densification using static-

dynamic approach

SECOND ORDER SIMULATED NETWORK ADJUSTMENT (STATIC-DYNAMIC APPROACH)

ITERATION = 2 VUW= 0.855268

RESULTS

| DISTANCE : | TRACE1= | 9.000 | ETWE1= | 8.701 | VC1= | 1.300 |
|--------------|----------|--------|--------|--------|------|-------|
| DIRECTIONS : | TRACE2= | 18.000 | ETWE2= | 20.207 | VC2= | 1.345 |
| RESTRICTIONS | :TRACE3= | 0.000 | ETWE3= | 8.278 | VC3= | 2.514 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| RA | Y | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|---|---------------|---------------|---------|-----------|
| 1 | 4 | 200.0600 | 200.3131 | 0.0052 | 0 42531 |
| 1 | 6 | 200.0400 | 199.9784 | 0.0058 | -0.0616 |
| 2 | 4 | 200.0800 | 199.9594 | 0.0054 | -0.1206 |
| 2 | 5 | 199.9800 | 199.6085 | 0.0054 | -0.3715 |
| 3 | 5 | 200.0300 | 200.4226 | 0.0052 | 0.3926 |
| 3 | 6 | 199.9300 | 199.9622 | 0.0058 | 0.0322 |
| 4 | 5 | 200.0200 | 200.0034 | 0.0052 | -0.0166 |
| 4 | 6 | 200.0900 | 200.5731 | 0.0056 | 0.4831 |
| 5 | 6 | 199,9200 | 200.1768 | 0.0056 | 0.2568 |

ADJUSTED DIRECTIONS

| RA | Y | OBSE | RVED-I | DIRECT | ADJU | USTED- | DIRECT | STD-ERR | RESIDUALS(") |
|----|---|------|--------|--------|------|--------|--------|---------|--------------|
| 1 | 4 | 30 | 0 | 0.00 | 29 | 59 | 57.11 | 5.2363 | -2.89 |
| 1 | 6 | 90 | 0 | 10.61 | 90 | 0 | 23.13 | 4.4107 | 12.52 |
| 2 | 4 | 209 | 59 | 53.01 | 209 | 59 | 42.26 | 4.9482 | -10.75 |
| 2 | 5 | 150 | 0 | 4.99 | 150 | 0 | 10.01 | 4.9470 | 5.02 |
| 3 | 5 | 329 | 59 | 54.99 | 329 | 59 | 44.79 | 5.2384 | -10.20 |
| 3 | 6 | 270 | 0 | 3.01 | 270 | 0 | 14.56 | 4.4130 | 11.55 |
| 4 | 1 | 210 | 0 | 0.00 | 209 | 59 | 57.11 | 5.2363 | -2.89 |
| 4 | 2 | 30 | 0 | 7.00 | 30 | 0 | 10.24 | 4.9482 | 3.24 |
| 4 | 5 | 89 | 59 | 52.62 | 89 | 59 | 46.73 | 6.4613 | -5.89 |
| 4 | 6 | 150 | 0 | 5.42 | 150 | 0 | 9.34 | 6.0438 | 3.92 |

| 5 | 2 | 329 | 59 | 50.90 | 329 | 59 | 41.83 | 4.9470 | -9.07 |
|---|---|-----|----|-------|-----|----|-------|--------|-------|
| 5 | 4 | 270 | 0 | 4.37 | 270 | 0 | 10.23 | 6.4613 | 5.86 |
| 5 | 6 | 209 | 59 | 58.02 | 209 | 59 | 53.76 | 6.0427 | -4.26 |
| 5 | 3 | 150 | 0 | 13.96 | 150 | 0 | 22.73 | 5.2384 | 8.77 |
| 6 | 1 | 270 | 0 | 0.00 | 270 | 0 | 1.91 | 4.4107 | 1.91 |
| 6 | 4 | 329 | 59 | 57.71 | 329 | 59 | 53.92 | 6.0438 | -3.79 |
| 6 | 5 | 30 | 0 | 6.43 | 30 | 0 | 10.58 | 6.0427 | 4.15 |
| 6 | 3 | 89 | 59 | 54.98 | 89 | 59 | 58.50 | 4.4130 | 3.52 |

APPENDIX B.2.3: Results of the second level real network densification using static-

dynamic approach

THIRD ORDER REAL NETWORK ADJUSTMENT (STATIC-DYNAMIC APPROACH)

ITERATION = 2 VUW= 1.089

RESULTS

| DISTANCE | : | TRACE1= | 30.000 ETWE1= | 6.926 |
|------------|---|---------|---------------|--------|
| DIRECTIONS | : | TRACE2= | 50.000 ETWE2= | 24.452 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| AY | | OBSERVED-DIST | | ADJUSTED-DIST | Γ | STD-ERR | | RESIDUALS |
|----|--|--|--|--|---|--|--|--|
| 26 | | 14773.890 | | 14773.894 | | 0.0332 | | -0.0040 |
| 28 | | 9653.420 | | 9653.417 | | 0.0337 | | 0.0033 |
| 29 | | 13934.030 | | 13934.026 | | 0.0216 | | 0.0037 |
| 24 | | 17550.110 | | 17550.095 | | 0.0241 | | 0.0146 |
| 3 | | 14026.280 | | 14026.287 | | 0.0179 | | -0,0070 |
| 24 | | 7500.980 | | 7500.963 | | 0.0246 | | 0.0170 |
| 22 | | 20768.540 | | 20768.536 | | 0.0411 | | 0.0036 |
| 23 | | 7148.220 | | 7148.220 | | 0.0429 | | -0.0003 |
| 4 | | 10861.010 | | 10861.009 | | 0.0205 | | 0.0012 |
| 5 | | 18725.550 | | 18725.559 | | 0.0184 | | -0.0090 |
| 3 | | 12954.160 | | 12954.155 | | 0.0218 | | 0.0050 |
| 21 | | 14309.080 | | 14309.071 | | 0.0291 | | 0.0087 |
| 5 | | 6615.690 | | 6615.690 | | 0.0150 | | 0.0004 |
| 4 | | 9616.290 | | 9616.289 | | 0.0142 | | 0.0011 |
| 18 | | 6763.580 | | 6763.583 | | 0.0268 | | -0.0034 |
| 21 | | 10493.270 | | 10493.267 | | 0.0214 | | 0.0025 |
| 20 | | 10463.230 | | 10463.226 | | 0.0249 | | 0.0045 |
| 16 | | 7137.810 | | 7137.804 | | 0.0217 | | 0.0060 |
| 17 | | 7795.220 | | 7795.233 | | 0.0484 | | -0.0133 |
| 7 | | 13557.220 | | 13557.216 | | 0.0204 | | 0.0044 |
| 18 | | 11414.360 | | 11414.357 | | 0.0317 | | 0.0030 |
| 35 | | 10445.030 | | 10445.025 | | 0.0176 | | 0.0047 |
| 17 | | 7476.300 | | 7476.310 | | 0.0349 | | -0.0104 |
| 7 | | 11935.450 | | 11935.458 | | 0.0156 | | -0.0077 |
| 8 | | 15218.090 | | 15218.089 | | 0.0141 | | 0.0012 |
| 16 | | 13176.150 | | 13176.153 | | 0.0238 | | -0.0026 |
| 7 | | 14752.400 | | 14752.402 | | 0.0138 | | -0.0022 |
| 14 | | 17156.360 | | 17156.352 | | 0.0321 | | 0.0079 |
| | AY 26 28 29 24 3 24 22 23 4 5 3 21 5 4 8 20 16 7 18 35 17 7 8 6 7 14 | AY 26 28 29 24 3 24 22 23 4 5 3 21 5 4 18 21 20 16 17 7 18 35 17 7 8 16 7 14 | AYOBSERVED-DIST2614773.890289653.4202913934.0302417550.110314026.280247500.9802220768.540237148.220410861.010518725.550312954.1602114309.08056615.69049616.290186763.5802110493.2702010463.230167137.810177795.220713557.220713557.2201811414.3603510445.030177476.300711935.450815218.0901613176.150714752.4001417156.360 | AY OBSERVED-DIST 26 14773.890 28 9653.420 29 13934.030 24 17550.110 3 14026.280 24 7500.980 22 20768.540 23 7148.220 4 10861.010 5 18725.550 3 12954.160 21 14309.080 5 6615.690 4 9616.290 18 6763.580 21 10493.270 20 10463.230 16 7137.810 17 7795.220 7 13557.220 7 13557.220 7 13557.220 7 13557.220 7 13557.220 7 14752.400 14 17156.360 | AYOBSERVED-DISTADJUSTED-DIST2614773.89014773.894289653.4209653.4172913934.03013934.0262417550.11017550.095314026.28014026.287247500.9807500.9632220768.54020768.536237148.2207148.220410861.01010861.009518725.55018725.559312954.16012954.1552114309.08014309.07156615.6906615.69049616.2909616.289186763.5806763.5832110493.27010493.2672010463.23010463.226167137.8107137.804177795.2207795.233713557.2161811414.36011414.3573510445.03010445.025177476.300711935.4501935.45815218.0891613176.15013176.153714752.40014752.4021417156.360 | AYOBSERVED-DISTADJUSTED-DIST2614773.89014773.894289653.4209653.4172913934.03013934.0262417550.11017550.095314026.28014026.287247500.9807500.9632220768.54020768.536237148.2207148.220410861.01010861.009518725.55018725.559312954.16012954.1552114309.08014309.07156615.6906615.69049616.2909616.289186763.5806763.5832110493.27010493.2672010463.23010463.226167137.8107137.804177795.2207795.233713557.22013557.2161811414.36011414.3573510445.03010445.025177476.3007476.310711935.45011935.458815218.09015218.0891613176.15013176.153714752.40014752.4021417156.36017156.352 | AYOBSERVED-DISTADJUSTED-CISTSTD-ERR2614773.89014773.8940.0332289653.4209653.4170.03372913934.03013934.0260.02162417550.11017550.0950.0241314026.28014026.2870.0179247500.9807500.9630.02462220768.54020768.5360.0411237148.2207148.2200.0429410861.01010861.0030.0205518725.55018725.5590.0184312954.16012954.1550.02182114309.08014309.0710.029156615.6906615.6900.015049616.2909616.2890.0142186763.5806763.5830.02682110493.27010493.2670.02142010463.23010463.2260.0249167137.8107137.8040.0217177795.2207795.2330.0484713557.2160.02041811414.36011414.3570.03173510445.03010445.0250.0176177476.3007476.3100.0349711935.45011935.4580.0156815218.09015218.0890.01411613176.15013176.1530.0238714752.40014752.4020.01381417156.36017156.3520.0321 | AYOBSERVED-DISTADJUSTED-DISTSTD-ERR2614773.89014773.8940.0332289653.4209653.4170.03372913934.03013934.0260.02162417550.11017550.0950.0241314026.28014026.2870.0179247500.9807500.9630.02462220768.54020768.5360.0411237148.2207148.2200.0429410861.01010861.0030.0205518725.55018725.5530.0184312954.16012954.1550.02182114309.08014309.0710.029156615.6906615.6900.015049616.2909616.2890.0142186763.5806763.5830.02682110493.27010493.2670.02142010463.23010463.2260.0249167137.8107137.8040.0217177795.2207795.2330.0484713557.22013557.2160.02041811414.36011414.3570.03171510445.03010445.0250.0176177476.3007476.3100.0349711935.45011935.4580.0156815218.0890.01411613176.15013176.1530.0238714752.40014752.4020.01381417156.36017156.3520.0321 |

| 40 | 11 | 12385.920 | 12385.928 | 0.0165 | -0.0080 |
|----|----|-----------|-----------|--------|---------|
| 41 | 13 | 17334.620 | 17334.635 | 0.0593 | -0.9146 |

ADJUSTED DIRECTIONS

| R/ | λY | OBSER | VED-D | TRECT | ADJU | STED- | DIRECT | STD-ERR | RESIDUALS(") |
|----|-----|-----------|-------|-------|------|-------|----------------|---------|--------------|
| 27 | 26 | 232 | 51 | 31.26 | 232 | 51 | 32.02 | 0.5201 | -0.76 |
| 27 | 19 | 28 | 38 | 17 97 | 28 | 38 | 17.33 | 0.7361 | 0.64 |
| 27 | 28 | 149 | 41 | 47.26 | 149 | 41 | 48.14 | 0.5988 | -0.88 |
| 28 | 27 | 329 | 41 | 49.25 | 329 | 41 | 48.14 | 0.5988 | 1.11 |
| 28 | 29 | 81 | 34 | 28 89 | 81 | 34 | 29.95 | 0.4442 | -1.06 |
| 28 | 24 | 105 | 50 | 4 45 | 105 | 50 | 3 54 | 0 3739 | 0.91 |
| 28 | 25 | 214 | 2 | 52 29 | 214 | 2 | 53 00 | 0 6201 | -0.71 |
| 20 | 20 | C14 C1 | 4 | 31 92 | 51 | 0 | 34 07 | 0.2662 | 0.75 |
| 20 | 24 | 166 | 25 | 5 04 | 155 | 25 | 1 99 | 0 6144 | 1 05 |
| 29 | 2.4 | 100 | 27 | 20 00 | 261 | 21 | 20 05 | 0.0444 | -0.96 |
| 27 | 20 | 201 | 24 | 20.33 | 201 | 24 | 29.9J Al A3 | 0.3556 | 0.00 |
| 20 | 24 | 200 | 21 | 41.43 | 200 | 16 | 41.45 | 0.3065 | 0.03 |
| 30 | 4 | 352 | 10 | 43.10 | 352 | 10 | 43.07 | 1 0626 | -0.03 |
| 30 | 23 | 252 | 53 | 6.97 | 202 | 23 | 7.00 | 1.0620 | -0.03 |
| 31 | 4 | 28 | 10 | 33.02 | 28 | 10 | 33.13 | 0.3000 | -0.11 |
| 31 | 22 | 262 | 44 | 43.89 | 202 | 44 | 44.70 | 0.5865 | -0.07 |
| 31 | 5 | 11 | 53 | 0.49 | 11 | 53 | 0.51 | 0.2200 | -0.02 |
| 32 | 5 | 86 | 39 | 13.99 | 86 | 39 | 13.96 | 0.3/93 | 0.03 |
| 32 | 3 | 219 | 27 | 48.46 | 219 | 27 | 47.60 | 0.3405 | 0.86 |
| 32 | 21 | 263 | 41 | 41.82 | 263 | 41 | 42.85 | 0.3860 | -1.03 |
| 32 | 17 | 20 | 2 | 9.29 | 20 | 2 | 9.14 | 0.7920 | 0.15 |
| 33 | 5 | 297 | 4 | 1.97 | 297 | 4 | 2.06 | 0.4386 | -0.09 |
| 33 | 15 | 52 | 8 | 46.69 | 52 | 8 | 46.58 | 0.6813 | 0.11 |
| 33 | 4 | 183 | 1 | 59.52 | 183 | 1 | 59.60 | 0.3422 | -0.08 |
| 34 | 18 | 329 | 7 | 12.99 | 329 | 7 | 13.85 | 0.8871 | -0.86 |
| 34 | 17 | 77 | 42 | 3.25 | 77 | 42 | 2.29 | 0.2954 | 0.96 |
| 34 | 21 | 186 | 24 | 52.69 | 186 | 24 | 53.75 | 0.5830 | -1.06 |
| 34 | 20 | 209 | 48 | 10.99 | 209 | 48 | 11.01 | 0.5632 | -0.02 |
| 35 | 16 | 32 | 10 | 16.87 | 32 | 10 | 16.16 | 0.6512 | 0.71 |
| 35 | 5 | 178 | 45 | 7.49 | 178 | 45 | 8.1.4 | 0.4.371 | -0.65 |
| 35 | 17 | 298 | 10 | 32.64 | 298 | 10 | 31.89 | 0.8689 | 0.75 |
| 36 | 12 | 32 | 44 | 39.26 | 32 | 44 | 40.50 | 0.3156 | PA.24 |
| 36 | 7 | 67 | 59 | 6.55 | 67 | 59 | 5.90 | 0.3667 | / * 0.65 |
| 36 | 18 | 213 | 37 | 30.21 | 213 | 37 | 30.80 | 0.5509 | -0.59 |
| 37 | 16 | 120 | 40 | 11.50 | 120 | 40 | 10.20 | 0.5793 | 1.30 |
| 37 | 35 | 163 | 45 | 30.30 | 163 | 45 | 31.22 | 0.4702 | -0.92 |
| 37 | 17 | 211 | 53 | 41.82 | 211 | 53 | 42.43 | 1.3186 | -0.61 |
| 37 | 7 | 328 | 36 | 9.94 | 328 | 36 | 9.23 | 0.3199 | 0.71 |
| 38 | 8 | 70 | 7 | 12.51 | 70 | 7 | 11.47 | 0.2319 | 1.04 |
| 38 | 16 | 187 | 43 | 14.82 | 187 | 43 | 14.79 | 0.3218 | 0.03 |
| 38 | 7 | 274 | 20 | 37.98 | 274 | 20 | 38.03 | 0.2523 | -0.05 |
| 38 | 13 | 346 | 41 | 53.56 | 346 | 41 | 53.62 | 1.0271 | -0.06 |
| 39 | 8 | 359 | 53 | 6.52 | 359 | 53 | 6.06 | 0.4590 | 0.46 |
| 39 | 14 | 72 | 48 | 16.88 | 72 | 48 | 16.90 | 0.7708 | -0.02 |
| 39 | 6 | 195 | 45 | 58.94 | 195 | 45 | 58.75 | 0.5008 | 0.19 |
| 40 | 11 | 0 | 27 | 45.30 | 0 | 27 | 45.74 | 0.6242 | -0.44 |
| 40 | 14 | 140 | 45 | 14.38 | 140 | 45 | 13.98 | 0.6856 | 0.50 |
| 40 | 8 | 240 | 29 | 37.98 | 240 | 29 | 39.23 | 0.4588 | -1.25 |
| 41 | 10 | 293 | 52 | 37.34 | 293 | 52 | 36.78 | 0.6513 | 0.56 |
| 41 | 11 | 64 | 34 | 8.77 | 64 | 34 | 8.51 | 0.5963 | 0.26 |
| 41 | 13 | 244 | 2 | 51.24 | 244 | 2 | 51.41 | 0.5748 | -0.17 |
APPENDIX B.2.4: Results of the second level simulated network densification using

static-dynamic approach

THIRD ORDER SIMULATED NETWORK ADJUSTMENT (STATIC-DYNAMIC APPROACH)

ITERATION = 2 VUW= 0.911081

RESULTS

| DISTANCE : | TRACE1= | 30.000 | ETWE1= | 4.266 | VC1= | 0.142 |
|--------------|----------|--------|---------|--------|------|-------|
| DIRECTIONS : | TRACE2= | 60.000 | ETWE2 = | 64.997 | VC2= | 1.600 |
| RESTRICTIONS | :TRACE3= | 0.000 | ETWE3= | 28.908 | VC3= | 2.209 |

ADJUSTED OBSERVATIONS

| RAY | OBSERVED-DIST | AI | JUSTE | D-DIST | STD-ERR | RESIDUALS |
|-------|--------------------|-----|--------|--------|---------|--------------|
| 1 7 | 100.0400 | | 99. | 9138 | 0.0043 | 0.1262 |
| 1 8 | 100.0600 | | 99. | 9897 | 0.0038 | 0.0703 |
| 2 10 | 100.3800 | | 99. | 9462 | 0.0042 | 0.1338 |
| 2 11 | 99.9800 | | 99. | 8794 | 0.0042 | 0.1006 |
| 3 13 | 100.0300 | | 100. | 0445 | 0.0038 | -0.0145 |
| 3 14 | 99.9300 | | 100. | 0363 | 0.0043 | -0.1063 |
| 4 8 | 100.0200 | | 99. | 8177 | 0.0052 | 0.2023 |
| 4 9 | 100.0400 | | 99. | 5793 | 0.0051 | 2.4607 |
| 4 10 | 100.0300 | | 100. | 2548 | 0.0053 | -0.2248 |
| 4 12 | 99.9700 | | 99. | 7985 | 0.0045 | 0.1715 |
| 5 11 | 99.8900 | | 100. | 4721 | 0.0053 | -0.5821 |
| 5 12 | 100. 800 | | 100. | 2398 | 0.0045 | -0.1598 |
| 5 13 | 99.3900 | | 99. | 5928 | 0.0052 | C.3972 |
| 5 15 | 99.9400 | | 99. | 8010 | 0.0051 | 0.1390 |
| 6 7 | 99.9800 | | 100. | 1879 | 0.0057 | -3.20-9 |
| 6 9 | 99.9300 | | 100. | 0277 | 0.0045 | -0/09-7 |
| 6 14 | 100.0300 | | 99. | 8613 | 0.0057 | 0.1685 |
| 6 15 | 100.2200 | | 99. | 8628 | 0.0045 | 0.1572 |
| 7 9 | 99.9700 | | 100. | 0376 | 0.0030 | -0.0676 |
| 8 7 | 100.000 | | 100. | 0197 | 0.0032 | -0.0197 |
| 8 9 | 100.0600 | | 100. | 0157 | 0.0032 | 0.0443 |
| 9 1 2 | 100.0400 | | 100. | 0502 | 0.0030 | -0.0102 |
| 9 1 5 | 100.0100 | | 100. | 0135 | 0.0030 | -0.0035 |
| 10 11 | 100.000 | | 99. | 9904 | 0.0030 | 0.0096 |
| 12 10 | 100.0600 | | 99. | 9876 | 0.0034 | 0.0724 |
| 12 11 | 99.9800 | | 99. | 9963 | 0.0034 | -0.0163 |
| 12 15 | 99.3700 | | 100. | 0390 | 0.0030 | -0.0690 |
| 13 14 | 99.3600 | | 100. | 0487 | 0.0032 | -0.0887 |
| 15 14 | 100.0500 | | 100. | 0583 | 0.0030 | -0.0083 |
| 15 13 | 100.0300 | | 100. | 0459 | 0.0032 | -0.0159 |
| A | DJUSTED DIRECTIONS | | | | | |
| RAY | OBSERVED-DIRECT | ADJ | JSTED- | DIRECT | STD-ERR | RESTDUATS (* |
| 1 8 | 29 59 54.90 | 30 | -0 | 16.38 | 3.3621 | -21.48 |
| 1 7 | 89 59 53.00 | 89 | 59 | 56.04 | 7.1340 | -3.04 |
| 2 10 | 209 59 57.01 | 209 | 59 | 39.34 | 7.4573 | 17.67 |
| 2 11 | 149 59 53.00 | 149 | 59 | 57.95 | 7.4581 | 0.05 |
| 3 13 | 330 0 0.00 | 329 | 59 | 58.17 | 3.3616 | 1.83 |

| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 3 | 14 | 269 | 59 | 52.01 | 269 | 59 | 50.63 | 7.1338 | 1.38 |
|---|----|----|-----|----------|-------|-----|----|-------|----------|--------|
| $ \begin{array}{ccccccccccccccccccccccccccccccccccc$ | 4 | 8 | 209 | 59 | 53.00 | 210 | 0 | 29.33 | 10.0363 | -36.33 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 4 | 9 | 150 | 0 | 4.00 | 149 | 59 | 47.99 | 9.7562 | 16.01 |
| 4 10 30 0 8.42 29 59 30.43 9.8465 -7.99 5 11 30 0 2.90 330 0 4.67 9.8367 -1.77 5 12 269 59 54.37 270 0 50.19 9.7449 -43.25 5 15 0 3.96 150 0 4.61 10.0478 -0.65 6 7 270 0 9.00 269 59 33.26 10.7264 21.45 6 14 90 0 1.98 90 28.09 8.3539 -26.11 8 1 210 0 0.097 8.3621 -2.394 7 150 0 0.10 90 2.269 6.4747 -2.34 7 8 30 10.00 330 0 7.157 7.1633 2.857 7 9 9 9 $5.7.00$ 89 59 28.77 5.3300 28.233 | 4 | 12 | 90 | 0 | 2.62 | 89 | 59 | 19.93 | 10.9300 | 42.69 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 4 | 10 | 30 | 0 | 8.42 | 29 | 59 | 30.43 | 9.8465 | 37.99 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 5 | 11 | 330 | 0 | 2.90 | 330 | 0 | 4.67 | 9.8367 | -1.77 |
| 5 15 210 0 50.19 9.7449 -45.17 5 13 150 0 3.96 150 0 4.61 10.0478 -0.65 6 7 270 0 9.00 269 59 33.26 10.7264 21.45 6 14 90 0 1.98 90 0 28.09 8.3539 -26.11 8 1 210 0 0.00 210 0 20.97 8.3521 -20.97 8 7 150 0 0.10 149 59 58.24 -1633 1.86 7 150 0 0.10 90 2.69 6.4747 -2.59 8 4 29 59 57.00 29 53.76 6.7515 -2.76 7 9 29 59 53.70 89 59 28.77 53.30 28.23 9 4 30 0 0.00 329 59 44.33 9.7562 15.61 9 < | 5 | 12 | 269 | 59 | 54.37 | 270 | 0 | 37.62 | 10.8959 | -43.25 |
| 5 13 150 0 4.61 10.0478 -0.65 6 7 270 0 9.00 269 59 39.57 8.3380 29.43 6 15 30 0 6.43 30 0 18.38 10.7415 -11.95 6 14 90 0 28.09 8.3539 -26.11 8 7 150 0 0.10 149 59 58.24 7.1633 1.269 8 9 9 0 0.10 90 2.69 6.4747 -2.59 8 30 0 10.00 330 0 7.15 7.1633 2.847 7 9 29 59 51.00 29 59 5.76 6.7515 -2.766 7 8 30 0 0.00 329 59 44.39 9.7562 15.61 9 4 30 0 0.00 249 59 56.65 6.0221 -1.655 9 8 270 | 5 | 15 | 210 | 0 | 5.02 | 210 | 0 | 50.19 | 9.7449 | -45.17 |
| 6 7 270 0 9.00 269 59 39.57 8.3380 29.43 6 9 329 59 54.71 329 59 33.26 10.7264 21.45 6 14 90 0 1.98 90 0 28.09 8.3539 -26.11 8 1 210 0 0.00 210 0 20.97 8.3621 -20.97 8 7 150 0 0.10 90 2.69 6.4747 -2.34 7 1 270 0 0.00 270 0 2.34 7.1340 -2.34 7 8 330 0 10.00 330 0 7.15 7.1633 2.85 7 9 9 55 57.00 85 59 28.77 5.3380 28.23 9 4 330 0 0.00 29 59 56.46 6.1143 -3.46 9 15 89 59 50.01 9 7.3300 41.63 </td <td>5</td> <td>13</td> <td>150</td> <td>0</td> <td>3.96</td> <td>150</td> <td>0</td> <td>4.61</td> <td>10.0478</td> <td>-0.65</td> | 5 | 13 | 150 | 0 | 3.96 | 150 | 0 | 4.61 | 10.0478 | -0.65 |
| 6 9 329 59 54.71 329 59 33.26 10.7264 21.45 6 15 30 0 6.43 30 0 18.38 10.7415 -11.95 6 14 90 0 20.09 8.3529 -26.11 8 1 210 0 0.00 210 0 20.97 8.3621 -20.97 8 7 150 0 0.10 90 0 2.69 6.4747 -2.59 8 4 29 59 57.90 30 0 33.74 10.0363 -2.34 7 9 29 59 51.00 29 59 53.76 6.7515 -2.76 7 9 29 59 53.00 29 59 56.46 6.1143 -3.46 9 4 30 0 0.03 29 59 56.46 6.1143 -3.46 9 6 150 0 10.99 21.00 0 2.07 6.143 -2.76 | 6 | 7 | 270 | 0 | 9.00 | 269 | 59 | 39.57 | 8.3380 | 29.43 |
| 6 15 30 0 18.38 10.7415 -11.95 6 14 90 0 1.98 90 0 28.09 8.3539 -26.11 8 7 150 0 0.10 149 59 58.24 7.1633 1.86 8 9 90 0 0.10 90 2.69 6.4747 -2.59 8 4 29 59 57.90 30 0 3.37 10.0363 -35.84 7 1 270 0 0.00 270 0 2.34 7.1340 -2.34 7 8 330 0 10.00 320 7.15 7.1633 2.85 9 9 59 51.00 29 59 53.76 6.7515 -2.76 7 8 330 0 0.00 329 59 54.66 6.1143 -3.46 9 12 9 59 59.00 210 0 7.10 6.4747 -2.10 12 <t< td=""><td>6</td><td>9</td><td>329</td><td>59</td><td>54.71</td><td>329</td><td>59</td><td>33.26</td><td>10.7264</td><td>21.45</td></t<> | 6 | 9 | 329 | 59 | 54.71 | 329 | 59 | 33.26 | 10.7264 | 21.45 |
| 6 14 90 0 1.98 90 0 28.09 8.3539 -26.11 8 1 210 0 0.00 210 0 20.97 8.3621 -20.97 8 7 150 0 0.10 90 0 2.69 6.4747 -2.59 8 4 29 59 57.90 30 0 33.74 10.0363 -35.84 7 9 29 59 51.00 29 59 53.76 6.7515 -2.76 7 9 29 59 51.00 29 59 56.46 6.1143 -3.46 9 4 330 0 0.00 329 59 44.39 9.7562 15.61 9 6 150 0 10.90 149 59 47.83 10.7264 23.07 9 7 209 59 50.00 270 7.10 5.4747 -2.10 12 9 10 0.00 210 0 2.76 6.1143 | 6 | 15 | 30 | 0 | 6.43 | 30 | 0 | 18.38 | 10.7415 | -11.95 |
| 8 1 210 0 20.97 8.3621 -20.97 8 7 150 0 0.10 190 56.24 7.1633 1.86 8 9 90 0 0.10 90 0 2.69 6.4747 -2.59 8 4 29 59 57.90 30 0 33.74 10.0363 2.34 7 1 270 0 0.00 270 0 2.34 7.1340 -2.34 7 9 29 59 51.00 29 55 -2.76 7 6 89 59 57.00 85 59 28.77 5.3380 28.23 9 4 330 0 0.00 29 55 56.65 5.0021 -1.65 9 150 0 0.99 59 54.66 5.1143 -2.10 12 29 210 0 0.00 210 0 2.76 5.1143 -2.76 12 130 0 0. | 6 | 14 | 90 | 0 | 1.98 | 90 | 0 | 28.09 | 8.3539 | -26.11 |
| 8 7 150 0 0.10 149 59 58.24 7.1633 1.86 8 9 90 0 0.10 90 0 2.69 6.4747 -2.59 8 4 29 59 57.90 30 0 33.74 10.0363 -35.84 7 270 0 2.34 7.1340 -2.34 7 8 330 0 10.00 330 0 7.15 7.1633 2.85 7 9 29 59 51.00 29 59 53.76 6.7515 -2.76 7 29 59 55.00 89 56.65 6.0221 -1.65 9 6 150 0 10.90 149 59 47.83 10.7264 23.07 9 7 209 59 50.00 270 7.10 6.1143 -2.16 12 4 269 59 50.00 29 59.90 6.3474 -2.10 12 1330 0 0.00 </td <td>8</td> <td>1</td> <td>210</td> <td>0</td> <td>0.00</td> <td>210</td> <td>0</td> <td>20.97</td> <td>8.3621</td> <td>-20.97</td> | 8 | 1 | 210 | 0 | 0.00 | 210 | 0 | 20.97 | 8.3621 | -20.97 |
| 8 9 90 0 0.10 90 0 2.69 6.4747 -2.59 8 4 29 59 57.90 30 0 33.74 10.0363 -35.84 7 9 29 59 51.00 29 59 53.76 6.7515 -2.76 7 9 29 59 53.00 29 59 3.380 28.23 9 4 330 0 0.00 329 59 44.39 9.7562 15.61 9 12 29 59 55.00 89 59 56.65 6.0021 -1.65 9 7 209 59 59.00 210 0 0.96 6.7515 -1.96 9 8 270 0 5.00 270 0 7.10 6.4747 -2.10 12 9 210 0 0.00 20 2.76 6.1143 -2.76 12 13 0 0.00 20 2.76 6.3476 1.08 | 8 | 7 | 150 | 0 | 0.10 | 149 | 59 | 58.24 | 7.1633 | 1.86 |
| 8 4 29 59 57.90 30 0 33.74 10.0363 -35.84 7 1 270 0 0.30 0 7.1340 -2.34 7 8 330 0 10.00 330 0 7.15 7.1633 2.85 7 9 29 59 51.00 29 59 53.76 6.7515 -2.76 7 6 89 59 57.00 89 59 28.77 5.3380 28.23 9 4 330 0 0.00 329 59 56.65 5.0021 -1.65 9 15 89 59 55.00 89 59 56.65 5.0021 -1.65 9 6 150 0 10.90 149 59 47.83 10.7264 23.07 9 72.09 59 50.00 210 0 2.76 6.1143 -2.76 12 10 30 0 0.00 29 59 59.99 4.63 <td>8</td> <td>9</td> <td>90</td> <td>0</td> <td>0.10</td> <td>90</td> <td>0</td> <td>2.69</td> <td>6.4747</td> <td>-2.59</td> | 8 | 9 | 90 | 0 | 0.10 | 90 | 0 | 2.69 | 6.4747 | -2.59 |
| 7127000.0027002.347.1340 -2.34 78330010.0033007.157.16332.8579295951.00295953.766.7515 -2.76 76895957.00895928.775.338028.239433000.003295944.399.756215.61912295953.00295956.466.1143 -3.46 915895955.00895956.656.0021 -1.65 96150010.901495947.8310.726423.07972095959.002100 0.96 6.7515 -1.96 9827005.002700 7.10 6.4747 -2.10 1292100 0.00 2205958.92 6.3484 0.91 12103300 0.00 295959.09 6.3484 0.91 12130 0.000 295959.104 6.1150 3.96 12130 0.000 2959 57.57 7.949 -0.05 12145950.001495951.04 6.3476 0.08 1012295950.0030 | 8 | 4 | 29 | 59 | 57.90 | 30 | 0 | 33.74 | 10.0363 | -35.84 |
| 78330010.0033007.157.16332.8579295951.00295953.76 6.7515 -2.76 76895957.00895928.77 3.3380 28.239433000.003295944.39 9.7562 15.61912295953.00295956.46 6.1143 -3.46 912295955.00895956.65 6.0021 -1.65 96150010.901495947.83 10.7264 23.07 972095959.002100 0.96 6.7515 -1.96 9827005.0027007.10 6.4747 -2.10 12921000.0021002.76 6.1143 -2.76 1242695952.00269910.3712.9300 41.63 121033000.002959.5959.09 6.3484 0.911259000.00295959.09 6.3484 0.91121495955.001495951.04 6.1150 3.96 102295957.00205951.57 -949 12133001.003300 0.65 | 7 | 1 | 270 | 0 | 0.00 | 270 | 0 | 2.34 | 7.1340 | -2.34 |
| 79295951.00295953.76 6.7515 -2.76 76895957.00895928.775.338028.239433000.003295956.466.1143 -3.46 915895955.00895956.655.0021 -1.65 96150010.901495947.83 1.7264 23.07972095959.0021000.96 6.7515 -1.96 12921000.0021002.76 6.1143 -2.76 12921000.002695910.3712.930041.6312113000.00295958.92 6.3476 1.0812113000.00295959.09 6.3484 0.911259000.00295957.33 7.4573 17.47 142095957.002095937.53 7.4573 17.47 1042095955.001495955.15 -9949 -0.05 1122095955.10295955.15 -9949 -1.15 11122095954.002695955.15 -9949 -1.15 111220959 </td <td>7</td> <td>8</td> <td>330</td> <td>0</td> <td>10.00</td> <td>330</td> <td>0</td> <td>7.15</td> <td>7.1633</td> <td>2.85</td> | 7 | 8 | 330 | 0 | 10.00 | 330 | 0 | 7.15 | 7.1633 | 2.85 |
| 76895957.00895928.77 3.380 28.239433000.003295944.399.756215.61912295955.002956.466.1143 -3.46 915895955.00895956.656.0021 -1.65 96150010.901495947.8310.726423.07972095959.0021000.966.7515 -1.96 9827005.0027007.106.4747 -2.10 1242695952.002695910.3710.930041.63121033000.00295959.09 5.3484 0.9212113000.00295959.09 5.3484 0.91121435955.001495951.04 6.1150 3.96121435955.001495951.04 6.1150 3.9610225957.002095937.53 -4573 17.477 1042095957.002095955.15 -9949 -0.05 11122095954.002095955.15 -9949 -1.15 11122095954.00209 <td>7</td> <td>9</td> <td>29</td> <td>59</td> <td>51.00</td> <td>29</td> <td>59</td> <td>53.76</td> <td>6.7515</td> <td>-2.76</td> | 7 | 9 | 29 | 59 | 51.00 | 29 | 59 | 53.76 | 6.7515 | -2.76 |
| 9433000.003295944.399.756215.61912295953.00295956.466.1143 -3.46 915895955.00895956.656.0021 -1.65 96150010.901495947.8310.726423.07972095959.0021000.966.7515 -1.96 9827005.0027007.106.4747 -2.10 12921000.0021002.766.1143 -2.76 1242695952.002695910.3710.930041.63121033000.00295959.096.34840.9112151495955.00295959.096.34840.9112151495955.00295937.377.4771042095957.002095920.153.846536.8510121495950.001495951.0429.4376.0.0511122095957.002095957.15 -1.9949 .4.1511122095954.002095953.69 6.3484 0.3111122095954.00 <td>7</td> <td>6</td> <td>89</td> <td>59</td> <td>57.00</td> <td>89</td> <td>59</td> <td>28.77</td> <td>5.3380</td> <td>28.23</td> | 7 | 6 | 89 | 59 | 57.00 | 89 | 59 | 28.77 | 5.3380 | 28.23 |
| 912295953.00295956.466.1143 -3.46 915895955.00895956.656.0021 -1.65 96150010.901495947.8310.726423.07972095959.0021000.966.7515 -1.96 9827005.0027007.106.4747 -2.10 12921000.0021002.766.1143 -2.76 1242695952.002695910.3710.390041.6312103000.00295959.096.34840.91125900.0090042.6910.8959 -42.69 121495955.001495951.046.11503.96102295957.00295937.53 -4573 17.471042095957.00295959.1046.11503.9611122095954.002095955.15 -9949 -0.05 11122095954.002095957.36 -3484 0.31 1515001.0015002.96 3867 -1.96 151233001.001500 <td>9</td> <td>4</td> <td>330</td> <td>0</td> <td>0.00</td> <td>329</td> <td>59</td> <td>44.39</td> <td>9.7562</td> <td>15.61</td> | 9 | 4 | 330 | 0 | 0.00 | 329 | 59 | 44.39 | 9.7562 | 15.61 |
| 915895955.00895956.65 6.0021 -1.65 96150010.901495947.8310.726423.07972095959.0021000.96 6.7515 -1.96 9827005.0027007.10 6.4747 -2.10 12921000.0021002.76 6.1143 -2.76 1242695952.002695910.3710.930041.63121033000.00295958.92 6.3476 1.081213000.00295951.04 6.1150 3.96121495955.001495951.04 6.1150 3.9610121495955.00295937.53 7.4573 17.471042095957.002095920.15 9.8465 36.8510121495950.001495955.15 7.9949 -0.05 11122095954.002095955.15 7.9494 -1.15 11122095954.002095957.34 6.1150 4.66 151233001.001500 2.96 3.8467 -1.96 1112209 <th< td=""><td>9</td><td>12</td><td>29</td><td>59</td><td>53.00</td><td>29</td><td>59</td><td>56.46</td><td>6.1143</td><td>-3.46</td></th<> | 9 | 12 | 29 | 59 | 53.00 | 29 | 59 | 56.46 | 6.1143 | -3.46 |
| 96150010.901495947.8310.726423.07972095959.0021000.966.7515 -1.96 9827005.0027007.106.4747 -2.10 12921000.0021002.766.1143 -2.76 1242695952.002695910.3710.930041.63121033000.00295959.09 6.3484 0.911259000.00295959.09 6.3484 0.911259000.00295951.046.11503.96102295955.002951.046.11503.961042095957.002095920.153.846536.8510121495950.001495949.926.34760.08101213001.0033000.65 4581 $.3635$ 11122095954.002095955.15 9949 -1.15 11122095954.002095953.696.34840.3111215001.0015002.963.867 -1.96 151233002.00320 | 9 | 15 | 89 | 59 | 55.00 | 89 | 59 | 56.65 | 5.0021 | -1.65 |
| 972095959.0021000.966.7515 -1.96 9827005.0027007.106.4747 -2.10 12921000.0021002.766.1143 -2.76 1242695952.002695910.3710.930041.63121033000.00295958.926.34761.0812113000.00295959.096.34840.911259000.00295951.046.11503.96121495955.00295937.53 4573 17.471042095957.002095920.15 3.8465 36.8510121495950.001495949.92 6.3476 0.0810129005.009005.515 9949 -0.05 1122095954.002095955.15 9949 -1.15 11122095954.002095955.15 9949 -1.56 15151601.0015002.963.8367 -1.96 15151501.0015002.336.7515 1.67 15151621002.90 </td <td>9</td> <td>6</td> <td>150</td> <td>0</td> <td>10,90</td> <td>149</td> <td>59</td> <td>47.83</td> <td>10.7264</td> <td>23.07</td> | 9 | 6 | 150 | 0 | 10,90 | 149 | 59 | 47.83 | 10.7264 | 23.07 |
| 9827005.0027007.10 6.4747 -2.1012921000.0021002.76 6.1143 -2.761242695952.002695910.3712.930041.6312103000.003295958.92 6.3476 1.0812113000.00295959.09 6.3484 0.911259000.0090042.6912.8859-42.6912151495955.00295937.537.457317.471042095957.002095920.153.846536.8510121495950.001495949.926.34760.0810121495950.001495949.926.34760.08119005.009005.057.9949-0.0511122095954.002095955.157.9949-1.1511122095954.002095957.346.11504.661592695957.466.0021-1.56151233007.0033007.346.11504.661592695950.10295957.346.1150 | 9 | 7 | 209 | 59 | 59.00 | 210 | 0 | 0.96 | 6.7515 | -1.96 |
| 12921000.0021002.766.1143 -2.76 1242695952.002695910.3712.930041.63121033000.003295958.926.34761.0812113000.00295959.096.34840.911259000.0090042.6912.8959 -42.69 12151495955.001495951.046.11503.96102295955.002937.53 4573 17.471042095957.002095920.15 9.8465 36.8510121495950.001495949.92 6.3476 0.0810121495950.001495949.92 6.3476 0.081012130050.009005.05 9949 -0.05 112095954.002095953.69 6.3484 0.3111122095954.002095953.69 6.3484 0.31151501.0015002.96 3.867 -1.96 152.995950.00300 36.68 5.7449 -46.68 15123300 2.00 329 <t< td=""><td>9</td><td>8</td><td>270</td><td>0</td><td>5.00</td><td>270</td><td>0</td><td>7.10</td><td>6.4747</td><td>-2.10</td></t<> | 9 | 8 | 270 | 0 | 5.00 | 270 | 0 | 7.10 | 6.4747 | -2.10 |
| 1242695952.002695910.3712.930041.63121033000.003295958.92 $\epsilon.3476$ 1.0812113000.00295959.09 $\delta.3484$ 0.911259000.0090042.6912.8959-42.6912145955.001495951.04 $\delta.1150$ 3.96102295955.00295937.53 $T.4573$ 17.471042095957.002095920.15 9.8465 36.8510121495950.001495949.92 6.3476 0.0810119005.009005.05 $T.9949$ -0.05 1122095954.002695955.15 $T.9949$ -1.15 11122095954.002695957.34 6.38867 -1.96 151233001.0015002.96 3.8367 -1.96 152.95950.0030036.68 5.7449 -46.68 151233002.003295957.46 6.0021 -1.56 15621002.90210015.2112.7415 -12.31 15141500 </td <td>12</td> <td>9</td> <td>210</td> <td>Õ</td> <td>0.00</td> <td>210</td> <td>Õ</td> <td>2.76</td> <td>6.1143</td> <td>-2.76</td> | 12 | 9 | 210 | Õ | 0.00 | 210 | Õ | 2.76 | 6.1143 | -2.76 |
| 1 10 330 0 0.00 329 59 58.92 6.3476 1.08 12 11 30 0 0.00 29 59 59.09 6.3484 0.91 12 5 90 0 0.00 90 0 42.69 12.8959 -42.69 12 15 149 59 55.00 29 59 37.53 7.4573 17.47 10 4 209 59 57.00 209 59 20.15 9.8465 36.85 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 10 12 149 59 50.00 149 59 50.55 7.9949 -0.05 11 9 0 5.00 209 59 55.15 7.9949 -1.15 11 2 209 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2. | 12 | 4 | 269 | 59 | 52.00 | 269 | 59 | 10.37 | 10,9300 | 41.63 |
| 11 30 0 0.00 29 59 59.09 6.3484 0.91 12 5 90 0 0.00 90 0 42.69 12.8959 -42.69 12 15 149 59 55.00 29 59 37.53 7.4573 17.47 10 4 209 59 57.00 209 59 20.15 9.8465 36.85 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 10 12 130 0 1.00 300 0 65 7.4581 70.35 11 0 0 5.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 2.96 38367 -1.96 15 12 330 0 1.00 150 0 2.33 6.7515 1. | 12 | 10 | 330 | 0 | 0.00 | 329 | 59 | 58.92 | 5.3476 | 1.08 |
| 12159000.0090042.6912.8959 -42.69 12151495955.001495951.046.11503.96102295955.00295937.53 4573 17.47 1042095957.002095920.15 3.8465 36.8510121495950.001495949.92 6.3476 0.0810119005.009005.05 9949 -0.05 11233001.0033000.65 4581 .06.3511102695954.002695955.15 9949 -1.15 11122095954.002095953.69 6.3484 0.3111515001.0015002.96 3.8367 -1.96 155295950.0030036.68 5.7449 -46.68 16592695957.46 6.0021 -1.56 15621002.90210015.2112.7415 -12.31 151415004.0015002.33 6.7515 1.67 1513895950.10895949.13 6.4757 0.97 131495958.00 </td <td>12</td> <td>11</td> <td>30</td> <td>ő</td> <td>0.00</td> <td>2.9</td> <td>59</td> <td>59.09</td> <td>5.3484</td> <td>0.91</td> | 12 | 11 | 30 | ő | 0.00 | 2.9 | 59 | 59.09 | 5.3484 | 0.91 |
| 12 15 149 59 55.00 149 59 51.04 6.1150 3.96 10 2 29 59 55.00 29 59 37.53 7.4573 17.47 10 4 209 59 57.00 209 59 20.15 9.8465 36.85 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 11 90 0 5.00 90 0 5.05 7.9949 -0.05 11 2 209 59 54.00 209 59 55.15 7.9949 -1.15 11 2 209 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.867 -1.96 15 2 9 59 55.90 269 59 5 | 12 | 5 | 90 | 0 | 0.00 | 90 | 0 | 42.69 | 10.8959 | -42.69 |
| 10 2 29 59 55.00 29 59 37.53 7.4573 17.47 10 4 209 59 57.00 209 59 20.15 9.8465 36.85 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 10 11 90 0 5.00 90 0 5.05 7.9949 -0.05 11 2 330 0 1.00 330 0 0.65 7.4581 70.35 11 2 209 59 54.00 209 59 55.15 7.9949 -1.15 11 2 209 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.867 -1.96 15 29 59 50.00 30 0 36.68 5.7449 -46.68 15 2 330 0 2.00 329 59 57.46< | 12 | 15 | 149 | 59 | 35.00 | 149 | 59 | 51.04 | 6.1150 | 3.96 |
| 10 4 209 59 57.00 209 59 20.15 9.8465 36.85 10 12 149 59 50.00 149 59 49.92 6.3476 0.08 10 12 330 0 1.00 330 0 0.65 7.9949 -0.05 11 2 330 0 1.00 330 0 0.65 7.4581 .90.35 11 0 269 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.8367 -1.96 15 5 29 59 50.00 30 0 36.68 3.7449 -46.68 15 2 330 0 2.00 329 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 10.7415 -12.31 15 14 150 0 2.00 89 59 </td <td>10</td> <td>2</td> <td>29</td> <td>59</td> <td>55.00</td> <td>29</td> <td>59</td> <td>37.53</td> <td>- 4573</td> <td>17.47</td> | 10 | 2 | 29 | 59 | 55.00 | 29 | 59 | 37.53 | - 4573 | 17.47 |
| 1 149 59 50.00 149 59 49.92 6.3476 0.08 10 12 330 0 1.00 330 0 0.65 7.9949 -0.05 11 2 330 0 1.00 330 0 0.65 7.4581 40.35 11 2 209 59 54.00 209 59 55.15 7.9949 -1.15 11 2 209 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.8367 -1.96 15 2 30 0 36.68 3.7449 -46.68 15 2 30 0 2.00 329 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 10.7415 -12.31 15 330 0 7.00 330 0 7.34 12.0478 -0.34 <td< td=""><td>10</td><td>4</td><td>209</td><td>59</td><td>57.00</td><td>209</td><td>59</td><td>20.15</td><td>9.8465</td><td>36.85</td></td<> | 10 | 4 | 209 | 59 | 57.00 | 209 | 59 | 20.15 | 9.8465 | 36.85 |
| 1011900 5.00 900 5.05 7.9949 -0.05 11233001.003300 0.65 7.4581 70.35 1102695954.002695955.15 7.9949 -1.15 11122095954.002095953.69 6.3484 0.31 11515001.0015002.96 3.8367 -1.96 155295950.0030036.68 3.7449 -46.68 151233002.003295957.34 6.1150 4.66 1592695955.902695957.46 6.0021 -1.56 15621002.90210015.21 12.7415 -12.31 151415004.0015002.33 6.7515 1.67 1513895950.10895949.13 6.4757 0.97 1353300 7.00 3300 7.34 12.0478 -0.34 1415002.00895956.24 6.4757 1.76 13142095958.002095958.97 7.1610 -0.97 1331495953.001495951.87 2.3616 1.13 14 <td>10</td> <td>12</td> <td>149</td> <td>59</td> <td>50.00</td> <td>149</td> <td>59</td> <td>49.92</td> <td>5.3476</td> <td>0.08</td> | 10 | 12 | 149 | 59 | 50.00 | 149 | 59 | 49.92 | 5.3476 | 0.08 |
| 11 2 330 0 1.00 330 0 0.65 7.4581 7.35 11 0 269 59 55.15 7.9949 -1.15 11 12 209 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.8367 -1.96 15 5 29 59 50.00 30 0 36.68 3.7449 -46.68 15 2 330 0 2.00 329 59 57.34 6.1150 4.66 15 9 269 59 55.90 269 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 12.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 13 89 59 58.00 269 59 56.24 6.4757 0.97 | 10 | 11 | 90 | 0 | 5.00 | 90 | 0 | 5.05 | 9949 | -0.05 |
| 11 10 269 59 54.00 269 59 55.15 7.9949 -1.15 11 12 209 59 54.00 209 59 53.69 5.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.8367 -1.96 15 5 29 59 50.00 30 0 36.68 3.7449 -46.68 15 2 330 0 2.00 329 59 57.34 6.1150 4.66 15 9 269 59 55.90 269 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 12.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 15 330 0 7.00 330 0 7.34 12.0478 -0.34 15 269 59 58.00 209 59 58.97 < | 11 | 2 | 330 | 0 | 1.00 | 330 | 0 | 0.65 | -,4581 | 20.35 |
| 11 12 209 59 54.00 209 59 53.69 6.3484 0.31 11 5 150 0 1.00 150 0 2.96 3.8367 -1.96 15 5 29 59 50.00 30 0 36.68 3.7449 -46.68 15 12 330 0 2.00 329 59 57.34 6.1150 4.66 15 9 269 59 55.90 269 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 10.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 13 89 59 50.10 89 59 49.13 6.4757 0.97 13 5 330 0 7.00 330 0 7.34 10.0478 -0.34 14 209 59 58.00 209 59 58.97 | 11 | 10 | 269 | 59 | 54.00 | 269 | 59 | 55.15 | - 9949 | -1.15 |
| 11515001.0015002.96 \exists .8367-1.96155295950.0030036.68 \exists .7449-46.68151233002.003295957.34 6.1150 4.661592695955.902695957.46 6.0021 -1.5615621002.90210015.2110.7415-12.31151415004.0015002.33 6.7515 1.671513895950.10895949.13 6.4757 0.9713533007.0033007.3410.0478-0.3413152695958.002095958.971.1610-0.97131495953.001495951.87 $\epsilon.3616$ 1.131439002.00895959.621.3382.3814627000.00270026.30 $\epsilon.3539$ -26.3014153295958.003295956.93 $\epsilon.7515$ 1.071413295950.10295951.867.1610-1.76 | 11 | 12 | 209 | 59 | 54.00 | 209 | 59 | 53.69 | 5.3484 | 0.31 |
| 15 5 29 59 50.00 30 0 36.68 3.7449 -46.68 15 12 330 0 2.00 329 59 57.34 6.1150 4.66 15 9 269 59 55.90 269 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 12.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 15 13 89 59 50.10 89 59 49.13 6.4757 0.97 13 5 330 0 7.00 330 0 7.34 12.0478 -0.34 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 149 59 53.00 149 59 51.87 2.3616 1.13 14 3 90 0 2.00 89 59 59. | 11 | 5 | 150 | 0 | 1.00 | 150 | 0 | 2.96 | 3.8367 | -1.96 |
| 15 12 330 0 2.00 329 59 57.34 6.1150 4.66 15 9 269 59 55.90 269 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 12.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 15 13 89 59 50.10 89 59 49.13 6.4757 0.97 13 5 330 0 7.00 330 0 7.34 12.0478 -0.34 13 15 269 59 58.00 269 59 58.97 7.1610 -0.97 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 149 59 53.00 149 59 51.87 ٤.3616 1.13 14 3 90 0 2.00 89 59 | 15 | 5 | 29 | 59 | 50.00 | 30 | Õ | 36.68 | 3.7449 | -46.68 |
| 12 333 1100 269 59 57.46 6.0021 -1.56 15 6 210 0 2.90 210 0 15.21 12.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 15 13 89 59 50.10 89 59 49.13 6.4757 0.97 13 5 330 0 7.00 330 0 7.34 12.0478 -0.34 13 15 269 59 58.00 269 59 56.24 6.4757 1.76 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 149 59 53.00 149 59 51.87 2.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 26.30 2.3539 -26.30 14 | 15 | 12 | 330 | <u> </u> | 2 00 | 329 | 59 | 57.34 | 6.1150 | 4 66 |
| 15 6 210 0 2.90 210 0 15.21 10.7415 -12.31 15 14 150 0 4.00 150 0 2.33 6.7515 1.67 15 13 89 59 50.10 89 59 49.13 6.4757 0.97 13 5 330 0 7.00 330 0 7.34 10.0478 -0.34 13 15 269 59 58.00 269 59 56.24 6.4757 1.76 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 149 59 53.00 149 59 51.87 2.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 26.30 5.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 | 15 | 9 | 269 | 59 | 55 90 | 269 | 59 | 57 46 | 6 0021 | -1 56 |
| 151415004.0015002.33 6.7515 1.671513895950.10895949.13 6.4757 0.9713533007.0033007.3412.0478 -0.34 13152695958.002695956.24 6.4757 1.7613142095958.002095958.97 1610 -0.97 1331495953.001495951.87 6.3616 1.131439002.00895959.62 1338 2.3814627000.00270026.30 6.3539 -26.30 14153295958.003295956.93 6.7515 1.071413295950.10295951.86 7.1610 -1.76 | 15 | 6 | 210 | 0 | 2 90 | 210 | 0 | 15 21 | 10 7415 | -12 31 |
| 15 13 89 59 50.10 89 59 49.13 6.4757 0.97 13 5 330 0 7.00 330 0 7.34 12.0478 -0.34 13 15 269 59 58.00 269 59 56.24 6.4757 1.76 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 3 149 59 53.00 149 59 51.87 8.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 0.00 270 0 26.30 8.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 15 | 14 | 150 | 0 | 4.00 | 150 | 0 | 2.33 | 6.7515 | 1.67 |
| 13 5 330 0 7.00 330 0 7.34 12.0478 -0.34 13 15 269 59 58.00 269 59 56.24 6.4757 1.76 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 3 149 59 53.00 149 59 51.87 8.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 0.00 270 0 26.30 8.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 15 | 13 | 89 | 59 | 50.10 | 89 | 59 | 49.13 | 6.4757 | 0.97 |
| 13 15 269 59 58.00 269 59 56.24 6.4757 1.76 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 14 209 59 53.00 149 59 51.87 8.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 0.00 270 0 26.30 8.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 13 | 5 | 330 | 0 | 7.00 | 330 | 0 | 7.34 | 10478 | -0.34 |
| 13 14 209 59 58.00 209 59 58.97 7.1610 -0.97 13 3 149 59 53.00 149 59 51.87 2.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 0.00 270 0 26.30 2.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 13 | 15 | 269 | 59 | 58.00 | 269 | 59 | 56.24 | 6.4757 | 1.76 |
| 13 3 149 59 53.00 149 59 51.87 £.3616 1.13 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 0.00 270 0 26.30 £.3539 -26.30 14 15 329 59 58.00 329 59 56.93 £.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 13 | 14 | 209 | 59 | 58.00 | 209 | 59 | 58.97 | - 1610 - | -0.97 |
| 14 3 90 0 2.00 89 59 59.62 7.1338 2.38 14 6 270 0 0.00 270 0 26.30 2.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 13 | 3 | 149 | 59 | 53.00 | 149 | 59 | 51.87 | 2,3616 | 1.13 |
| 14 6 270 0 26.30 2.3539 -26.30 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 14 | 3 | 90 | 0 | 2.00 | 89 | 59 | 59.62 | 7,1338 | 2 38 |
| 14 15 329 59 58.00 329 59 56.93 6.7515 1.07 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 14 | 6 | 270 | č | 0.00 | 270 | 0 | 26.30 | 2.3539 | -26 30 |
| 14 13 29 59 50.10 29 59 51.86 7.1610 -1.76 | 14 | 15 | 329 | 59 | 58.00 | 329 | 59 | 56.93 | 6.7515 | 1.07 |
| | 14 | 13 | 2.9 | 59 | 50.10 | 29 | 59 | 51.86 | 7,1610 | -1.76 |

APPENDIX B.3: RESULTS FOR SUB-OPTIMAL FUSION DENSIFICATION

APPENDIX B.3.1: Results of the first level real network densification using sub-optimal

fusion approach

SECOND ORDER REAL NETWORK ADJUSTMENT (SUB-OPTIMAL FUSION APPROACH)

ITERATION = 2 VUW= 1.000000

RESULTS

| DISTANCE | : | TRACE1= | 30.000 | ETWE1= | 190. | 811 |
|------------|---|---------|--------|--------|------|-----|
| DIRECTIONS | : | TRACE2= | 52.000 | ETWE2= | 86. | 793 |

ADJUSTED OBSERVATIONS

| RAY | | OBSER | VED-DIST | A | DJUSTE | ED-DIST | STD-EF | RESIDUALS |
|-------|--------|--------|----------|------|--------|---------|--------|------------------|
| 12 7 | | 113 | 92.335 | | 11392 | 2.306 | 0.0143 | 0.029 |
| 12 9 | | 123 | 69.293 | | 12369 | 9.346 | 0.0148 | -0.053 |
| 13 9 | | 138 | 14.687 | | 13814 | .697 | 0.0166 | -0.010 |
| 14 6 | | 246 | 23.681 | | 24623 | 3.710 | 0.0243 | -0.029 |
| 14 8 | | 169 | 35.563 | | 16935 | 5.592 | 0.0190 | -0.029 |
| 15 6 | | 106 | 83.383 | | 10683 | 3.358 | 0.0145 | 0.025 |
| 16 5 | | 148 | 37.980 | | 14837 | 7.981 | 0.0155 | -0.001 |
| 16 6 | | 132 | 69.516 | | 13269 | 9.534 | 0.0157 | -0.018 |
| 16 8 | | 243 | 10.634 | | 24310 | 0.538 | 0.0151 | 0.096 |
| 17 7 | | 166 | 90.070 | | 16690 | 0.109 | 0.0188 | -0.039 |
| 18 20 | | 149 | 84.326 | | 14984 | 1.288 | 0.0164 | 0.038 |
| 18 7 | | 238 | 65.886 | | 23865 | 5.831 | 0.0205 | 0.055 |
| 18 5 | | 314 | 83.464 | | 31483 | 3.506 | 0.0246 | -0.042 |
| 19 26 | | 247 | 90.315 | | 24790 |).370 | 0.0229 | -0.055 |
| 19 20 | | 143 | 08.001 | | 14808 | 3.025 | 2.0170 |) <i>4</i> 6.024 |
| 20 21 | | 42 | 47.690 | | 4247 | 7.690 | 0.0106 | 5 .0.000 |
| 21 3 | | 103 | 40.648 | | 10340 |).553 | 5.0139 | 0.095 |
| 21 7 | | 350 | 00.587 | | 35000 |).722 | 1.0214 | -0.135 |
| 22 2 | | 161 | 16.390 | | 16116 | 5.922 | 0.0166 | -0.032 |
| 22 23 | | 152. | 38.942 | | 15238 | 8.933 | 1.0177 | 0.009 |
| 22 5 | | 233 | 94.975 | | 23394 | .968 | 0.0181 | 0.007 |
| 23 4 | | 153 | 96.022 | | 15396 | 5.085 | 0.0173 | -0.063 |
| 24 2 | | 158. | 23.386 | | 15824 | 1.036 | 0.0169 | -0.050 |
| 24 3 | | 174 | 16.302 | | 17476 | 5.312 | 0.0182 | -0.010 |
| 24 26 | | 337 | 94.283 | | 33794 | 1.461 | 0.0190 | -0.178 |
| 24 25 | | 236 | 81.294 | | 23681 | 285 | 0.0200 | 0.009 |
| 25 1 | | 254 | 19.370 | | 25419 | .342 | 0.0203 | 0.028 |
| 25 26 | | 135. | 52.337 | | 13552 | 2.330 | 0.0158 | 0.007 |
| 26 1 | | 163 | 36.366 | | 16336 | 5.668 | 0.0168 | -0.102 |
| 26 24 | | 337 | 94.482 | | 33794 | 1.461 | 0.0190 | 0.021 |
| į | ADJUST | ED DIR | ECTIONS | | | | | |
| RAY | OBS | ERVED- | DIRECT | ADJU | JSTED- | DIRECT | STD-ER | R RESIDUALS(") |
| 12 7 | 169 | 22 | 42.30 | 169 | 22 | 42.07 | 0.4396 | 0.23 |
| 12 9 | 37 | 17 | 34.90 | 37 | 17 | 36.11 | 0.4013 | -1.21 |
| 13 7 | 233 | 35 | 16.50 | 233 | 35 | 16.04 | 0.2754 | 0.46 |
| 13 8 | 106 | 41 | 48.00 | 106 | 41 | 48.62 | 0.5162 | -0.62 |

| 13 | 9 | 330 | 0 | 20.65 | 330 | 0 | 20.66 | 0.8656 | -0.01 |
|----|-----|-----|-----|-------|-----|----|-------|--------|-------|
| 14 | 6 | 231 | 32 | 25.31 | 231 | 32 | 24.83 | 0.2616 | 0.48 |
| 14 | 8 | 284 | 20 | 12.64 | 284 | 20 | 12.06 | 0.4146 | 9.58 |
| 14 | 11 | 341 | 1 | 11.63 | 341 | 1 | 11.22 | 0.1927 | 0.41 |
| 15 | 4 | 207 | 42 | 24.54 | 207 | 42 | 25.18 | 0.4994 | -0.64 |
| 15 | 5 | 257 | 44 | 42.41 | 257 | 44 | 42.35 | 0.3778 | 0.06 |
| 15 | 6 | 17 | 50 | 53.63 | 17 | 50 | 53.97 | 0.8211 | -0.34 |
| 16 | 5 | 194 | 6 | 54.60 | 194 | 6 | 54.51 | 0.2719 | 0.09 |
| 16 | 6 | 95 | 31 | 21.62 | 95 | 31 | 22.58 | 0.2826 | -0.96 |
| 16 | 8 | 41 | 24 | 51.23 | 41 | 24 | 52.10 | 0.1717 | -0.87 |
| 16 | 7 | 317 | 36 | 22.62 | 317 | 36 | 23.26 | 0.1736 | -0.64 |
| 17 | 5 | 149 | 36 | 47.34 | 149 | 36 | 47.90 | 0.7007 | -0.56 |
| 17 | 3 | 209 | 32 | 9.51 | 209 | 32 | 8.92 | 0.3496 | 0.59 |
| 17 | 18 | 275 | 15 | 46.63 | 275 | 15 | 46.87 | 0.2823 | -0.24 |
| 17 | 7 | 352 | 11 | 25.96 | 352 | 11 | 27.33 | 0.6342 | -1.37 |
| 18 | 20 | 186 | 37 | 34.51 | 186 | 37 | 34.04 | 0.4104 | 0.47 |
| 18 | 7 | 52 | 19 | 28.91 | 52 | 19 | 28.29 | 0.2190 | 0.62 |
| 18 | 17 | 95 | 15 | 46.03 | 95 | 15 | 46.87 | 0.2823 | -0.84 |
| 18 | 5 | 116 | 21 | 25.06 | 116 | 21 | 26.10 | 0.1456 | -1.04 |
| 19 | 26 | 222 | 47 | 24.01 | 222 | 47 | 23.85 | 0.3632 | 0.16 |
| 19 | 24 | 143 | 18 | 7.51 | 143 | 18 | 6.52 | 0.2145 | 0.99 |
| 19 | 3 | 105 | 26 | 4.12 | 105 | 26 | 5.47 | 0.2818 | -1.35 |
| 19 | 20 | 78 | 16 | 29.43 | 78 | 16 | 30.39 | 0.5550 | -1.46 |
| 20 | 21 | 108 | 30 | 23.41 | 108 | 30 | 25.27 | 0.6649 | -1.86 |
| 20 | 18 | 6 | 37 | 34.92 | 6 | 37 | 34.04 | 0.4104 | 0.88 |
| 20 | 19 | 258 | 16 | 29.64 | 258 | 16 | 30.89 | 0.5550 | -1.25 |
| 21 | 3 | 144 | 36 | 27.98 | 144 | 36 | 31.56 | 0.4936 | -3.58 |
| 21 | 20 | 288 | 30 | 23.42 | 288 | 30 | 25.27 | 0.6649 | -1.85 |
| 21 | 7 | 28 | 17 | 39.99 | 28 | 17 | 38.78 | 0.1190 | 1.21 |
| 22 | 2 | 186 | 46 | 39.33 | 186 | 46 | 37.09 | 0.4767 | 2.24 |
| 22 | 23 | 120 | 5 | 28.54 | 120 | 5 | 30.70 | 0.3216 | -2.16 |
| 22 | 5 | 33 | 37 | 5.13 | 33 | 37 | 5.66 | 0.3242 | -0.53 |
| 22 | 3 | 321 | 36 | 42.00 | 321 | 36 | 41.:0 | 0.4587 | 0.60 |
| 23 | 2 | 240 | 59 | 50.20 | 240 | 59 | 49.73 | 0.3610 | 0.47 |
| 23 | 4 | 19 | 32 | 28.15 | 19 | 32 | 29.14 | 0.5247 | -0.99 |
| 23 | 22 | 300 | 5 | 28.42 | 300 | 5 | 30.70 | 0.3216 | -2.28 |
| 24 | 2 | 125 | 26 | 21.12 | 125 | 26 | 25.12 | 0.2842 | -4.00 |
| 24 | 3 | 26 | 35 | 49.90 | 26 | 35 | 48.31 | 0.2348 | 11.09 |
| 24 | 19 | 323 | 1.8 | 7.51 | 323 | 18 | 6.32 | 0.2145 | 0.99 |
| 24 | 26 | 277 | 2 | 39.00 | 277 | 8 | 39.11 | 0.2134 | -0.11 |
| 24 | 25 | 258 | 4 | 39.42 | 258 | 47 | 39.25 | 0.3421 | 0.17 |
| 25 | 1 | 275 | 1.8 | 29.72 | 275 | 18 | 26.60 | 0.3295 | 3.12 |
| 25 | 2.6 | 310 | 31 | 10.60 | 310 | 31 | 11.62 | 0.4325 | -1.02 |
| 25 | 24 | 78 | 4 | 38.42 | 78 | 47 | 39.75 | 0.3421 | -0.83 |
| 26 | 1 | 246 | 43 | 54.13 | 246 | 43 | 54.=- | 0.4352 | -0.84 |
| 26 | 25 | 130 | 31 | 11.12 | 130 | 31 | 11.62 | 0.4325 | -0.50 |
| 26 | 24 | 97 | 8 | 39.56 | 97 | 8 | 39.11 | 0.2134 | 0.45 |
| 26 | 19 | 42 | 4 - | 24.43 | 42 | 47 | 23.85 | 0.3632 | 0.58 |
| - | | | - | | | | | | 0.00 |

APPENDIX B.3.2: Results of the first level simulated network densification using sub-

optimal fusion

SECOND ORDER SIMULATED NETWORK ADJUSTMENT (SUB-OPTIMAL FUSION APPROACH)

ITERATION = 2 VUW= 0.935921

RESULTS

| DISTANCE | : | TRACE1= | 9.000 | ETWE1= | 8.777 | VCl= | 0.753 |
|--------------|---|----------|--------|--------|--------|------|-------|
| DIRECTIONS : | : | TRACE2= | 18.000 | ETWE2= | 16.708 | VC2= | 2.039 |
| RESTRICTIONS | S | :TRACE3= | 0.000 | ETWE3= | 8.278 | VC3= | 2.514 |

ADJUSTED OBSERVATIONS

| | ADJUS | TED DISTANCES | | | |
|----|-------|---------------|---------------|---------|-----------|
| RA | Y | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
| 1 | 4 | 200.0600 | 199.6483 | 0.0053 | 0.4117 |
| 1 | 6 | 200.0400 | 200.1119 | 0.0054 | -0.0719 |
| 2 | 4 | 200.0800 | 200.2265 | 0.0054 | -0.1465 |
| 2 | 5 | 199.9800 | 200.5482 | 0.0054 | -0.5682 |
| 3 | 5 | 200.0300 | 199.4195 | 0.0053 | 0.6105 |
| 3 | 6 | 199.9300 | 199.9170 | 0.0054 | 0.0130 |
| 4 | 5 | 200.0200 | 199.9965 | 0.0046 | 0.0235 |
| 4 | 6 | 200.0900 | 199.2806 | 0.0046 | 0.8094 |
| 5 | 6 | 199.9200 | 199.5369 | 0.0046 | 0.3831 |

ADJUSTED DIRECTIONS

| RA | Y | OBSEF | NVED- | DIRECT | ADJU | JSTED | -DIRECT | STD-ERR | RESIDUALS(" |
|----|-------------------|-------|----------|--------|------|-------|---------|---------|-------------|
| 1 | 4 | 30 | 0 | 0.00 | 29 | 59 | 57.94 | 3.7048 | 2.06 |
| 1 | 6 | 90 | 0 | 10.61 | 90 | 0 | 11.35 | 3.5314 | -0.74 |
| 2 | \mathcal{L}_{2} | 209 | 59 | 53.01 | 209 | 59 | 56.43 | 3.5488 | -3.42 |
| 2 | 5 | 150 | О | 4.99 | 150 | 0 | 1.67 | 3.5483 | 3.32 |
| 3 | 5 | 329 | 59 | 54.99 | 329 | 59 | 58.83 | 3.7060 | -3.84 |
| 3 | 6 | 270 | Ū | 3.01 | 269 | 59 | 59.86 | 3.5325 | 3.15 |
| 4 | 1 | 210 | 0 | 0.00 | 209 | 59 | 57.94 | 3.7048 | 2.06 |
| 4 | 2 | 30 | 0 | 7.00 | 30 | 0 | 9.02 | 3.5488 | -2.02 |
| 4 | 5 | 89 | 59 | 52.62 | 89 | 59 | 53.21 | 4.1041 | -0.59 |
| 4 | 6 | 150 | 0 | 5.42 | 150 | 0 | 5.02 | 4.1041 | 0.40 |
| 5 | 2 | 329 | 59 | 50.90 | 329 | 59 | 48.99 | 3.5483 | 1.91 |
| 5 | 4 | 270 | 2 | 4.37 | 270 | 0 | 3.79 | 4.1041 | 0.58 |
| 5 | 6 | 209 | 59 | 58.02 | 209 | 59 | 58.45 | 4.1041 | -0.43 |
| 5 | 3 | 150 | - | 13.96 | 150 | 0 | 15.91 | 3.7060 | 1.95 |
| 6 | 1 | 270 | 0 | 0.00 | 270 | 0 | 1.80 | 3.5314 | /-1.80 |
| 6 | 4 | 329 | 59 | 57.71 | 329 | 59 | 58.09 | 4.1041 | -0.38 |
| 6 | 5 | 30 | Û | 6.43 | 30 | 0 | 6.02 | 4.1041 | 0.41 |
| 6 | 3 | 89 | () () | 54.98 | 89 | 59 | 52.64 | 3.5325 | 2.34 |

APPENDIX B.3.3: Results of the second level real network densification using sub-

optimal fusion

THIRD ORDER REAL NETWORK ADJUSTMENT (SUB-OPTIMAL FUSION APPROACH)

ITERATION = 2 VUW= 1.0024

RESULTS

| DISTANCE | : | TRACE1= | 30.000 | ETWE1= | 427.703 |
|------------|---|---------|--------|--------|---------|
| DIRECTIONS | : | TRACE2= | 50.000 | ETWE2= | 462.847 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| RA | λY | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|----|---------------|---------------|---------|-----------|
| 27 | 26 | 14773.890 | 14774.000 | 0.0173 | -0.110 |
| 27 | 28 | 9653.420 | 9653.427 | 0.0113 | -0.007 |
| 28 | 29 | 13934.030 | 13933.904 | 0.0124 | 0.126 |
| 28 | 24 | 17550.110 | 17550.101 | 0.0149 | 0.009 |
| 29 | 3 | 14026.280 | 14026.123 | 0.0127 | 0.157 |
| 29 | 24 | 7500.980 | 7501.022 | 0.0121 | -0.042 |
| 30 | 22 | 20768.540 | 20768.432 | 0.0252 | 0.108 |
| 30 | 23 | 7148.220 | 7148.174 | 0.0229 | 0.046 |
| 31 | 4 | 10861.010 | 10861.021 | 0.0120 | -0.011 |
| 31 | 5 | 18725.550 | 18725.561 | 0.0144 | -0.011 |
| 32 | 3 | 12954.160 | 12954.270 | 0.0128 | -0.110 |
| 32 | 21 | 14309.080 | 14309.127 | 0.0174 | -0.047 |
| 33 | 5 | 6615.690 | 6615.769 | 0.0097 | -0.079 |
| 33 | 4 | 9616.290 | 9616.256 | 0.0107 | 0.034 |
| 34 | 18 | 6763.580 | 6763.531 | 0.0154 | 0.049 |
| 34 | 21 | 10493.270 | 10493.321 | 0.0139 | -0.051 |
| 34 | 20 | 10463.230 | 10463.187 | 0.0152 | 0.043 |
| 35 | 16 | 7137.810 | 7137.810 | 0.0126 | 0.000 |
| 35 | 17 | 7795.220 | 7795.275 | 0.0365 | -0.055 |
| 36 | 7 | 13557.220 | 13557.214 | 0.0128 | 0.006 |
| 36 | 18 | 11414.360 | 11414.413 | 0.0177 | -0.053 |
| 37 | 35 | 10445.030 | 10445.024 | 0.0103 | 0.006 |
| 37 | 17 | 7476.300 | 7476.322 | 0.0243 | -0.022 |
| 37 | 7 | 11935.450 | 11935.492 | 0.0114 | -0.042 |
| 38 | 8 | 15218.090 | 15218.053 | 0.0112 | 0.032 |
| 38 | 16 | 13176.150 | 13176.170 | 0.0154 | -0.020 |
| 38 | 7 | 14752.400 | 14752.410 | 0.0118 | -0.010 |
| 39 | 14 | 17156.360 | 17156.330 | 0.0170 | 0.030 |
| 40 | 11 | 12385.920 | 12385.859 | 0.0128 | 0.061 |
| 41 | 13 | 17334.620 | 17334.604 | 0.0343 | 0.016 |

ADJUSTED DIRECTIONS

| | | | | | | | | | 1 4 |
|----|----|-------|--------|--------|-----|--------|---------|---------|-------------|
| R | AY | OBSEI | RVED-1 | DIRECT | ADJ | USTED- | -DIRECT | STD-ERR | RESIDUALS " |
| 27 | 26 | 232 | 51 | 31.26 | 232 | 51 | 33.18 | 0.4277 | -1.92 |
| 27 | 19 | 28 | 38 | 17.97 | 28 | 38 | 21.90 | 0.5851 | -3.93 |
| 27 | 28 | 149 | 41 | 47.26 | 149 | 41 | 44.31 | 0.4504 | 2.95 |
| 28 | 27 | 329 | 41 | 49.25 | 329 | 41 | 44.31 | 0.4504 | 4.94 |
| 28 | 29 | 81 | 34 | 28.89 | 81 | 34 | 31.50 | 0.3747 | -2.61 |
| 28 | 24 | 105 | 50 | 4.45 | 105 | 49 | 58.17 | 0.3297 | 6.28 |
| 28 | 25 | 214 | 2 | 52.29 | 214 | 2 | 53.15 | 0.5014 | -0.86 |
| 29 | 3 | 51 | 9 | 34.82 | 51 | 9 | 31.83 | 0.2727 | 2.99 |
| 29 | 24 | 155 | 35 | 6.04 | 155 | 34 | 53.94 | 0.4752 | 12.10 |
| 29 | 28 | 261 | 34 | 28.99 | 261 | 34 | 31.50 | 0.3747 | -2.51 |
| 30 | 22 | 285 | 27 | 41.43 | 285 | 27 | 41.36 | 0.3316 | -0.13 |
| 30 | 4 | 352 | 16 | 43.10 | 352 | 16 | 40.43 | 0.3789 | 2.67 |
| 30 | 23 | 252 | 53 | 6.97 | 252 | 53 | 6.05 | 0.7934 | 0.92 |
| 31 | 4 | 58 | 16 | 33.02 | 58 | 16 | 32.96 | 0.4150 | 0.06 |
| 31 | 22 | 262 | 44 | 43.89 | 262 | 44 | 46.80 | 0.5035 | -2.91 |
| 31 | 5 | 11 | 53 | 0.49 | 11 | 53 | 0.35 | 0.2377 | 0.14 |
| 32 | 5 | 86 | 39 | 13.99 | 86 | 39 | 15.98 | 0.3762 | -1.99 |
| 32 | 3 | 219 | 27 | 48.46 | 219 | 27 | 42.94 | 0.3869 | 5.52 |
| 32 | 21 | 263 | 41 | 41.82 | 263 | 41 | 39.77 | 0.3563 | 2.05 |
| 32 | 17 | 20 | 2 | 9.29 | 20 | 2 | 13.93 | 0.6875 | -4.64 |
| 33 | 5 | 297 | 4 | 1.97 | 297 | 4 | 2.05 | 0.4370 | -0.08 |
| | | | | | | | | | |

1

| 33 | 15 | 52 | 8 | 46.69 | 52 | 8 | 48.19 | 0.5463 | -1.50 |
|----|----|-----|----|-------|-----|----|-------|--------|-------|
| 33 | 4 | 183 | 1 | 59.52 | 183 | 1 | 58.04 | 0.3115 | 1.48 |
| 34 | 18 | 329 | 7 | 12.99 | 329 | 7 | 18.54 | 0.6896 | -5.55 |
| 34 | 17 | -7 | 42 | 3.25 | 77 | 42 | 2.82 | 0.2589 | 0.43 |
| 34 | 21 | 186 | 24 | 52.69 | 186 | 24 | 47.27 | 0.4962 | 5.42 |
| 34 | 20 | 209 | 48 | 10.99 | 209 | 48 | 6.90 | 0.4675 | 4.09 |
| 35 | 16 | 32 | 10 | 16.87 | 32 | 10 | 15.03 | 0.5285 | 1.84 |
| 35 | 5 | 178 | 45 | 7.49 | 178 | 45 | 7.15 | 0.4093 | 0.34 |
| 35 | 17 | 298 | 10 | 32.64 | 298 | 10 | 30.51 | 0.6687 | 2.13 |
| 36 | 12 | 32 | 44 | 39.26 | 32 | 44 | 38.86 | 0.3203 | 0.40 |
| 36 | 7 | 67 | 59 | 6.55 | 67 | 59 | 3.68 | 0.4109 | 2.87 |
| 36 | 18 | 213 | 37 | 30.21 | 213 | 37 | 30.98 | 0.5468 | -0.77 |
| 37 | 16 | 120 | 40 | 11.50 | 120 | 40 | 10.95 | 0.4504 | 0.55 |
| 37 | 35 | 163 | 45 | 30.30 | 163 | 45 | 32.10 | 0.3530 | -1.80 |
| 37 | 17 | 211 | 53 | 41.82 | 211 | 53 | 41.59 | 1.0290 | 0.23 |
| 37 | 7 | 328 | 36 | 9.94 | 328 | 36 | 8.85 | 0.3304 | 1.09 |
| 38 | 8 | 70 | 7 | 12.51 | 70 | 7 | 10.81 | 0.2379 | 1.70 |
| 38 | 16 | 187 | 43 | 14.82 | 187 | 43 | 15.95 | 0.2839 | -1.13 |
| 38 | 7 | 274 | 20 | 37.98 | 274 | 20 | 38.84 | 0.2389 | -0.86 |
| 38 | 13 | 346 | 41 | 53.56 | 346 | 41 | 53.73 | 0.8406 | -0.17 |
| 39 | 8 | 359 | 53 | 6.52 | 359 | 53 | 7.14 | 0.4408 | -0.62 |
| 39 | 14 | -2 | 48 | 16.88 | 72 | 48 | 15.27 | 0.6500 | 1.61 |
| 39 | 6 | 195 | 45 | 58.94 | 195 | 45 | 58.37 | 0.5400 | 0.57 |
| 40 | 11 | 0 | 27 | 45.30 | 0 | 27 | 45.28 | 0.6101 | 0.02 |
| 40 | 14 | 140 | 45 | 14.38 | 140 | 45 | 12.28 | 0.5684 | 2.10 |
| 40 | 8 | 240 | 29 | 37.98 | 240 | 29 | 40.72 | 0.4435 | -2.74 |
| 41 | 10 | 293 | 52 | 37.34 | 293 | 52 | 36.45 | 0.5523 | 0.89 |
| 41 | 11 | 64 | 54 | 8.77 | 64 | 34 | 7.82 | 0.6447 | 0.95 |
| 41 | 13 | 244 | 2 | 51.24 | 244 | 2 | 51.71 | 0.4993 | -0.47 |

APPENDIX B.3.4: Results of the second level simulated network densification using

sub-optimal fusion

THIRD ORDER SIMULATED NETWORK ADJUSTMENT (SUB-OPTIMAL FUSION APPROACH)

14.1

ITERATION = 2 VUW= 0.986242

RESULTS

| DISTANCE : | | TRACE1= | 30.000 | ETWE1= | | 5.408 | VCl= | C | .180 |
|--------------|---|---------|--------|--------|---|-------|------|---|------|
| DIRECTIONS : | | TRACE2= | 60.000 | ETWE2= | 5 | 9.504 | VC2= | 1 | .575 |
| RESTRICTIONS | ; | TRACE3= | 0.000 | ETWE3= | 2 | 5.477 | VC3= | C | .870 |

ADJUSTED OBSERVATIONS

| RA | ΥA | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|----|---------------|---------------|---------|-----------|
| 1 | 7 | 100.0400 | 99.8721 | 0.0037 | 0.1679 |
| 1 | 8 | 100.0600 | 99.9849 | 0.0034 | 0.0751 |
| 2 | 10 | 100.0800 | 99.9189 | 0.0036 | 0.1611 |
| 2 | 11 | 99.9800 | 99.8231 | 0.0036 | 0.1569 |
| 3 | 13 | 100.0300 | 100.0686 | 0.0034 | -0.0386 |
| 3 | 14 | 99.9300 | 100.0531 | 0.0037 | -0.1231 |
| 4 | 8 | 100.0200 | 99.8181 | 0.0048 | 0.2019 |

| 4 9 4 10 4 12 5 11 5 12 5 13 5 15 6 7 6 9 6 14 6 15 7 9 8 7 9 12 9 15 10 11 12 10 12 11 12 15 13 14 15 13 | | 100 100 99 99 99 99 99 99 99 99 99 99 99 99 9 | 0.0400 0.0300 9.9700 9.9900 9.9900 9.9400 9.9800 9.9800 9.9300 0.0300 0.0200 9.9700 0.0600 0.0600 0.0600 0.0600 9.9800 9.9900 9.0000 9.0000 9.0000 9.0000 9.0000 9.0000 9.0000 9.0000 9.0000 9.0000 9.00000 9.00000 9.00000 9.00000 9.0000000000 | | 999. 100. 999. 100. 100. 100. 100. 100. | 5176 2870 7515 5302 2471 5669 2268 0493 8475 8569 0537 0300 0203 0786 0240 9842 9793 9920 0619 0724 0863 0652 | 0.0045 0.0048 0.0040 0.0048 0.0040 0.0045 0.0053 0.0040 0.0053 0.0040 0.0024 0.0025 0.0024 0.0023 0.0024 0.0025 0.0024 0.0024 0.0025 0.0024 0.0024 0.0023 0.0024 0.00 | 0.5224 -0.2570 0.2185 -0.6402 -0.1671 0.4231 0.1731 -0.2468 -0.1193 0.1825 0.1631 -0.0837 -0.0300 0.0397 -0.0386 -0.0140 0.0158 0.0807 -0.0120 -0.0919 -0.1124 -0.0363 -0.0352 |
|--|---|---|--|--|--|---|--|--|
| AD | JUSTEE | DIR | ECTIONS | | | | | |
| RAY 1 8 1 7 2 10 2 11 3 13 3 14 4 9 4 12 4 10 5 12 5 15 5 13 6 9 6 15 6 14 8 7 8 9 4 12 5 15 5 13 6 7 9 6 15 8 7 9 8 4 1 7 9 6 15 9 12 9 15 9 6 9 12 9 15 9 7 9 8 9 7 9 8 9 8 9 8 9 8 9 15 9 7 9 8 9 7 9 8 9 7 9 8 9 7 9 8 9 7 9 7 9 8 9 7 9 8 9 7 9 8 9 7 9 8 9 7 9 8 9 8 9 15 9 8 9 15 9 8 9 15 9 7 9 15 9 15 15 15 15 15 15 15 15 15 15 | OBSER 29 89 209 149 330 269 209 150 90 300 269 210 150 270 329 30 90 210 150 290 210 150 290 210 150 29 330 29 89 330 29 89 330 29 89 30 20 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 329 270 270 329 270 270 329 270 270 329 270 270 329 270 329 270 329 270 270 329 270 329 270 329 270 329 270 329 270 270 329 270 270 329 270 329 270 329 270 320 270 329 270 329 270 329 270 329 270 329 270 329 270 270 270 290 270 290 270 300 270 270 270 270 270 270 270 270 270 2 | | DIRECT 54.90 53.00 57.01 58.00 0.00 52.01 53.00 4.00 2.62 8.42 2.90 54.37 5.02 3.96 9.00 54.37 5.02 3.96 9.00 54.71 6.43 1.98 0.00 0.10 0.10 57.90 0.00 57.90 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.10 0.10 57.90 0.00 57.00 0.00 57.00 0.10 0.10 57.90 0.00 57.00 0.10 0.10 57.90 0.00 57.00 0.10 0.10 57.90 0.00 57.90 0.00 57.00 0.00 57.00 0.00 57.90 0.00 57.90 0.00 57.00 0.00 57.90 0.00 57.00 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.90 0.00 57.00 0.00 57.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 0.00 57.00 57.00 0.00 50.00 | ADJ 29 89 210 149 300 269 210 150 270 210 150 270 229 90 209 150 89 300 269 300 269 300 269 300 269 300 269 300 269 150 89 300 269 209 150 89 300 209 150 89 300 209 150 209 209 209 209 200 209 200 200 200 20 | CSTED- 59 59 59 59 59 59 59 59 59 59 59 59 59 | DIRECT 24.70 48.21 25.34 59.76 2.73 53.15 23.25 16.75 30.54 40.20 1.14 26.23 30.28 1.21 13.82 42.03 41.20 0.85 29.80 2.72 56.07 28.15 55.21 12.62 48.16 1.82 12.75 48.75 53.24 58.22 56.16 0.97 | STD-ERR 5.9021 5.2531 5.1278 5.1279 5.9031 5.2534 8.1620 8.0949 9.2220 8.1219 8.1142 9.1973 8.0880 8.1684 6.8056 9.1915 9.2033 6.8161 5.9021 3.9740 3.9740 3.9726 8.1620 5.2531 3.9740 3.9733 6.8056 8.0949 3.6127 3.6188 9.1915 3.9733 3.9726 | RESIDUALS(30.20 4.79 -28.33 -1.76 -2.73 -1.14 -30.25 -12.75 32.08 28.22 71.76 -2.75 -4.82 12.68 25.23 1.13 30.20 -2.62 4.03 -30.25 4.79 -2.62 2.84 -4.82 -12.75 4.25 1.76 12.68 2.84 4.03 |

| 10 | 12 | 149 | 59 | 50.00 | 149 | 59 | 51.48 | 3.9714 | -1.48 |
|----|----|-----|----|-------|-----|----|-------|--------|--------|
| 10 | 11 | 90 | 0 | 5.00 | 90 | 0 | 4.08 | 3.9727 | 0.92 |
| 11 | 2 | 330 | 0 | 1.00 | 330 | 0 | 2.76 | 5.1279 | -1.76 |
| 11 | 10 | 269 | 59 | 54.00 | 269 | 59 | 53.08 | 3.9727 | 0.92 |
| 11 | 12 | 209 | 59 | 54.00 | 209 | 59 | 55.22 | 3.9725 | -1.22 |
| 11 | 5 | 150 | 0 | 1.00 | 149 | 59 | 59.24 | 8.1142 | 1.76 |
| 12 | 9 | 210 | 0 | 0.00 | 209 | 59 | 55.75 | 3.6127 | 4.25 |
| 12 | 4 | 269 | 59 | 52.00 | 269 | 59 | 19.92 | 9.2220 | 32.08 |
| 12 | 10 | 330 | 0 | 0.00 | 330 | 0 | 1.48 | 3.9714 | -1.48 |
| 12 | 11 | 30 | 0 | 0.00 | 30 | 0 | 1.22 | 3.9725 | -1.22 |
| 12 | 5 | 90 | 0 | 0.00 | 90 | 0 | 31.86 | 9.1973 | -31.86 |
| 12 | 15 | 149 | 59 | 55.00 | 150 | 0 | 1.68 | 3.6128 | -6.68 |
| 13 | 5 | 330 | 0 | 7.00 | 330 | 0 | 4.25 | 8.1684 | 2.75 |
| 13 | 15 | 269 | 59 | 58.00 | 270 | 0 | 0.74 | 3.9736 | -2.74 |
| 13 | 14 | 209 | 59 | 58.00 | 209 | 59 | 56.51 | 3.9738 | 1.49 |
| 13 | 3 | 149 | 59 | 53.00 | 149 | 59 | 55.73 | 5.9031 | -2.73 |
| 14 | 3 | 90 | О | 2.00 | 90 | 0 | 3.14 | 5.2534 | -1.14 |
| 14 | 6 | 270 | 0 | 0.00 | 269 | 59 | 58.87 | 6.8161 | 1.13 |
| 14 | 15 | 329 | 59 | 58.00 | 329 | 59 | 59.99 | 3.9731 | -1.99 |
| 14 | 13 | 29 | 59 | 50.10 | 29 | 59 | 48.61 | 3.9738 | 1.49 |
| 15 | 5 | 29 | 59 | 50.00 | 30 | 0 | 15.26 | 8.0880 | -25.26 |
| 15 | 12 | 330 | 0 | 2.00 | 330 | 0 | 8.68 | 3.6128 | -6.68 |
| 15 | 9 | 269 | 59 | 55.90 | 269 | 59 | 54.14 | 3.6188 | 1.76 |
| 15 | 6 | 210 | 0 | 2.90 | 209 | 59 | 37.67 | 9.2033 | 25.23 |
| 15 | 14 | 150 | 0 | 4.00 | 150 | 0 | 5.99 | 3.9731 | -1.99 |
| 15 | 13 | 89 | 59 | 50.10 | 89 | 59 | 52.84 | 3.9736 | -2.74 |

APPENDIX B.4: RESULTS FOR DYNAMIC DENSIFICATION

APPENDIX B.4.1: Results of the first level real network densification using dynamic

approach

SECOND ORDER REAL NETWORK ADJUSTMENT (DYNAMIC ADJUSTMENT)

ITERATION = 0 VUW= 1.00938

RESULTS

| DISTANCE | : | TRACE1= | 30. | 000 | ETWE1= | 19.093 |
|------------|---|---------|-----|-----|--------|--------|
| DIRECTIONS | : | TRACE2= | 52. | 000 | ETWE2= | 10.738 |

ADJUSTED OBSERVATIONS

| RA | Y | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|---|---------------|---------------|---------|-----------|
| 12 | 7 | 11392.335 | 11392.344 | 0.0158 | -0.009 |
| 12 | 9 | 12369.293 | 12369.301 | 0.0164 | -0.008 |
| 13 | 9 | 13814.687 | 13814.684 | 0.0184 | 0.003 |
| 14 | 6 | 24623.681 | 24623.697 | 0.0269 | -0.016 |
| 14 | 8 | 16935.563 | 16935.557 | 0.0211 | 0.006 |
| 15 | 6 | 10683.383 | 10683.384 | 0.0160 | -0.001 |
| 16 | 5 | 14837.980 | 14837.969 | 0.0171 | 0.011 |
| 16 | б | 13269.516 | 13269.524 | 0.0173 | -0.008 |
| 16 | 8 | 24310.634 | 24310.592 | 0.0167 | 0.042 |
| 17 | 7 | 16690.070 | 16690.071 | 0.0209 | -0.001 |

| 18 | 20 | 14984.326 | 14984.288 | 0.0183 | 0.038 |
|----|----|-----------|-----------|--------|--------|
| 18 | 7 | 23865.886 | 23865.798 | 0.0227 | 0.088 |
| 18 | 5 | 31483.464 | 31483.585 | 0.0273 | -0.121 |
| 19 | 26 | 24790.315 | 24790.370 | 0.0255 | -0.055 |
| 19 | 20 | 14808.001 | 14808.025 | 0.0188 | -0.024 |
| 20 | 21 | 4247.690 | 4247.690 | 0.0118 | 0.000 |
| 21 | 3 | 10340.648 | 10340.632 | 0.0151 | 0.016 |
| 21 | 7 | 35000.587 | 35000.681 | 0.0237 | -0.094 |
| 22 | 2 | 16116.890 | 16116.934 | 0.0180 | -0.044 |
| 22 | 23 | 15238.942 | 15238.933 | 0.0197 | 0.009 |
| 22 | 5 | 23394.975 | 23395.007 | 0.0199 | -0.032 |
| 23 | 4 | 15396.022 | 15396.042 | 0.0192 | -0.020 |
| 24 | 2 | 15823.986 | 15824.010 | 0.0182 | -0.024 |
| 24 | 3 | 17476.302 | 17476.297 | 0.0199 | 0.005 |
| 24 | 26 | 33794.283 | 33794.461 | 0.0212 | -0.178 |
| 24 | 25 | 23681.294 | 23681.285 | 0.0222 | 0.009 |
| 25 | 1 | 25419.370 | 25419.365 | 0.0221 | 0.005 |
| 25 | 26 | 13552.337 | 13552.330 | 0.0176 | 0.007 |
| 26 | 1 | 16336.566 | 16336.636 | 0.0179 | -0.070 |
| 26 | 24 | 33794.482 | 33794.461 | 0.0212 | 0.021 |

ADJUSTED DIRECTIONS

| RA | Y | OBSER | RVED-I | DIRECT | ADJI | USTED | -DIRECT | STD-ERR | RESIDUALS(") |
|----|----|-------|--------|--------|------|-------|---------|----------|--------------|
| 12 | 7 | 169 | 22 | 42.30 | 169 | 22 | 41.74 | 0.4876 | 0.56 |
| 12 | 9 | 37 | 17 | 34.90 | 37 | 17 | 36.18 | 0.4457 | -1.28 |
| 13 | 7 | 233 | 35 | 16.50 | 233 | 35 | 16.39 | 0.3053 | 0.11 |
| 13 | 8 | 106 | 41 | 48.00 | 106 | 41 | 49.16 | 0.5737 | -1.16 |
| 13 | 9 | 330 | 0 | 20.65 | 330 | 0 | 21.30 | 0.9621 | -0.65 |
| 14 | 6 | 231 | 32 | 25.31 | 231 | 32 | 24.59 | 0.2904 | 0.72 |
| 14 | 8 | 284 | 20 | 12.64 | 284 | 20 | 11.53 | 0.4607 | - 1.11 |
| 14 | 11 | 341 | 4 | 11.63 | 341 | 1 | 11.37 | 0.2141 | 0.26 |
| 15 | 4 | 207 | 42 | 24.54 | 207 | 42 | 25.42 | 0.5550 | -0.88 |
| 15 | 5 | 257 | 44 | 42.41 | 257 | 44 | 42.74 | 0.4187 | -0.33 |
| 15 | 6 | 17 | 50 | 53.63 | 17 | 50 | 54.29 | 0.9118 | -0.66 |
| 16 | 5 | 194 | 6 | 54.60 | 194 | 6 | 55.67 | 0.3009 | -1.07 |
| 16 | 6 | 95 | 31 | 21.62 | 95 | 31 | 23.03 | 0.3135 | -1.41 |
| 16 | 8 | 41 | 24 | 51.23 | 4 - | 24 | 52.00 | 0.1907 | 6.77 |
| 16 | 7 | 317 | 36 | 22.62 | 317 | 36 | 23.64 | 0.1916 | -1.02 |
| 17 | 5 | 149 | 36 | 17.34 | 149 | 36 | 48.91 | 0.7781 | -1.57 |
| 17 | 3 | 209 | 32 | 9.51 | 209 | 32 | 9.56 | 0.3882 | -0.05 |
| 17 | 18 | 275 | 15 | 46.63 | 275 | 15 | 46.37 | 0.3139 | -0.24 |
| 17 | 7 | 352 | 11 | 25.96 | 352 | 11 | 27.53 | 0.7048 | -1.57 |
| 18 | 20 | 186 | 37 | 34.51 | 186 | 37 | 34.04 | 0.4563 | 0.47 |
| 18 | 7 | 52 | 19 | 28.91 | 52 | 19 | 28.07 | 0.2430 | 0.84 |
| 18 | 17 | 95 | 15 | 46.03 | 95 | 15 | 46.37 | 0.3139 | -0.84 |
| 18 | 5 | 116 | 21 | 25.06 | 116 | 21 | 26.30 | 0.1610 | -1.24 |
| 19 | 26 | 222 | 47 | 24.01 | 222 | 47 | 23.85 | 0.4038 | 0.16 |
| 19 | 24 | 143 | 18 | 7.51 | 143 | 18 | 6.52 | 0.2385 | 0.99 |
| 19 | 3 | 105 | 26 | 4.12 | 105 | 26 | 5.22 | 0.3120 • | -1.10 |
| 19 | 20 | 78 | 16 | 29.43 | 78 | 16 | 30.39 | 0.6170 | -1.46 |
| 20 | 21 | 108 | 30 | 23.41 | 108 | 30 | 25.27 | 0.7392 | -1.86 |
| 20 | 18 | 6 | 37 | 34.92 | 6 | 37 | 34.04 | 0.4563 | 0.88 |
| 20 | 19 | 258 | 16 | 29.64 | 258 | 16 | 30.89 | 0.6170 | -1.25 |
| 21 | 3 | 144 | 36 | 27.98 | 144 | 36 | 32.04 | 0.5453 | -4.06 |
| 21 | 20 | 288 | 30 | 23.42 | 288 | 30 | 25.27 | 0.7392 | -1.85 |
| 21 | 7 | 28 | 17 | 39.99 | 28 | 17 | 38.72 | 0.1320 | 1.27 |
| 22 | 2 | 186 | 46 | 39.33 | 186 | 46 | 36.63 | 0.5274 | 2.70 |
| 22 | 23 | 120 | 5 | 28.54 | 120 | 5 | 30.70 | 0.3575 | -2.16 |
| 22 | 5 | 33 | 37 | 5.13 | 33 | 37 | 5.00 | 0.3600 | 0.13 |
| 22 | 3 | 321 | 36 | 42.00 | 321 | 36 | 41.03 | 0.5066 | 0.97 |

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| 23 | 2 | 240 | 59 | 50.20 | 240 | 59 | 49.60 | 0.3981 | 0.60 |
|----|----|-----|----|-------|-----|----|-------|--------|-------|
| 23 | 4 | 19 | 32 | 28.15 | 19 | 32 | 28.95 | 0.5831 | -0.80 |
| 23 | 22 | 300 | 5 | 28.42 | 300 | 5 | 30.70 | 0.3575 | -2.28 |
| 24 | 2 | 125 | 26 | 21.12 | 125 | 26 | 24.75 | 0.3119 | -3.63 |
| 24 | 3 | 26 | 35 | 49.90 | 26 | 35 | 47.86 | 0.2595 | 2.04 |
| 24 | 19 | 323 | 18 | 7.51 | 323 | 18 | 6.52 | 0.2385 | 0.99 |
| 24 | 26 | 277 | 8 | 39.00 | 277 | 8 | 39.11 | 0.2372 | -0.11 |
| 24 | 25 | 258 | 47 | 39.42 | 258 | 47 | 39.25 | 0.3804 | 0.17 |
| 25 | 1 | 275 | 18 | 29.72 | 275 | 18 | 25.71 | 0.3643 | 4.01 |
| 25 | 26 | 310 | 31 | 10.60 | 310 | 31 | 11.62 | 0.4808 | -1.02 |
| 25 | 24 | 78 | 47 | 38.42 | 78 | 47 | 39.25 | 0.3804 | -0.83 |
| 26 | 1 | 246 | 43 | 54.13 | 246 | 43 | 53.63 | 0.4812 | 0.50 |
| 26 | 25 | 130 | 31 | 11.12 | 130 | 31 | 11.62 | 0.4808 | -0.50 |
| 26 | 24 | 97 | 8 | 39.56 | 97 | 8 | 39.11 | 0.2372 | 0.45 |
| 26 | 19 | 42 | 47 | 24.43 | 42 | 47 | 23.85 | 0.4038 | 0.58 |

APPENDIX B.4.2: Results of the first level simulated network densification using

dynamic approach

SECOND ORDER SIMULATED NETWORK ADJUSTMENT (DYNAMIC APPROACH)

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-4-1

ITERATION = 2 '/UW= 1.183034

RESULTS

| DISTANCE : | TRACE1= | 9.000 | ETWE1= | 6.735 | VC1= | 0.754 |
|--------------|----------|--------|--------|--------|------|-------|
| DIRECTIONS : | TRACE2= | 18.000 | ETWE2= | 78.488 | VC2= | 4.360 |
| RESTRICTIONS | :TRACE3= | 0.000 | ETWE3= | 15.085 | VC3= | 2.514 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| | | | | | 24 |
|----|---|---------------|---------------|---------|-----------|
| RA | Y | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
| 1 | 4 | 200.0600 | 199.6296 | 0.0062 | 0.4304 |
| 1 | 6 | 200.0400 | 200.0911 | 0.0063 | -0.0511 |
| 2 | 4 | 200.0800 | 200.2017 | 0.0063 | -0.1217 |
| 2 | 5 | 199.9800 | 200.5273 | 0.0063 | -0.5473 |
| 3 | 5 | 200.0300 | 199.4049 | 0.0062 | 0.6251 |
| 3 | 6 | 199.9300 | 199.8980 | 0.0063 | 0.0320 |
| 4 | 5 | 200.0200 | 199.9965 | 0.0055 | 0.0235 |
| 4 | 6 | 200.0900 | 199.2806 | 0.0055 | 0.8094 |
| 5 | 6 | 199.9200 | 199.5369 | 0.0055 | 0.3831 |

ADJUSTED DIRECTIONS

| RAY | | OBSEF | VED- | DIRECT | ADJ | USTED | -DIRECT | STD-ERR | RESIDUALS(" |
|-----|---|-------|------|--------|-----|-------|---------|---------|-------------|
| 1 | 4 | 30 | 0 | 0.00 | 29 | 59 | 59.30 | 4.0128 | 0.70 |
| 1 | 6 | 90 | 0 | 10.61 | 90 | 0 | 10.36 | 3.9495 | 0.25 |
| 2 | 4 | 209 | 59 | 53.01 | 209 | 59 | 55.42 | 4.0110 | -2.41 |
| 2 | 5 | 150 | 0 | 4.99 | 150 | 0 У | 3.38 | 4.0104 | 1.61 |
| 3 | 5 | 329 | 59 | 54.99 | 329 | 59 | 57.44 | 4.0139 | -2.45 |
| 3 | 6 | 270 | 0 | 3.01 | 270 | 0 | 0.48 | 3.9508 | 2.53 |
| 4 | 1 | 210 | 0 | 0.00 | 209 | 59 | 59.30 | 4.0128 | 0.70 |

| 4 | 2 | 30 | 0 | 7.00 | 30 | 0 | 8.01 | 4.0110 | -1.01 |
|---|---|-----|----|-------|-----|----|-------|--------|-------|
| 4 | 5 | 89 | 59 | 52.62 | 89 | 59 | 53.21 | 4.8832 | -0.59 |
| 4 | 6 | 150 | 0 | 5.42 | 150 | 0 | 5.02 | 4.8832 | 6.40 |
| 5 | 2 | 329 | 59 | 50.90 | 329 | 59 | 50.70 | 4.0104 | 0.20 |
| 5 | 4 | 270 | 0 | 4.37 | 270 | 0 | 3.79 | 4.8832 | 0.58 |
| 5 | 6 | 209 | 59 | 58.02 | 209 | 59 | 58.45 | 4.8832 | -0.43 |
| 5 | 3 | 150 | 0 | 13.96 | 150 | 0 | 14.52 | 4.0139 | -0.56 |
| 6 | 1 | 270 | 0 | 0.00 | 270 | 0 | 0.82 | 3.9495 | -0.82 |
| 6 | 4 | 329 | 59 | 57.71 | 329 | 59 | 58.09 | 4.8832 | -0.38 |
| 6 | 5 | 30 | 0 | 6.43 | 30 | 0 | 6.02 | 4.8832 | 0.41 |
| 6 | 3 | 89 | 59 | 54.98 | 89 | 59 | 53.25 | 3.9508 | 1.73 |
| | | | | | | | | | |

APPENDIX B.4.3: Results of the second level real network densification using dynamic

approach

THIRD ORDER REAL NETWORK ADJUSTMENT (DYNAMIC APPROACH)

ITERATION = 3 VUW= 1.062579

RESULTS

| DISTANCE | : | TRACE1= | 30.000 | ETWE1= | 53.927 |
|------------|---|---------|--------|--------|--------|
| DIRECTIONS | : | TRACE2= | 50.000 | ETWE2= | 88.962 |

ADJUSTED OBSERVATIONS

| RAY | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|-------|---------------|---------------|---------|-----------|
| 27 26 | 14773.890 | 147-3.879 | 0.0179 | 0.011 |
| 27 28 | 9653.420 | 9653.421 | 0.0145 | -0.001 |
| 28 29 | 13934.030 | 13933.995 | 0.0158 | 0.035 |
| 28 24 | 17550.110 | 17550.148 | 0.0168 | 70.038 |
| 29 3 | 14026.280 | 14026.222 | 0.0157 | 0.058 |
| 29 24 | 7500.930 | 7500.959 | 0.0127 | 0.021 |
| 30 22 | 20765.540 | 20768.531 | 0.0223 | 0.009 |
| 30 23 | 7148.220 | 7143.226 | 0.0128 | -0.006 |
| 31 4 | 10861.010 | 10861.005 | 0.0151 | 0.005 |
| 31 5 | 18725.550 | 18725.556 | 0.0183 | -0.006 |
| 32 3 | 12954.160 | 12954.184 | 0.0159 | -0.024 |
| 32 21 | 14309.080 | 14309.040 | 0.0169 | 0.040 |
| 33 5 | 6615.690 | 6615.679 | 0.0121 | 0.011 |
| 33 4 | 9616.290 | 9616.293 | 0.0134 | -0.003 |
| 34 18 | 6763.580 | 6763.577 | 0.0121 | 0.003 |
| 34 21 | 10493.270 | 10493.284 | 0.0134 | -0.014 |
| 34 20 | 10463.230 | 10463.209 | 0.0138 | 0.021 |
| 35 16 | 7137.310 | 7137.816 | 0.0120 | -0.006 |
| 35 17 | 7795.220 | 7795.211 | 0.0126 | 0.009 |
| 36 7 | 13557.220 | 13557.203 | 0.0161 | 0.017 |
| 36 18 | 11414.360 | 11414.346 | 0.0150 | 0.014 |
| 37 35 | 10445.030 | 10445.020 | 0.0131 | 0.010 |
| 37 17 | 7476.300 | v 7476.301 | 0.0124 | -0.001 |
| 37 7 | 11935.450 | 11935.436 | 0.0143 | 0.014 |
| 38 8 | 15218.390 | 15218.143 | 0.0141 | -0.053 |
| 38 16 | 13176.150 | 13176.160 | 0.0164 | -0.010 |

| 38 | 7 | | 147 | 52.400 | | 14752 | 2.441 | 0.0149 | -0.041 |
|-----|-----|--------|----------|---------|-----|----------|---------|---------|--------------|
| 39 | 14 | | 171 | 56.360 | | 17156 | 5.362 | 0.0199 | -0.002 |
| 40 | 11 | | 123 | 85.920 | | 12385 | 5.940 | 0.0162 | -0.020 |
| 41 | 13 | | 173 | 34.620 | | 17334 | 1.624 | 0.0208 | -0.064 |
| | | | | | | 2.00 | | | |
| | A | JUSTED | DIR | ECTIONS | | | | | |
| | _ | | | | | | | | |
| R | ΑY | OBSER | VED-I | DIRECT | ADJ | USTED- | -DIRECT | STD-ERR | RESIDUALS(") |
| 27 | 26 | 232 | 51 | 31.26 | 232 | 51 | 31.51 | 0.5194 | -0.25 |
| 27 | 19 | 28 | 38 | 17.97 | 28 | 38 | 18.16 | 0.6793 | -0.19 |
| 27 | 28 | 149 | 41 | 47 26 | 149 | 4 1 | 47.52 | 0.5748 | -0.26 |
| 28 | 27 | 320 | 11 | 49 25 | 329 | 41 | 47 52 | 0 5748 | 1 73 |
| 20 | 20 | 01 | 31 | 28 80 | 81 | 31 | 29 97 | 0 4782 | -1 08 |
| 20 | 23 | 105 | 54 | 20.09 | 105 | 50 | 1 36 | 0.4050 | 0.00 |
| 20 | 24 | 105 | 50 | 4.40 | 105 | 50 | 4.50 | 0.4050 | 0.09 |
| 28 | 25 | 214 | 2 | 52.29 | 214 | 2 | 52.80 | 0.3963 | -0.51 |
| 29 | 3 | 51 | 9 | 34.82 | 51 | 9 | 33.26 | 0.3468 | 1.56 |
| 29 | 24 | 155 | 35 | 6.04 | 155 | 35 | 8.85 | 0.5441 | -2.81 |
| 29 | 28 | 261 | 34 | 28.99 | 261 | 34 | 29.97 | 0.4782 | -0.98 |
| 30 | 22 | 285 | 27 | 41.43 | 285 | 27 | 40.62 | 0.4137 | 0.81 |
| 30 | 4 | 352 | 16 | 43.10 | 352 | 16 | 41.91 | 0.4817 | 1.19 |
| 30 | 23 | 252 | 53 | 6.97 | 252 | 53 | 6.79 | 0.9712 | 0.18 |
| 31 | 4 | 58 | 16 | 33.02 | 58 | 16 | 31.91 | 0.5273 | 1.11 |
| 31 | 22 | 2.62 | 44 | -3.89 | 262 | 44 | 43.05 | 0.6076 | 0.84 |
| 31 | 5 | 11 | 53 | 0 49 | 11 | 52 | 59.64 | 0 3023 | 0.85 |
| 32 | 5 | 86 | 39 | - 3 99 | 86 | 39 | 14 45 | 0 4782 | -0.46 |
| 32 | 2 | 210 | 27 | -2.46 | 219 | 27 | 15 75 | 0.4028 | 2 71 |
| 22 | 21 | 212 | <u> </u> | 00 | 263 | <u> </u> | 41 40 | 0.4920 | 2.71 |
| 32 | 41 | 203 | 41 | 04 | 205 | 4 T | 41.42 | 0.4240 | 0.40 |
| 32 | 1/ | 20 | 2 | 9.29 | 20 | 2 | 11.98 | 0.4971 | -2.69 |
| 33 | - | 297 | 4 | 97 | 297 | 4 | 1.28 | 0.5525 | 0.69 |
| 33 | 15 | 52 | 8 | -5.69 | 52 | 8 | 48.52 | 0.6025 | -1.83 |
| 33 | 4 | 183 | 1 | E9.52 | 183 | 1 | 56.93 | 0.3939 | 2.59 |
| 34 | 18 | 329 | 7 | 12.99 | 329 | 7 | 14.29 | 0.7264 | -1.30 |
| 34 | 17 | 77 | 42 | 3.25 | 77 | 42 | 3.09 | 0.2595 | 0.16 |
| 34 | 21 | 186 | 24 | E2.69 | 186 | 24 | 53.19 | 0.5696 | -0.50 |
| 34 | 20 | 209 | 48 | 10.99 | 209 | 48 | 9.32 | 0.5708 | 1.67 |
| 35 | 16 | 32 | 10 | 16.87 | 32 | 10 | 19.06 | 0.6321 | -2.19 |
| 35 | 5 | 178 | 45 | 49 | 178 | 45 | 7.29 | 0.5191 | AN 0.20 |
| 35 | 17 | 298 | 10 | 32.64 | 298 | 10 | 32.12 | 0.4987 | 0.52 |
| 36 | 12 | 32 | 44 | 39.26 | 32 | 44 | 40.25 | 0.4051 | -0.99 |
| 36 | 7 | 67 | 59 | ÷ 55 | 67 | 59 | 4 96 | 0 5233 | 1 59 |
| 36 | 1.8 | 213 | 37 | 27 21 | 213 | 37 | 31 53 | 0 6435 | -1 32 |
| 37 | 16 | 120 | 4.0 | 1 50 | 120 | 4.0 | 10 11 | 0 1999 | 1 30 |
| 37 | 35 | 163 | 45 | 31 30 | 163 | .15 | 31 00 | 0.4504 | -1 60 |
| 27 | 17 | 211 | 50 | | 211 | 50 | 10.26 | 0.4004 | -1.00 |
| 27 | ± / | 211 | 35 | 2 04 | 320 | 36 | 40.20 | 0.3300 | 1.00 |
| 37 | 6 | 328 | 06 | 5.94 | 323 | 20 | 9.01 | 0.4195 | 0.93 |
| 38 | 8 | 70 | 1 | DI | 107 | 12 | 11.05 | 0.3033 | 1.46 |
| 38 | 16 | 18/ | 43 | 82 | 187 | 43 | 13.48 | 0.3404 | 1.34 |
| 38 | 1 | 274 | 20 | 2.98 | 2/4 | 20 | 38.71 | 0.3035 | -0.73 |
| 38 | 13 | 346 | 41 | 53.56 | 346 | 41 | 53.77 | 0.7167 | -0.21 |
| 39 | 8 | 359 | 53 | ē.52 | 359 | 53 | 6.77 | 0.5605 | -0.25 |
| 39 | 14 | 72 | 48 | 16.88 | 72 | 48 | 16.77 | 0.8192 | 0.11 |
| 39 | 6 | 195 | 45 | 55.94 | 195 | 45 | 58.97 | 0.6886 | -0.03 |
| 40 | 11 | 0 | 27 | 45.30 | 0 | 27 | 46.11 | 0.7784 | -0.81 |
| 40 | 14 | 140 | 45 | 14.38 | 140 | 45 | 12.80 | 0.7026 | 1.58 |
| 40 | 8 | 240 | 29 | 37.98 | 240 | 29 | 41.40 | 0.5655 | -3.42 |
| 41 | 10 | 293 | 52 | 37.34 | 293 | 52 | 36.74 | 0.7046 | 0 60 |
| 41 | 11 | 64 | 34 | 5.77 | 64 | 34 | 8,42 | 0.8222 | 0.35 |
| 41 | 12 | 244 | 2 | 51.24 | 244 | 2 | 51.36 | 0 6000 | _0 12 |
| 2 1 | | 633 | - | | | - | | 0.0000 | 0.14 |

APPENDIX B.4.4: Results of the second level simulated network densification using

dynamic approach

THIRD ORDER SIMULATED NETWORK ADJUSTMENT (DYNAMIC APPROACH)

ITERATION = 2 VUW= 1.090861

RESULTS

| DISTANCE : | TRACE1= | 30.000 | ETWE1= | 8.554 | VC1= | 0.285 |
|--------------|----------|--------|--------|--------|------|-------|
| DIRECTIONS : | TRACE2= | 60.000 | ETWE2= | 28.379 | VC2= | 0.473 |
| RESTRICTIONS | :TRACE3= | 0.000 | ETWE3= | 38.442 | VC3= | 9.870 |

ADJUSTED OBSERVATIONS

| RAY | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|-------|---------------------|-----------------|----------|-----------|
| 1 7 | 100.0400 | 99.9420 | 0.0036 | 0.0980 |
| 1 8 | 100.3600 | 99.9820 | 0.0036 | 0.0780 |
| 2 10 | 100.0300 | 99.9156 | 0.0037 | 0.1644 |
| 2 11 | 99.9800 | 99.8815 | 0.0037 | 0.0985 |
| 3 13 | 100.0300 | 100.0448 | 0.0036 | -0.0145 |
| 3 14 | 99.9300 | 100.0291 | 0.0036 | -0.0991 |
| 4 8 | 100.0200 | 99.7018 | 0.0033 | 0.3182 |
| 4 9 | 100.0400 | 99.3606 | 0.0026 | 0.6791 |
| 4 10 | 100.0300 | 100.4194 | 0.0033 | -0.3894 |
| 4 12 | 99.9700 | 99.7195 | 0.0026 | 0.2505 |
| 5 11 | 99.3900 | 100.6928 | 0.0033 | -0.8028 |
| 5 12 | 100.0800 | 100.3108 | 0.0026 | -0.2308 |
| 5 13 | 99.9900 | 99.4188 | 0.0033 | 0.5712 |
| 5 15 | 99.9400 | 99.6754 | 0.0026 | 0.2640 |
| 6 7 | 99.9800 | 100.2228 | 0.0034 | -0.2428 |
| 6 9 | 99.9300 | 99.9318 | 0.0026 | -0,*0018 |
| 6 14 | 100.0300 | 99.8669 | 0.0034 | 0.1631 |
| 6 15 | 100.0200 | 99.7513 | 0.0026 | 0.2687 |
| 79 | 99.9700 | 100.0621 | 0.0028 | -0.0921 |
| 8 7 | 100.0000 | 100.0385 | 0.0029 | -0.0325 |
| 8 9 | 100.0600 | 100.0298 | 0.0028 | 0.0312 |
| 9 12 | 100.0400 | 100.0856 | 0.0026 | -0.0455 |
| 9 15 | 100.0100 | 100.0309 | 0.0026 | -0.0203 |
| 10 11 | 100.0000 | 99.9924 | 0.0029 | 0.0076 |
| 12 10 | 100.0600 | 99.9873 | 0.0028 | 0.0727 |
| 12 11 | 99.9800 | 100.0004 | 0.0028 | -0.0204 |
| 12 15 | 99.9700 | 100.0685 | 0.0026 | -0.0986 |
| 13 14 | 99.9600 | 100.0799 | 0.0029 * | -0.1193 |
| 15 14 | 100.0500 | 100.0938 | 0.0028 | -0.0438 |
| 15 13 | 100.0300 | 100.0728 | 0.0028 | -0.0425 |
| : | ADJUSTED DIRECTIONS | | | |
| RAY | OBSERVED-DIRECT | ADJUSTED-DIRECT | STD-ERR | RESTDUZTS |
| 1 8 | 29 59 54.90 | 29 59 43.41 | 4.4529 | 11 49 |
| 1 7 | 89 59 53.00 | 89 59 56.27 | 4.3684 | -3.27 |
| 2 10 | 209 59 57.01 | 210 0 9.98 | 4.4158 | -12 97 |
| 2 11 | 149 59 58.00 | 149 59 54.43 | 4.4158 | 3.57 |
| 2 1 2 | 330 0 0.00 | 330 0 3 71 | 4 4525 | _ 2 |

| 3 | 14 | 269 | 59 | 52.01 | 269 | 59 | 50.66 | 4.3680 | 1.35 |
|----|----|-----|-----|-------|-----|----|-------|----------|--------|
| 4 | 8 | 209 | 59 | 53.00 | 210 | 0 | 47.91 | 4.2665 | -54.91 |
| 4 | 9 | 150 | 0 | 4.00 | 150 | 0 | 6.62 | 4.3473 | -2.62 |
| 4 | 12 | 90 | 0 | 2.62 | 89 | 58 | 56.13 | 4.3623 | 66.49 |
| 4 | 10 | 30 | 0 | 8.42 | 29 | 59 | 15.94 | 4.2518 | 52.49 |
| 5 | 11 | 330 | 0 | 2.90 | 330 | 0 | 6.43 | 4.2509 | -3.53 |
| 5 | 12 | 269 | 59 | 54.37 | 270 | 0 | 56.36 | 4.3586 | -61.99 |
| 5 | 15 | 210 | 0 | 5.02 | 210 | 0 | 55.61 | 4.3462 | -50.59 |
| 5 | 13 | 150 | 0 | 3.96 | 149 | 59 | 56.03 | 4.2688 | 7.93 |
| 6 | 7 | 270 | 0 | 9.00 | 269 | 59 | 45.32 | 4.1959 | 23.68 |
| 6 | 9 | 329 | 59 | 54.71 | 329 | 59 | 29.98 | 4.3595 | 24.73 |
| 6 | 15 | 30 | 0 | 6.43 | 29 | 59 | 57.47 | 4.3612 | 8.96 |
| 6 | 14 | 90 | 0 | 1.98 | 90 | 0 | 29.18 | 4.1981 | -27.20 |
| 8 | 1 | 210 | 0 | 0.00 | 209 | 59 | 48.51 | 4.4529 | 11.49 |
| 8 | 7 | 150 | 0 | 0.10 | 150 | 0 | 2.71 | 4.6045 | -2.61 |
| 8 | 9 | 90 | 0 | 0.10 | 89 | 59 | 56.08 | 4.6028 | 4.02 |
| 8 | 4 | 29 | 59 | 57.90 | 30 | 0 | 52.81 | 4.2665 | -54.91 |
| 4 | 1 | 270 | 0 | 0.00 | 270 | 0 | 3.21 | 4.3684 | -3.27 |
| 4 | 8 | 330 | 0 | 10.00 | 330 | 50 | 12.61 | 4.6045 | -2.61 |
| 1 | 9 | 29 | 59 | 51.00 | 29 | 59 | 48.17 | 4.6037 | 2.83 |
| 1 | Ó | 220 | 29 | 57.00 | 220 | 29 | 33.32 | 4.1909 | 23.63 |
| 0 | 4 | 330 | = 0 | 53.00 | 330 | 50 | 2.02 | 4.34/3 | -2.62 |
| 2 | 15 | 29 | 59 | 53.00 | 29 | 59 | 40.00 | 4.1000 | 4.20 |
| 9 | 10 | 150 | 29 | 10.00 | 1/0 | 59 | 16 17 | 4.1929 | 1.80 |
| 9 | 7 | 200 | 50 | == 00 | 200 | 50 | 56 17 | 4.5555 | 24.73 |
| 9 | 0 | 209 | 79 | 59.00 | 209 | 0 | 0 98 | 4.6029 | 2.03 |
| 10 | q | 210 | 0 | 2.00 | 209 | 59 | 55 80 | 4.1858 | 4.02 |
| 12 | 4 | 269 | 5.9 | 52.00 | 269 | 58 | 45 51 | 4.1000 | 66 / 9 |
| 12 | 10 | 330 | 5 | 22.00 | 330 | 0 | 1 51 | 4 6014 | -1 51 |
| 12 | 11 | 30 | õ | 1.00 | 30 | 0 | 1.26 | 4.6028 | -1 26 |
| 12 | 5 | 90 | õ | 1.00 | 90 | 1 | 1.99 | 4.3586 | -61 99 |
| 12 | 15 | 149 | 59 | 55.00 | 150 | 0 | 1.69 | 4.1860 | -6 69 |
| 10 | 2 | 29 | 59 | 53.00 | 30 | 0 | 7.97 | 4.4158 | +12.97 |
| 10 | 4 | 209 | 59 | 57.00 | 209 | 59 | 4.52 | 4.2518 | 52.48 |
| 10 | 12 | 149 | 59 | 50.00 | 149 | 59 | 51.51 | 4.6014 | -1.51 |
| 10 | 11 | 90 | С | 5.00 | 90 | 0 | 4.05 | 4.6030 | .0.95 |
| 11 | 2 | 330 | 0 | 1.00 | 329 | 59 | 57.43 | 4.4158 | 13.5 |
| 11 | 10 | 269 | 59 | 54.00 | 269 | 59 | 53.05 | 4.6030 | 0.95 |
| 11 | 12 | 209 | 59 | 54.00 | 209 | 59 | 55.26 | 4.6028 | -1.26 |
| 11 | 5 | 150 | 0 | 1.00 | 150 | 0 | 4.53 | 4.2509 | -3.53 |
| 15 | 5 | 29 | 59 | 50.00 | 30 | 0 | 40.59 | 4.3462 | -50.59 |
| 15 | 12 | 330 | 0 | 2.00 | 330 | 0 | 8.69 | 4.1860 | -6.69 |
| 15 | 9 | 269 | 59 | 55.90 | 269 | 59 | 54.10 | 4.1929 | 1.80 |
| 15 | 6 | 210 | 0 | 2.90 | 209 | 59 | 53.94 | 4.3612 | 8.96 |
| 15 | 14 | 150 | 0 | 4.00 | 150 | 0 | 5.98 | 4.6034 | -1.98 |
| 15 | 13 | 89 | 59 | 50.10 | 39 | 59 | 52.83 | 4.6040 | -2.73 |
| 13 | 5 | 330 | 0 | 00 | 329 | 59 | 59.07 | 4.2688 | 7.93 |
| 13 | 15 | 269 | 59 | 58.00 | 270 | 0 | 0.73 | 4.6040 | -2.73 |
| 13 | 14 | 209 | 59 | 58.00 | 209 | 59 | 56.52 | 4.6042 • | 1.48 |
| 13 | 3 | 149 | 59 | 53.00 | 149 | 59 | 56.71 | 4.4525 | -3.71 |
| 14 | 3 | 90 | 0 | 2.50 | 90 | 0 | 0.65 | 4.3680 | 1.35 |
| 14 | 6 | 270 | 0 | 53.00 | 270 | 0 | 27.20 | 4.1981 | -27.20 |
| 14 | 15 | 329 | 59 | 56.00 | 329 | 59 | 59.98 | 4.6034 | -1.98 |
| 14 | 13 | 29 | SA | 50.10 | 29 | 29 | 48.62 | 4.6042 | 1.48 |

APPENDIX B.5: RESULTS FOR STATIC DENSIFICATION

APPENDIX B.5.1: Results of the first level real network densification using static

approach

SECOND ORDER REAL NETWORK ADJUSTMENT (STATIC APPROACH)

ITERATION = 0 VUW= 1.06678

RESULTS

| DISTANCE | : | TRACE1= | 30.000 | ETWE1= | 14.178 |
|------------|---|---------|--------|--------|--------|
| DIRECTIONS | : | TRACE2= | 52.000 | ETWE2= | 7.066 |

ADJUSTED OBSERVATIONS

| R | ΑY | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|---------|---------------|-----------------|---------|---------------|
| 12 | 7 | 11392.335 | 11392.346 | 0.0142 | -0.0110 |
| 12 | 9 | 12369.293 | 12369.303 | 0.0176 | -0.0096 |
| 13 | 9 | 13814.687 | 13814.686 | 0.0358 | 0.0006 |
| 14 | 6 | 24623.681 | 24623.700 | 0.0246 | -0.0191 |
| 14 | 8 | 16935.563 | 16935.563 | 0.0187 | -0.0002 |
| 15 | 6 | 10683.383 | 10683.379 | 0.0213 | 0.0040 |
| 16 | 5 | 14837.980 | 14837.962 | 0.0167 | 0.0181 |
| 16 | 6 | 13269.516 | 13269.545 | 0.0168 | -0.0288 |
| 16 | 8 | 24310.634 | 24310.559 | 0.0159 | 0.0755 |
| 17 | 7 | 16690.070 | 16690.075 | 0.0203 | -0.0048 |
| 18 | 20 | 14984.326 | 14984.286 | 0.0264 | 0.0398 |
| 18 | 7 | 23865.386 | 23865.811 | 0.0220 | 0.0753 |
| 18 | 5 | 31483.464 | 31483.550 | 0.0224 | -0.0858 |
| 19 | 26 | 24790.315 | 24790.377 | 0.0396 | -0,0622 |
| 19 | 20 | 14808.001 | 14808.023 | 0.0336 | -0.0217 |
| 20 | 21 | 4247.690 | 4247.702 | 0.0281 | '-0.0117 |
| 21 | 3 | 10340.648 | 10340.606 | 0.0195 | 0.0417 |
| 21 | 7 | 35000.587 | 35000.682 | 0.0179 | -0.0953 |
| 22 | 2 | 16116.390 | 16116.937 | 0.0201 | -0.0468 |
| 22 | 23 | 15238.942 | 15238.938 | 0.0420 | 0.0040 |
| 22 | 5 | 23394.975 | 23394.972 | 0.0237 | 0.0031 |
| 23 | 4 | 15396.022 | 15396.064 | 0.0222 | -0.0418 |
| 24 | 2 | 15823.986 | 15824.017 | 0.0191 | -0.0313 |
| 24 | 3 | 17476.302 | 17476.267 | 0.0188 | 0.0351 |
| 24 | 26 | 33794.283 | 33794.472 | 0.0216 | -0.1886 |
| 24 | 25 | 23681.294 | 23681.304 | 0.0237 | -0.0104 |
| 25 | 1 | 25419.370 | 25419.371 | 0.0218 | -0.0005 |
| 25 | 26 | 13552.337 | 13552.322 | 0.0355 | 0.0147 |
| 26 | 1 | 16336.566 | 16336.687 | 0.0228 | -0.1213 |
| 26 | 24 | 33794482 | 33794.472 | 0.0216 | 0.0104 |
| | ACJUSTE | D DIRECTIONS | | | |
| | | | | | |
| R | AY OBSE | RVED-DIRECT | ADJUSTED-DIRECT | STD-ERR | RESIDUALS (") |

| 170 | - | 0202 | | | | | | OID LINN | VERTONATS |
|-----|---------------|------|----|-------|-----|----|-------|----------|-----------|
| 12 | 7 | 169 | 22 | 42.30 | 169 | 22 | 41.65 | 0.4031 | 0.65 |
| 12 | 9 | 37 | 17 | 34.90 | 37 | 17 | 35.87 | 0.3300 | -0.97 |
| 13 | 7 | 233 | 35 | 16.50 | 233 | 35 | 16.17 | 0.5088 | 0.33 |

| 13 | 8 | 106 | 41 | 48.00 | 106 | 41 | 48.45 | 0.3778 | -0.45 |
|-----|----|------|----|-------|-----|----|-------|--------|-------|
| 13 | 9 | 330 | 0 | 20.65 | 330 | 0 | 20.81 | 0.6649 | -0.16 |
| 14 | 6 | 231 | 32 | 25.31 | 231 | 32 | 25.06 | 0.2313 | 0.25 |
| 14 | 8 | 284 | 20 | 12.64 | 284 | 20 | 12.17 | 0.3778 | 0.47 |
| 14 | 11 | 341 | 1 | 11.63 | 341 | 1 | 11.05 | 0.1793 | 0.58 |
| 15 | 4 | 207 | 42 | 24.54 | 207 | 42 | 25.16 | 0.4201 | -0.62 |
| 15 | 5 | 257 | 44 | 42.41 | 257 | 44 | 42.10 | 0.2957 | 0.31 |
| 15 | 6 | 17 | 50 | 53.63 | 17 | 50 | 53.94 | 0.7276 | -0.31 |
| 16 | 5 | 194 | 6 | 54.60 | 194 | 6 | 54.62 | 0.2267 | -0.02 |
| 16 | 6 | 95 | 31 | 21.62 | 95 | 31 | 22.86 | 0.2609 | -1.24 |
| 16 | 8 | 41 | 24 | 51.23 | 41 | 24 | 52.11 | 0.1346 | -0.88 |
| 16 | 7 | 317 | 36 | 22.62 | 317 | 36 | 23.04 | 0.1748 | -0.42 |
| 17 | 5 | 149 | 36 | 47.34 | 149 | 36 | 48.32 | 0.6302 | -0.98 |
| 17 | 3 | 209 | 32 | 9.51 | 209 | 32 | 9.36 | 0.3412 | 0.15 |
| 17 | 18 | 275 | 15 | 46.63 | 275 | 15 | 46.53 | 0.2653 | 0.10 |
| 17 | 7 | 352 | 11 | 25.96 | 352 | 11 | 26.77 | 0.5878 | -0.81 |
| 18 | 20 | 186 | 37 | 34.51 | 186 | 37 | 33.96 | 0.4048 | 0.55 |
| 18 | 7 | 52 | 19 | 28.91 | 52 | 19 | 27.78 | 0.1882 | 1.13 |
| 18 | 17 | 95 | 15 | 46.03 | 95 | 15 | 46.53 | 0.2653 | -0.50 |
| 18 | 5 | 116 | 21 | 25.06 | 116 | 21 | 25.81 | 0.1422 | -0.75 |
| 19 | 26 | 222 | 47 | 24.01 | 222 | 47 | 24.41 | 0.3199 | -0.40 |
| 19 | 24 | 143 | 18 | 7.51 | 143 | 18 | 6.84 | 0.2460 | 0.67 |
| 19 | 3 | 105 | 26 | 4.12 | 105 | 26 | 5.21 | 0.2889 | -1.09 |
| 19 | 20 | 78 | 16 | 29.43 | 78 | 16 | 31.24 | 0.5363 | -1.81 |
| 20 | 21 | 108 | 30 | 23.41 | 108 | 30 | 25.00 | 1.1370 | -1.59 |
| 20 | 18 | 6 | 37 | 34.92 | 6 | 37 | 33.96 | 0.4048 | 0.96 |
| 20 | 19 | 258 | 16 | 29.64 | 258 | 16 | 31.24 | 0.5363 | -1.60 |
| 21 | 3 | 144 | 36 | 27.98 | 144 | 36 | 31.21 | 0.4144 | -3.23 |
| 21 | 20 | 288 | 30 | 23.42 | 288 | 30 | 25.00 | 1.1370 | -1.58 |
| 21 | 7 | 28 | 17 | 39.99 | 28 | 17 | 38.55 | 0.1201 | 1.44 |
| 22 | 2 | 186 | 46 | 39.33 | 186 | 46 | 37.60 | 0.4339 | 1.73 |
| 22 | 23 | 120 | 5 | 28.54 | 120 | 5 | 30.93 | 0.4271 | -2.39 |
| 22 | 5 | 33 | 37 | 5.13 | 33 | 37 | 5.28 | 0.2575 | -0.15 |
| 22 | 3 | 321 | 36 | 42.00 | 321 | 36 | 41.08 | 0.5268 | 0.92 |
| 23 | 2 | 240 | 59 | 50.20 | 240 | 59 | 50.21 | 0.3041 | -0.01 |
| 23 | 4 | 19 | 32 | 28.15 | 19 | 32 | 28.69 | 0.4510 | -0.54 |
| 23 | 22 | 300. | 5 | 28.42 | 300 | 5 | 30.93 | 0.4271 | -2.51 |
| 24 | 2 | 125 | 26 | 21.12 | 125 | 26 | 24.48 | 0.2527 | 43.36 |
| 24 | 3 | 26 | 35 | 49.90 | 26 | 35 | 49.11 | 0.2086 | 0.79 |
| 2.4 | 19 | 323 | 18 | 7.51 | 323 | 18 | 6.84 | 0.2460 | 0.67 |
| 24 | 26 | 277 | 8 | 39.00 | 277 | 8 | 39.38 | 0.2080 | -0.38 |
| 24 | 25 | 258 | 47 | 39.42 | 258 | 47 | 39.47 | 0.3429 | -0.05 |
| 25 | 1 | 275 | 18 | 29.72 | 275 | 18 | 26.62 | 0.3234 | 3.10 |
| 25 | 26 | 310 | 31 | 10.60 | 310 | 31 | 11.78 | 0.5933 | -1 18 |
| 25 | 24 | 78 | 47 | 38.42 | 78 | 47 | 39.47 | 0.3429 | -1 05 |
| 26 | 1 | 246 | 43 | 54.13 | 246 | 43 | 54.69 | 0.4107 | -0.56 |
| 26 | 25 | 130 | 31 | 11.12 | 130 | 31 | 11.78 | 0.5933 | -0.66 |
| 2.6 | 24 | 97 | 8 | 39.50 | 97 | 8 | 39.38 | 0.2080 | 0.00 |
| 2.6 | 19 | 42 | 47 | 24.43 | 42 | 47 | 24.41 | 0.3199 | 0.10 |
| | | | | | | | | 4.0222 | 0.02 |

APPENDIX B.5.2: Results of the first level simulated network densification using static

approach

SECOND ORDER SIMULATED NETWORK ADJUSTMENT (STATIC APPROACH)

ITERATION = 2 VUW= 1.093478

RESULTS

| DISTANCE | : | TRACE1= | 9.000 | ETWE1= | | 2.220 | VC1= | 0.247 |
|-------------|----|----------|--------|--------|---|--------|------|--------|
| DIRECTIONS | | TRACE2= | 18.000 | ETWE2= | 1 | 95.819 | VC2= | 10.879 |
| RESTRICTION | IS | :TRACE3= | 0.000 | ETWE3= | | 15.085 | VC3= | 2.514 |

ADJUSTED OBSERVATIONS

ADJUSTED DISTANCES

| RA | Y | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|----|---|---------------|---------------|---------|-----------|
| 1 | 4 | 200.0600 | 200.2937 | 0.0042 | 0.2337 |
| 1 | 6 | 200.0400 | 199.9886 | 0.0042 | -0.0514 |
| 2 | 4 | 200.0800 | 199.9789 | 0.0042 | -0.1011 |
| 2 | 5 | 199.9800 | 199.6440 | 0.0042 | -0.3360 |
| 3 | 5 | 200.0300 | 200.3872 | 0.0042 | 0.3572 |
| 3 | 6 | 199.9300 | 199.9519 | 0.0042 | 0.0219 |
| 4 | 5 | 200.0200 | 200.0067 | 0.0040 | -0.0133 |
| 4 | 6 | 200.0900 | 200.5337 | 0.0040 | 0.4437 |
| 5 | 6 | 199.9200 | 200.1427 | 0.0040 | 0.2227 |

ADJUSTED DIRECTIONS

| RAY | | OBSER | OBSERVED-DIRECT | | | JSTED | -DIRECT | STD-ERR | RESIDUALS (") |
|-----|---|-------|-----------------|-------|-----|-------|---------|---------|---------------|
| 1 | 4 | 30 | 0 | 0.00 | 29 | 59 | 28.74 | 2.6845 | -31.26 |
| 1 | 6 | 90 | 0 | 10.61 | 90 | 0 | 36.15 | 2.6825 | 25.54 |
| 2 | 4 | 209 | 59 | 53.01 | 210 | 0 | 10.57 | 2.6819 | 17.56 |
| 2 | 5 | 150 | 0 | 4.99 | 150 | 0 | 9.60 | 2.6808 | 4.61 |
| 3 | 5 | 329 | 59 | 54.99 | 329 | 59 | 45.20 | 2.6856 | -9.79 |
| 3 | 6 | 270 | 0 | 3.01 | 270 | 0 | 1.52 | 2.6839 | -1.49 |
| 4 | 1 | 210 | 0 | 0.00 | 209 | 59 | 28.74 | 2.6845 | -31.26 |
| 4 | 2 | 30 | 0 | 7.00 | 30 | 0 | 38.55 | 2.6819 | 31.55 |
| 4 | 5 | 89 | 59 | 52.62 | 89 | 59 | 46.43 | 3.7944 | -6.19 |
| 4 | 6 | 150 | 0 | 5.42 | 150 | 0 | 28.26 | 3.7944 | 22.84 |
| 5 | 2 | 329 | 59 | 50.90 | 329 | 59 | 41.42 | 2.6808 | -9.48 |
| 5 | 4 | 270 | 0 | 4.37 | 270 | 0 | 9.93 | 3.7944 | 45.56 |
| 5 | 6 | 209 | 59 | 58.02 | 209 | 59 | 24.86 | 3.7944 | -33.16 |
| 5 | 3 | 150 | 0 | 13.96 | 150 | 0 | 23.14 | 2.6856 | 9.18 |
| 6 | 1 | 270 | 0 | 0.00 | 270 | 0 | 14.93 | 2.6825 | 14.93 |
| 6 | 4 | 329 | 59 | 57.71 | 330 | 0 | 12.84 | 3.7944 | 15.13 |
| 6 | 5 | 30 | 0 | 6.43 | 29 | 59 | 41.68 | 3.7944 | -24.75 |
| 6 | 3 | 89 | 59 | 54.98 | 89 | 59 | 45.46 | 2.6839 | -9.52 |

APPENDIX B.5.3: Results of the second level real network densification using static

approach

THIRD ORDER REAL NETWORK ADJUSTMENT (STATIC APPROACH)

10.0

ITERATION = 3 VUW= 1.032345

RESULTS

| DISTANCE | | TRACE1= | 30.000 | ETWE1= | 4.323 |
|------------|---|---------|--------|--------|--------|
| DIRECTIONS | : | TRACE2= | 50.000 | ETWE2= | 34.100 |

ADJUSTED OBSERVATIONS

| R | AY | 0 | BSER | VED-DIST | A | DJUST | ED-DIST | STD-ERR | RESIDUALS |
|----|-------------|---------|--------|----------|-----|--------|---------|---------|-------------|
| 27 | 26 | | 147 | 73.890 | | 1477 | 3.878 | 0.0147 | 0.0122 |
| 27 | 28 | | 96 | 53.420 | | 965 | 3.417 | 0.0120 | 0.0032 |
| 28 | 29 | | 139 | 34.030 | | 1393 | 4.022 | 0.0128 | 0.0076 |
| 28 | 24 | | 175 | 50 110 | | 1755 | 0 119 | 0 0131 | -0.0093 |
| 29 | 2 | | 110 | 26 280 | | 1/02 | 6 286 | 0.0122 | ~0.0055 |
| 20 | 24 | | 75 | 20.200 | | 7500 | 0.200 | 0.0122 | 0.0000 |
| 29 | 24 | | 10 | 00.900 | | 2070 | 0.900 | 0.0105 | 0.0125 |
| 30 | 22 | | 207 | 68.540 | | 20760 | 8.530 | 0.0137 | 0.0096 |
| 30 | 23 | | /1 | 48.220 | | /14 | 8.223 | 0.0102 | -0.0029 |
| 31 | 4 | | 108 | 61.010 | | 1086 | 1.008 | 0.0126 | 0.0021 |
| 31 | 5 | | 187 | 25.550 | | 1872 | 5.558 | 0.0148 | -0.0076 |
| 32 | 3 | | 129 | 54.160 | | 1295 | 4.162 | 0.0129 | -0.0024 |
| 32 | 21 | | 143 | 09.080 | | 1430 | 9.067 | 0.0135 | 0.0128 |
| 33 | 5 | | 66 | 15.690 | | 661 | 5.692 | 0.0101 | -0.0018 |
| 33 | 4 | | 96 | 16.290 | | 961 | 6.288 | 0.0111 | 0.0024 |
| 34 | 18 | | 67 | 63.580 | | 676 | 3.574 | 0.0094 | 0.0057 |
| 34 | 21 | | 104 | 93.270 | | 10493 | 3.272 | 0.0078 | -0.0019 |
| 34 | 20 | | 104 | 63.230 | | 1046 | 3.221 | 0.0096 | 0.0085 |
| 35 | 16 | | 71 | 37.810 | | 713 | 7.813 | 0.0094 | -0.0026 |
| 35 | 17 | | 77 | 95.220 | | 779 | 5.224 | 0.0094 | -0.0045 |
| 36 | 7 | | 135 | 57 220 | | 1355 | 7 220 | 0 0128 | 0.0003 |
| 36 | 1.9 | | 111 | 11 360 | | 1141 | 1 359 | 0.0120 | 0.0005 |
| 27 | 35 | | 104 | 45 030 | | 10441 | 5 125 | 0.0121 | 0.0008 |
| 27 | 17 | | - TO4- | 40.000 | | 747 | 5.525 | 0.0099 | 0.0045 |
| 27 | 1/ | | 110 | 70.300 | | 1102 | 0.303 | 0.0098 | -0.0048 |
| 37 | / 11935.450 | | | | | 1193: | 0204 | 0.0105 | -0.0039 |
| 38 | 8 | | 152 | 18.090 | | 15218 | 3.390 | 0.0107 | -0.0003 |
| 38 | 16 | | 131 | 76.150 | | 13170 | 6.145 | 0.0136 | 0.0052 |
| 38 | 7 | | 147 | 52.400 | | 1475 | 2.401 | 0.0117 | -0.0014 |
| 39 | 14 | | 171 | 56.360 | | 1715 | 6.360 | 0.0165 | -0.0005 |
| 40 | 11 | | 123 | 85.920 | | 12385 | 5.926 | 0.0135 | -0.0058 |
| 41 | 13 | | 173 | 34.620 | | 17334 | 4.623 | 0.0173 | -0.0029 |
| | | | | | | | | | 1 |
| | AI | DJUSTED | DIR | ECTIONS | | | | | |
| RA | ĄΥ | OBSER | VED- | DIRECT | ADJ | USTED- | -DIRECT | STD-ERR | RESIDUALS " |
| 27 | 26 | 232 | 51 | 31.26 | 232 | 51 | 32.23 | 0.3082 | -0.97 |
| 27 | 19 | 28 | 38 | 17.97 | 28 | 38 | 17.37 | 0.3914 | 0.60 |
| 27 | 28 | 149 | 41 | 47.26 | 149 | 41 | 47.99 | 0.4283 | -0.73 |
| 28 | 27 | 329 | 41 | 49.25 | 329 | 41 | 17.99 | 0.4283 | 1.26 |
| 28 | 29 | 81 | 34 | 28.89 | 81 | 34 | 30.17 | 0.3628 | -1.28 |
| 28 | 24 | 105 | 50 | 4.45 | 105 | 50 | 3.09 | 0.2829 | 1.36 |
| 28 | 25 | 214 | 2 | 52.29 | 214 | 2 | 53.37 | 0.2876 | -1.08 |
| 29 | 3 | 51 | 9 | 34.82 | 51 | 9 | 33.76 | 0.1588 | 1.06 |
| 29 | 24 | 155 | 35 | 6.04 | 155 | 35 | 4.10 | 0.3426 | 1.94 |
| 29 | 28 | 261 | 34 | 28.99 | 261 | 34 | 30.17 | 0.3628 | -1.18 |
| 30 | 22 | 285 | 27 | 41.43 | 285 | 27 | 41.49 | 0.2221 | -0.06 |
| 30 | 4 | 352 | 16 | 43.10 | 352 | 16 | 43.09 | 0.1619 | 0.01 |
| 30 | 23 | 252 | 53 | 6.97 | 252 | 53 | 6 61 | 0.6980 | 0.36 |
| 31 | 4 | 58 | 16 | 33.02 | 58 | 16 | 33 11 | 0 4077 | -0.00 |
| 21 | 22 | 262 | 44 | 43.89 | 262 | 44 | 44 88 | 0 1115 | -0.09 |
| 21 | 64 | 11 | 53 | 0.49 | 11 | 53 | 0 51 | 0.9115 | -0.99 |
| 27 | 5 | 96 | 39 | 13.99 | 86 | 30 | 14 09 | 0.2200 | -0.02 |
| 22 | 2 | 210 | 27 | 48.46 | 219 | 27 | 17 21 | 0.3438 | -0.09 |
| 32 | 21 | 263 | 41 | 41.82 | 263 | 41 | 12 61 | 0.3236 | 1.15 |
| 32 | 21 | 203 | 2 | 9.29 | 200 | 2 | 42.01 | 0.2877 | -0.79 |
| 32 | 1/ | 20 | 6 | 2.60 | 20 | 4 | 9.4/ | 0.2/26 | -0.18 |

| 33 | 5 | 297 | 4 | 1.97 | 297 | 4 | 2.05 | 0.3933 | -0.08 |
|----|----|-----|----|-------|-----|----|-------|--------|-------|
| 33 | 15 | 52 | 8 | 46.69 | 52 | 8 | 46.67 | 0.1951 | 0.02 |
| 33 | 4 | 183 | 1 | 59.52 | 183 | 1 | 59.56 | 0.2517 | -0.04 |
| 34 | 18 | 329 | 7 | 12.99 | 329 | 7 | 14.27 | 0.3760 | -1.28 |
| 34 | 17 | 77 | 42 | 3.25 | 77 | 42 | 2.38 | 0.0898 | 0 87 |
| 34 | 21 | 186 | 24 | 52.69 | 186 | 24 | 53.15 | 0.2632 | -0.46 |
| 34 | 20 | 209 | 48 | 10.99 | 209 | 48 | 10.66 | 0.2399 | 0 33 |
| 35 | 16 | 32 | 10 | 16.87 | 32 | 10 | 15.73 | 0.2716 | 1.14 |
| 35 | 5 | 178 | 45 | 7.49 | 178 | 45 | 8.34 | 0.2387 | -0.85 |
| 35 | 17 | 298 | 10 | 32.64 | 298 | 10 | 31.56 | 0.2486 | 1.08 |
| 36 | 12 | 32 | 44 | 39.26 | 32 | 44 | 40.34 | 0.2562 | -1.08 |
| 36 | 7 | 67 | 59 | 6.55 | 67 | 59 | 5.71 | 0.3618 | 0.84 |
| 36 | 18 | 213 | 37 | 30.21 | 213 | 37 | 30.76 | 0.4360 | -0.55 |
| 37 | 16 | 120 | 40 | 11.50 | 120 | 40 | 10.43 | 0.2560 | 1.07 |
| 37 | 35 | 163 | 45 | 30.30 | 163 | 45 | 31.36 | 0.3108 | -1.06 |
| 37 | 17 | 211 | 53 | 41.82 | 211 | 53 | 42.61 | 0.3473 | -0.79 |
| 37 | 7 | 328 | 36 | 9.94 | 328 | 36 | 8.98 | 0.2082 | 0.96 |
| 38 | 8 | 70 | 7 | 12.51 | 70 | 7 | 11.49 | 0.1968 | 1.02 |
| 38 | 16 | 187 | 43 | 14.82 | 187 | 43 | 14.93 | 0.1859 | -0.11 |
| 38 | 7 | 274 | 20 | 37.98 | 274 | 20 | 38.00 | 0.1922 | -0.02 |
| 38 | 13 | 346 | 41 | 53.56 | 346 | 41 | 53.54 | 0.2132 | 0.02 |
| 39 | 8 | 359 | 53 | 6.52 | 359 | 53 | 6.28 | 0.4145 | 0.24 |
| 39 | 14 | 72 | 48 | 16.88 | 72 | 48 | 17.20 | 0.6559 | -0.32 |
| 39 | 6 | 195 | 45 | 58.94 | 195 | 45 | 58.37 | 0.5528 | 0.57 |
| 40 | 11 | 0 | 27 | 45.30 | 0 | 27 | 45.89 | 0.6312 | -0.59 |
| 40 | 14 | 140 | 45 | 14.38 | 140 | 45 | 13.54 | 0.5297 | 0.84 |
| 40 | 8 | 240 | 29 | 37.98 | 240 | 29 | 39.18 | 0.4464 | -1.20 |
| 41 | 10 | 293 | 52 | 37.34 | 293 | 52 | 36.52 | 0.5004 | 0.82 |
| 41 | 11 | 64 | 34 | 8.77 | 64 | 34 | 8.56 | 0.6518 | 0.21 |
| 41 | 13 | 244 | 2 | 51.24 | 244 | 2 | 51.37 | 0.4213 | -0.13 |

APPENDIX B.5.4: Results of the second level simulated network densification using

static approach

THIRD ORDER SIMULATED NETWORK ADJUSTMENT (STATIC APPROACH)

ITERATION = 2 VUW= 1.0464495

RESULTS

| DISTANCE : | TRACE1= | 30.000 | ETWE1= | 4.591 | VC1= | 0.153 |
|--------------|----------|--------|--------|--------|------|--------|
| DIRECTIONS : | TRACE2= | 60.000 | ETWE2= | 82.517 | VC2= | 9.375 |
| RESTRICTIONS | :TRACE3= | 0.000 | ETWE3= | 30.514 | VC3= | 69.209 |

ADJUSTED OBSERVATIONS

| RAY | OBSERVED-DIST | ADJUSTED-DIST | STD-ERR | RESIDUALS |
|------|---------------|---------------|---------|-----------|
| 1 7 | 100.0400 | 99.8900 | 0.0020 | 0.1500 |
| 1 8 | 100.0600 | 99.9726 | 0.0020 | 0.0874 |
| 2 10 | 100.0800 | 99.8931 | 0.0020 | 0.1869 |
| 2 11 | 99.9800 | 99.8182 | 0.0020 | 0.1618 |
| 3 13 | 100.0300 | 100.0425 | 0.0020 | -0.0125 |
| 3 14 | 99.9300 | 100.0333 | 0.0020 | -0.1033 |

| 4 4 4 4 5 5 5 5 6 6 6 6 7 8 8 9 9 0 2 2 2 3 5 1 5 1 5 1 5 | 8 9 10 12 13 15 7 9 14 15 9 7 9 12 15 11 10 11 15 14 14 13 | | 100 100 99 99 100 100 100 100 100 100 10 | 0.0200 0.0400 0.0300 9.9700 9.8900 0.0800 9.9900 9.9400 9.9300 0.0300 0.0200 9.9700 0.0000 0.0600 0.0400 0.0400 0.0100 0.0600 9.9800 9.9800 9.9700 9.9600 0.0500 0.0300 | | 999 999 100 100 100 100 100 100 100 100 | .8542 .5952 .2884 .8038 .4979 .2314 .6303 .8090 .2015 .0512 .8748 .8889 .0887 .0485 .0199 .1244 .0198 .9452 .9395 .9531 .1039 .0847 .1131 .0618 | 0.0020 0.0014 0.0020 0.0014 0.0020 0.0014 0.0020 0.0014 0.0020 0.0014 0.0020 0.0014 0.0018 0.0020 0.0018 0.0017 0.0020 0.0018 0.0017 0.0020 0.0018 0.0018 0.0017 | 0.1658 0.4448 -0.2584 0.1662 -0.6079 -0.1514 0.3597 0.1310 -0.2215 -0.1212 0.1552 0.1311 -0.1187 -0.0485 0.0401 -0.0844 -0.0844 -0.0098 0.0548 0.1205 0.0269 -0.1247 -0.0631 -0.0318 | |
|---|---|----------|--|--|------|--|--|--|---|--|
| | 1 | ADJUSTED | DIP | ECTIONS | | | | | | |
| RA | AY | OBSER | VED-I | DIRECT | ADJU | JSTED- | -DIRECT | STD-ERR | RESIDUALS(") | |
| 1 | 0 | 29 | 59 | 53 00 | 20 | 59 | 47 07 | 2.5001 | -24.27 | |
| 2 | 10 | 209 | 59 | 57 01 | 209 | 59 | 36 98 | 2 5924 | 20.03 | |
| 2 | 11 | 149 | 59 | 58 00 | 149 | 59 | 58 44 | 2 5939 | -0.44 | |
| 2 | 13 | 330 | 0 | 0:00 | 329 | 59 | 56 96 | 2.5955 | 3 04 | |
| 2 | 14 | 269 | 59 | 52 01 | 269 | 59 | 58 62 | 2.5890 | -6 61 | |
| 1 | 14 | 209 | 50 | 52.01 | 209 | 0 | 20.02 | 2.5090 | -0.01 | |
| 4 | 0 | 150 | 0 | 33.00 | 140 | 50 | 20.07 | 2.5313 | -27.07 | |
| 48 A | 20 | 100 | 0 | 4.00 | 149 | 50 | 40.92 | 2.5417 | 17.00 | |
| 4 | 10 | 30 | 0 | 2.02 | 20 | 59 | 40.00 | 2.5410 | 17.24 | |
| 4 | 10 | 30 | 0 | 0.42 | 230 | 29 | 38.40 | 2.5869 | 1.02 | |
| 5 | 11 | 330 | 50 | 2.90 | 330 | 0 | 4.11 | 2.5855 | -1.21 | |
| 2 | 14 | 269 | 29 | 54.5 | 270 | 0 | 12.20 | 2.5345 | -17.83 | |
| D | 10 | 210 | 0 | 5.02 | 210 | 0 | 40.36 | 2.5387 | -35.34 | |
| 5 | 13 | 150 | 0 | 3.90 | 150 | 50 | 5.90 | 2.5942 | -1.94 | |
| 0 | <i>.</i> | 270 | EO | 9.00 | 209 | 59 | 51.14 | 2.5885 | 17.86 | |
| 6 | 9 | 329 | 29 | 54.7_ | 329 | 59 | 38.12 | 2.5353 | 16.59 | |
| 6 | 15 | 30 | 0 | 6.43 | 30 | 0 | 22.41 | 2.5381 | -15.98 | |
| 6 | 14 | 90 | 0 | 1.95 | 90 | 0 | 17.47 | 2.5908 | -15.49 | |
| 8 | 1 | 210 | 0 | 0.00 | 210 | 0 | 23.76 | 2.5881 | -23.76 | |
| 8 | 7 | 150 | 0 | 0.10 | 149 | 59 | 53.96 | 3.5259 | 6.14 | |
| 8 | 9 | 90 | C | 0.10 | 90 | 0 | 6.64 | 3.5250 | -6.54 | |
| 8 | 4 | 29 | 59 | 57.90 | 30 | 0 | 25.28 | 2.5919 | -27.38 | |
| 7 | 1 | 270 | 0 | 0.00 | 269 | 59 | 53.37 | 2.5911 | 6.63 | |
| 7 | 8 | 330 | 0 | 10.00 | 330 | 0 | 2.87 | 3.5259 | 7.13 | |
| 7 | 9 | 29 | 59 | 51.00 | 29 | 59 | 58.01 | 3.5255 | -7.01 | |
| 7 | 6 | 89 | 59 | 57.00 | 89 | 59 | 40.34 | 2.5885 | 16.66 | |
| 9 | 4 | 330 | 0 | 0.00 | 329 | 59 | 43.32 | 2.5417 | 16.68 | |
| 9 | 12 | 29 | 59 | 53.00 | 30 | 0 | 3.58 | 3.0655 | -10.58 | |
| 9 | 15 | 89 | 59 | 55.00 | 89 | 59 | 57.91 | 3.0643 | -2.91 | |
| 9 | 6 | 150 | 0 | 10.90 | 149 | 59 | 52.69 | 2.5353 | 18.21 | |
| 9 | 7 | 209 | 59 | 59.00 | 210 | 0 | 5.21 | 3.5255 | -6.21 | |
| 9 | 8 | 270 | 0 | 5.00 | 270 | 0 | 11.05 | 3.5250 | -6.05 | |
| 12 | 9 | 210 | 0 | 0.00 | 210 | 0 | 9.88 | 3.0655 | -9.88 | |
| | | | | | | - 11 | | | | |



| 12 | 4 | 269 | 59 | 52.00 | 269 | 59 | 35.82 | 2.5416 | 16.18 |
|----|----|-----|----|-------|-----|----|-------|--------|--------|
| 12 | 10 | 330 | 0 | 0.00 | 329 | 59 | 58.58 | 3.5251 | 1.42 |
| 12 | 11 | 30 | 0 | 0.00 | 29 | 59 | 58.66 | 3.5258 | 1.34 |
| 12 | 5 | 90 | 0 | 0.00 | 90 | 0 | 17.27 | 2.5345 | -17.27 |
| 12 | 15 | 149 | 59 | 55.00 | 149 | 59 | 43.09 | 3.0656 | 11.91 |
| 10 | 2 | 29 | 59 | 55.00 | 29 | 59 | 35.17 | 2.5924 | 19.83 |
| 10 | 4 | 209 | 59 | 57.00 | 209 | 59 | 28.12 | 2.5869 | 28.88 |
| 10 | 12 | 149 | 59 | 50.00 | 149 | 59 | 49.58 | 3.5251 | 0.42 |
| 10 | 11 | 90 | 0 | 5.00 | 90 | 0 | 5.55 | 3.5259 | -0.55 |
| 11 | 2 | 330 | 0 | 1.00 | 330 | 0 | 1.14 | 2.5939 | -0.14 |
| 11 | 10 | 269 | 59 | 54.00 | 269 | 59 | 55.65 | 3.5259 | -1.65 |
| 11 | 12 | 209 | 59 | 54.00 | 209 | 59 | 53.26 | 3.5258 | 0.74 |
| 11 | 5 | 150 | 0 | 1.00 | 150 | 0 | 2.40 | 2.5855 | -1.40 |
| 15 | 5 | 29 | 59 | 50.00 | 30 | 0 | 26.84 | 2.5387 | -36.84 |
| 15 | 12 | 330 | 0 | 2.00 | 329 | 59 | 49.39 | 3.0656 | 12.61 |
| 15 | 9 | 269 | 59 | 55.90 | 269 | 59 | 58.72 | 3.0643 | -2.82 |
| 15 | 6 | 210 | 0 | 2.90 | 210 | 0 | 19.24 | 2.5381 | -16.34 |
| 15 | 14 | 150 | 0 | 4.00 | 149 | 59 | 58.86 | 3.5251 | 5.14 |
| 15 | 13 | 89 | 59 | 50.10 | 89 | 59 | 45.82 | 3.5254 | 4.28 |
| 13 | 5 | 330 | 0 | 7.00 | 330 | 0 | 8.63 | 2.5942 | -1.63 |
| 13 | 15 | 269 | 59 | 58.00 | 269 | 59 | 52.93 | 3.5254 | 5.07 |
| 13 | 14 | 209 | 59 | 58.00 | 210 | 0 | 2.53 | 3.5255 | -4.53 |
| 13 | 3 | 149 | 59 | 53.00 | 149 | 59 | 50.66 | 2.5861 | 2.34 |
| 14 | 3 | 90 | 0 | 2.00 | 90 | 0 | 7.61 | 2.5890 | -5.61 |
| 14 | б | 270 | 0 | 0.00 | 270 | 0 | 15.69 | 2.5908 | -15.69 |
| 14 | 15 | 329 | 59 | 58.00 | 329 | 59 | 53.46 | 3.5251 | 4.54 |
| 14 | 13 | 29 | 59 | 50.10 | 29 | 59 | 55.42 | 3.5255 | -5.32 |

APPENDIX C: DERIVATION OF ERROR ELLIPSE PARAMETERS

Given the position variances σ_x^2 and σ_y^2 in two mutually perpendicular directions (typically in the N-S and E-W) and the covariance σ_{xy}^2 we may ask the question, which are the variances σ_m^2 and σ_n^2 in two other mutually perpendicular directions with azimuths ψ and $\psi + 90^{\circ}$ respectively?

It is well known that

 $m = x \cos \psi + y \sin \psi$

 $n = x \cos(\psi + 90) + y \sin(\psi + 90)$

Applying Gauss's Propagation

of Error Law we have



Positional Error Ellipse parameter Derivations

(2)

$$\sigma_m^2 = \cos^2 \psi \, \sigma_x^2 + \sin^2 \psi \, \sigma_y^2 + 2\cos \psi \sin \psi \, \sigma_{xy} \tag{1}$$

Ψ

$$\sigma_n^2 = \sin^2 \psi \, \sigma_x^2 + \cos^2 \psi \, \sigma_y^2 - 2 \cos \psi \sin \psi \, \sigma_{xy}$$

Now it is interesting to consider in which direction is σ_m^2 a maximum and what is the

value of that maximum. For maximum or minimum

$$\frac{\partial(\sigma_m^2)}{\partial\psi} = 0 \tag{3}$$

Hence differentiating (4.3.3)

$$\therefore 0 = -2\cos\psi_m \sin\psi_m \sigma_x^2 + 2\sin\psi_m \cos\psi_m \sigma_y^2 + 2(\cos^2\psi_m - \sin^2\psi_m)\sigma_x$$

$$= -\sin 2\psi_m \sigma_x^2 + \sin 2\psi_m \sigma_y^2 + 2\cos 2\psi_m \sigma_{xy}$$
⁽⁴⁾

giving

$$\tan 2\psi_m = \frac{2\sigma_{xy}}{(\sigma_x^2 - \sigma_y^2)}$$
(5)

substituting this into (4.3.1) and (4.3.2) and manipulating gives

 $\sigma_m^2 = \sigma_{\max}^2 = \frac{1}{2} \left[\sigma_x^2 + \sigma_y^2 + ((\sigma_y^2 - \sigma_x^2)^2 + 4(\sigma_{xy})^2)^{\frac{1}{2}} \right]$ (6a)

$$\sigma_n^2 = \sigma_{\min}^2 = \frac{1}{2} \left[\sigma_x^2 + \sigma_y^2 - \left((\sigma_y^2 - \sigma_x^2)^2 + 4(\sigma_{xy})^2 \right)^{\frac{1}{2}} \right]$$
(6b)

Hence we can compute the directions and values of the maximum and minimum variances at

any point in the network.